

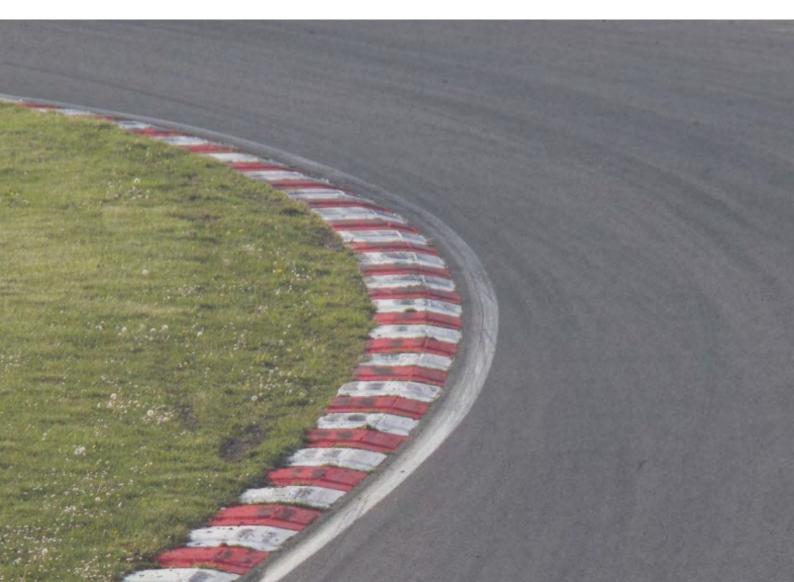
Albany Motorsport Park – Development Application

Water Management Plan

City of Albany

16 August 2021

→ The Power of Commitment



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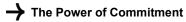
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Abbreviations

Term	Definition
AHD	Australian Height Datum
AMP	Albany Motorsport Park
AMV Inc.	Albany Motorsport Venue Incorporated
ASS	Acid Sulfate Soil
ATV	All-terrain vehicle
BGL	Below ground level
BMP	Best management practices
ВоМ	Bureau of Meteorology
CAMS	Confederation of Australian Motor Sport Limited
CEMP	Construction Environmental Management Plan
CEO	Chief Executive Officer
СоА	City of Albany
DPIRD	Department of Primary Industries and Regional Development
DPLH	Department of Planning, Lands and Heritage
DWER	Department of Water and Environmental Regulation
EMP	Environmental Management Plan
ESA	Environmentally Sensitive Areas
FIA	Federation Internationale de l'Automobile
FIM	Federation Internationale Motocyclisme
GIS	Geographic information system
GoWA	Government of Western Australia
GSMG	Great Southern Motorplex Group Inc.
JDAP	Joint Development Assessment Panel
LGA	Local Government Area
LWMS	Local Water Management Strategy
LGSTWSS	Lower Great Southern Towns Water Supply Scheme
MA	Motorcycling Australia
PDWSA	Public drinking water source area
RIWI Act	Rights in Water and Irrigation Act 1914
SMP	Stormwater Management Plan
TN	Total Nitrogen
ТР	Total Phosphorus
WQPN	Water quality protection note
WSUD	Water sensitive urban design
4WD	Four-wheel drive

1. Introduction

1.1 **Project description**

The City of Albany (CoA) has engaged GHD Pty Ltd (GHD) to prepare an Application for Planning Approval for the staged construction of the Albany Motorsport Park (AMP) at Lot 5780 (No. 54) Down Road South, Drome (the Site) (Figure 1, Appendix A). The project Proponent is the Great Southern Motorplex Group Inc. (GSMG).

At full development, the proposed AMP will consist of:

- Sealed, configurable multi-use track (3.5 km long × 12 m wide) for motor car racing, motorcycle racing, drifting, driver training and cycling:
 - Designed to comply with Motorsport Australia *Track Operator's Safety Guide*^[1] and Motorcycling Australia (MA) *Track Guidelines*^[2].
 - To be licensed by Motorsport Australia for Fédération Internationalé de l'Automobile (FIA) Grade 2 and Fédération Internationalé Motocyclisme (FIM) Grade B (i.e. up to second-tier international motor racing).
- A motocross circuit designed and constructed in association with MA guidelines.
- An off-road four wheel drive (4WD) and all-terrain vehicle (ATV) training area.
- Associated buildings and infrastructure.

Due to the scale and nature of the complex, the works have been broken down into two key stages which comprise of the following:

- Stage 1 (this Development Application):
 - Stage 1A: Construction of motocross track, 4WD driver training area, all-terrain vehicle (ATV) area and associated infrastructure.
 - Stage 1B: Construction of racetrack and associated infrastructure (subject to funding).
- Future Development: Construction and replacement of final permanent structures to support the function of the motorsports complex (subject to funding). Stage 2 will be addressed as a separate Development Application.

A Master Plan, which illustrates the various aspects of the Site and staging areas, has been developed by the GSMG and CoA to support the Development Application for the AMP (Figure 2,Appendix A).

Once operational the AMP will be operated by Albany Motorsport Venue Incorporated (AMV Inc.).

1.2 Site location

Lot 5780 Down Road South, Drome is located approximately 20 km to the north of the Albany CBD and is 192.34 ha in size. The AMP comprises 141.7 ha (including 0.2 ha for crossovers) in the eastern portion of the Site. Two areas within Lot 5780 are excluded from the AMP development and include 49.47 ha at the western end of the Site which is covered with native vegetation and a dam area (1.37 ha) on the northern boundary which is subleased to Plantation Energy.

The site is zoned 'Special Use - SU26' under City of Albany Local Planning Scheme No. 1.

The Site is bounded by Down Road West to the north, Down Road South to the east, Lot 5781 Down Road South to the south (privately owned) and a local road reserve and the Avon-Albany rail reserve to the west. The Site is located adjacent to the Mirambeena Timber Processing Precinct and sits within the industrial buffer area.

¹ CAMS. (2012). Track Operator's Safety Guide. Malvern East: Confederation of Australian Motor Sports.

² MA. (2011). *Track Guidelines*. South Melbourne: Motorcycling Australia.

1.3 Purpose of this report

This Water Management Plan (WMP) has been prepared to support the Application for Planning Approval. The WMP identifies the principles, criteria and water management strategies to manage water across the Site during construction and operational phases.

1.4 Albany Motorsport Park design

1.4.1 Events and usage

For the purposes of sizing facilities and infrastructure GSMG have provided conceptual usage of the AMP, with an assumed typical /frequent site attendance of 300 persons for the Motocross Precinct and 500 persons for the Race Track Precinct (i.e. competitors + officials + spectators). This was determined through discussion with the GSMG on the nature and size of expected typical events. For special events that anticipate a greater number of site attendees, additional water servicing management measures will need to be implemented (e.g. drinking water carts, port-a-loos).

1.4.2 Elements of AMP design

Key elements of the track design and consideration for Water Sensitive Urban Design (WSUD) are summarised in Table 1.

Track element	Description	WSUD considerations
AMP facilities	 Includes the following: Facility buildings (clubrooms, first aid, toilets, storage sheds) 	Considered impervious areas contributing surface runoff. To be protected from flood events.
	Carpark (competitor and spectator)Pit and garage areasRefueling area	Pit and garage areas and refueling areas are key water quality treatment areas.
Access roads	Entry and exit roads consisting of 7 m wide gravel road, with 2 m wide grassed verges either side.	Road and verge have limited permeability.
Overflow parking	Grassed overflow parking	Considered pervious.
Race Track pavement	The Race Track pavement consists of 12 m wide track.	Considered impervious areas contributing surface runoff.
Race Track verge	The Race Track verge is predominantly grass and gravel with limited asphalt on T11.(recovery area)	Gravel verge is considered permeable.
Run-off areas	Run-off areas occur around the Race Track to enable drivers to dissipate speed during a race. Run-off areas are composed of loose gravel underlain by compacted pavement material.	Pavement layer underneath is considered impervious.
Motocross Track	Compacted clay and sand Motocross track.	Limited permeability.
4WD Driver Training and ATV Precinct	4WD and ATV area comprises finished natural surface after removal of some gravel, sand and clay to build the Motocross track.	Limited permeability.

 Table 1
 Key AMP design elements and WSUD considerations

1.5 Previous studies

Numerous studies and investigations have been undertaken to support development planning for the Albany Motorsports Complex. A summary of key documents of relevance to integrated water management of the Site is provided below:

- Pavement Investigation Report 4212/1 Albany Motorsport Park Development (Great Southern Geotechics , 2021)
 - A geotechnical investigation was completed for the proposed Albany Motorsport Park Development including assessment of soil types and profiles, characteristics of selected soil samples and completion of in-situ permeability testing at selected locations.
- Albany Motorsport Park Local Water Management Strategy (GHD, 2021)
 - A Local Water Management Strategy (LWMS) was prepared (as part of the Scheme Amendment) that identified the key water management principles, design criteria, and strategies for the proposed development of the Albany Motorsport Park. The water management strategies in the LWMS were developed with reference to the concept track design and with regard to the site characteristics.
- Albany Motorsport Park Site Feasibility Study Lot 5780 Down Road South, Drome (GHD, 2018)
 - A site feasibility assessment was completed as part of preliminary planning investigations for the
 proposed Albany Motorsport Park. The feasibility assessment included a range of desktop technical
 investigations including review of servicing requirements and traffic impact assessment, and desktop
 geotechnical, hydrogeological, noise and water management planning. The feasibility assessment
 further included a preliminary risk assessment of the key issues identified and identified a suite of
 recommended remedial actions based on a hierarchy of controls. A number of recommended remedial
 and control actions were outlined to provide guidance for the various stages of the development.
- Albany hinterland prospective groundwater resources map; Explanatory notes (DWER, 2017)
 - Hydrogeological report and map for the Albany hinterland developed by the Department of Water and Environmental Regulation (DWER) as part of the Royalties for Regions South Coast Groundwater Investigation project. The Albany hinterland area in the South Coast is known as an important resource for water supply in the Great Southern region. In 2013, DWER undertook some hydrogeological (surface water and groundwater) investigations (as part of South Coast groundwater investigation by Western Australian Government on groundwater availability) and mapped prospective groundwater resources in the Albany hinterland region in order to support regional developments.
 - The report and map were used to develop a conceptual hydrogeological model for the Site as part of the LWMS, in order to understand the groundwater and surface water sources and pathways.
- Motorplex Development, Down Road Surface and Groundwater Monitoring 2018 Summary Report (Bio Diverse Solutions, 2018)
 - Summary reporting of shallow groundwater monitoring bore monitoring program. Monitoring of shallow
 groundwater bores installed across the Site commenced in February 2018. The 2018 report
 summarises preliminary results for the 2018 monitoring period, with additional monitoring completed up
 to November 2019 which were included in the LWMS.
- Proposed Motorsport Park, Lot 5780 Down Road, Drome Reconnaissance Flora and Level 1 Fauna Survey Report (Bio Diverse Solutions, 2019)
 - Bio Diverse Solutions completed a desktop assessment and reconnaissance flora survey and Level 1 Fauna survey of the Project Site in Spring 2018. The survey included identification of habitat trees and threatened fauna dependent hollows, and mapping of vegetation communities (GIS mapping, vegetation condition mapping, fauna habitat types and condition).

1.6 Scope and limitations

This report: has been prepared by GHD for City of Albany and may only be used and relied on by City of Albany for the purpose agreed between GHD and City of Albany as set out in section 1.3 of this report. GHD otherwise disclaims responsibility to any person other than City of Albany arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.

GHD has prepared this report on the basis of information provided by City of Albany and others who provided information to GHD (including Government authorities), which GHD has not independently verified or checked beyond the agreed scope of work. GHD does not accept liability in connection with such unverified information, including errors and omissions in the report which were caused by errors or omissions in that information.

2. Existing environment

This section summarises key information relating to catchment characteristics for the Site. The LWMS (GHD, 2021) provides a comprehensive overview of environmental characteristics.

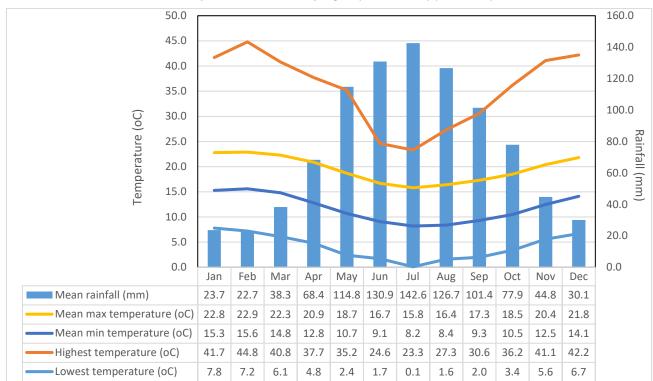
2.1 Existing activities

The perimeter of the site is entirely fenced and is currently used for the primary purpose of cattle grazing. Historically the site is likely to also have been used mainly for the purpose of agriculture, as well as some limited resource extraction (sand and gravel). The western end of the site consists of 52 ha of native vegetation that will be retained. A number of small dams are located across the site for stock watering. These will be retained and maintained for the AMP.

2.2 Climate

Albany is located on the south coast of Western Australia and the climate is broadly described as Mediterranean, with warm dry summers and mild wet winters. The nearest Bureau of Meteorology (BoM) official recording station is Albany Airport (Station No. 9500). This station records temperature, rainfall, relative humidity, wind speed and direction and has data available dating back to 1877. Table 2 illustrates recorded average monthly meteorological data for the Bunbury AWS BoM station for years 1877 to 2020 (BoM, 2020).

Temperatures range from a mean maximum of 22.9 °C in summer and drop to a mean maximum of 15.8 °C in winter. Mean minimum temperatures follow a similar trend, reaching 15.6 °C in summer and 8.2 °C in winter. Rainfall is low throughout the summer months and peaks in July, with a monthly average of 142.6 mm. The mean annual rainfall is 925.2 mm, with approximately 103.1 rain days a year. Relative humidity at Albany reflects the Mediterranean climate, demonstrating drier summers and a comparatively high relative humidity of 82 % in the morning in winter (BoM, 2020).





2.3 Topography, landform and soils

2.3.1 Topography

The surface elevation of the site ranges from approximately 41 m AHD to 73 m AHD (GoWA, 2021). The lowest elevation is on the southern boundary and extends through the center of the site within a gully (a tributary to Marbelup Brook) that lies in a north-easterly direction. The highest elevation occurs on the eastern boundary of the site.

2.3.2 Surface soils and geology

Regional geology is described with reference to the 1:50,000 Environmental Geology series map (Albany sheet) and the 1:250,000 Geological Series map (Mt Barker – Albany sheet). These indicate the site is underlain by Cainozoic sand of colluvial origin – "Qc: *Colluvium* – *Sand, silt and clay*" on the slopes and within the low-lying areas of the Marbelup Brook "QA – *Clay, silt, sand and gravel in watercourses*" (Allen & Sofoulis, 1984). The sand is described as pale grey, fine to coarse, angular to sub-rounded quartz that is loose and moderately sorted and contains occasional pebbles of laterite. The thickness of the sand unit is not indicated on the maps, however the 1:250,000 map sheet indicates sand unit generally overlays laterite.

Local soils and geology are further delineated by Department of Primary Industries and Regional Development (DPIRD) Soil Landscape Mapping as summarized in Table 3 and presented in Figure 3 (Appendix A).

Site investigations were completed by Great Southern Geotechnics across the site in March 2021 to assess soil types and profiles and in-situ permeability. Eight test pits were completed, with soil types typically in agreement with DPIRD Soil Landscape Mapping. Gravels were identified on the western slope in the vicinity of the 4WD Driver Training and ATV Area, and deep sands present on the valley slopes and duplex soils in the valley floors.

In-situ soil permeability testing was completed for test pit locations TP4 to TP8, with saturated hydraulic conductivity ranging between 0.41 m/day (TP8) and 3.29 m/day (TP6 and TP7).

The locations of the test pits, soil logs and soil permeability results provided in Appendix B.

Map unit symbol	Name	Landform	Geology	Soil
242KgDMc	Dempster Crest phase	Broad convex crests of sandy and lateritic spurs and ridges	Deeply weathered siltstone	Duplex sandy gravels; Grey deep sandy duplexes; Pale deep sand; Shallow gravels
242KgS7f	Minor Valleys S7 floor phase	Foot slopes and swampy valley floors of minor valleys	Colluvial and alluvial deposits over weathered sedimentary rocks	Wet and semi-wet soils; Pale deep sands; Grey deep sandy duplexes
242KgS7h	Minor Valleys S7 slope phase	Side slopes of minor valleys	Colluvium sedimentary rocks	Pale deep sands; Grey deep sandy duplexes
242ReDMc	Dempster Crest phase	Elongate crests	No information recorded	Sands and laterite

 Table 3
 Soil map units within the Project Site (GoWA, 2021)

2.3.3 Acid sulfate soils risk mapping

An overlay of the site onto the DWER ASS risk mapping for the Albany-Torbay region (GoWA, 2021) is presented as Figure 4 (Appendix A), which identifies that the site is located outside of the boundary extent of the mapped areas.

Given that tributaries of Marbelup Brook located approximately 750 m to the south of the site are mapped as "Moderate to Low Risk" of ASS occurring, GHD has inferred that where these tributaries of Marbelup Brook extend into the site that they would also be considered to represent the same level of ASS risk. This is also consistent with the more broadly mapped risk areas where there are obvious low lying drainage lines, creeks and tributaries.

To more accurately inform the ASS risk onsite, a preliminary ASS investigation was completed as part of the onsite geotechnical investigation undertaken by Great Southern Geotechnics on 25 March 2021. Based on the ASS assessments to date, inorganic sulfidic sources capable of rapid acid release upon disturbance were not observed. Other, more slow releasing acidity sources were observed in the ASS assessment and will require management if disturbed in volumes greater than 100 m³.

Any impacts associated with dewatering (if required) during construction will need to be considered in the ASS management plan. Further detail is captured in the associated AMP Environmental Management Plan.

2.4 Hydrology

A summary of desktop searches related to hydrology datasets is provided in Table 4. Further detail is provided in the following sections where relevant.

Dataset	Details	Result
Public Drinking Water Source Areas (PDWSA)	PDWSA is a collective term used for the description of Water Reserves, Catchment Areas and Underground Pollution Control Areas declared (gazetted) under the provisions of the <i>Metropolitan Water Supply, Sewage and Drainage Act 1909</i> or the <i>Country Area Water Supply Act 1947</i> .	Site lies within the Priority 2 Marbelup Brook Catchment Area (Section 2.4.1).
Groundwater Areas	Groundwater areas proclaimed under the <i>Rights in Water and Irrigation Act 1914</i> (RIWI).	Site lies within Albany Groundwater Area (Section 2.4.2, Figure 5).
Surface Water Areas	Surface water areas proclaimed under the RIWI Act 1914.	None present.
Irrigation District	Irrigation Districts proclaimed under the RIWI Act 1914.	None present.
Rivers	Rivers proclaimed under the RIWI Act 1914.	None present.
Waterways Management Areas	Areas proclaimed under the <i>Waterway Conservation Act</i> 1976.	None present within the Site; however, the Albany Waterways Management Area is located approx. 800 m to the north.
Clearing Control Catchments	Country Area Water Supply Act 1947 Part 2A.	None present.
South Coast Significant Wetlands	Represents the regionally significant wetlands of the South Coast.	Site contains the Marbelup Flats, a conservation class wetland (Section 2.4.3).

 Table 4
 Summary of hydrology dataset queries within the Project Site

2.4.1 Public drinking water source area

The site is located within a Priority 2 (P2) area of the Marbelup Brook public drinking water source area (PDWSA) (GoWA, 2021). This PDWSA is gazetted under the *Country Areas Water Supply Act 1947*, however is currently not used. It has been identified as a potential future water source option in the *Great Southern Regional Water Supply Strategy 2014* (DoW, 2014).

The Minister for Water has formally provided advice to the City of Albany (Kelly, 2018) that while a motorsport facility is incompatible with a P2 PDWSA (DoW, 2016), "*there are measures that can be put in place to protect water quality should the City proceed to approve the development*". These measures are further discussed in Section 4.2 (Wastewater servicing), Section 5.2 (Stormwater quantity management), Section 5.3 (Stormwater quality management) and Section 6 (Construction management) and Section 7 (Monitoring).

2.4.2 Groundwater conditions

On a regional scale, the 250K Map Series – Hydrogeology identifies a "*sedimentary aquifer within intergranular porosity – extensive aquifers, major groundwater resources*" underlying the Site (DoW, 2002). Groundwater salinity in the local area is in the range of 500 – 1000 mg/L, which is considered to be marginal for productive uses (GoWA, 2021).

A review of the DWER Water Information Reporting database identified no publicly available groundwater level or groundwater quality data within 2 km from the Site.

2.4.3 Wetlands and groundwater dependent ecosystems

Desktop searches identified no internationally important (Ramsar) or Nationally Important listed wetlands within 5 km of the Site (GoWA, 2021).

The South Coast Significant Wetlands dataset (DBCA-018) identifies the unnamed water course located within the Site as the Marbelup Flats, part of the King River Suite, and a Conservation Class wetland (Figure 4, Appendix A) (GoWA, 2021).

2.4.4 Surface water features

An unnamed creek line runs from the north-east corner of the site through to the south-west corner, from where it joins into Marbelup Brook located approximately 800 m west of the site boundary.

During a site visit (June 2018) the watercourse was observed to be in a modified state, with cattle currently having access to the watercourse. Erosion was evident, particularly in the eastern extent of the watercourse. This area was also mostly devoid of native vegetation, with the exception of some sedges (*Juncus* spp) (GHD, 2018). The western section of the watercourse contains native shrubs / sedges and had a defined bed / banks.



Plate 1 Eastern extent of the watercourse showing evidence of erosion and cattle access

2.4.5 Summary of pre-development monitoring (Bio Diverse Solutions)

Bio Diverse Solutions completed quarterly monitoring of surface water and groundwater at the Project Site for the period February 2018 to November 2019. An overview of the key results is provided in the following sections with sampling locations, the 2018 summary report and baseline water quality results for surface water and groundwater provided in Appendix C.

2.4.5.1 Surface water

Field records indicate two surface water sample locations within the unnamed watercourse were flowing for all monitoring dates in 2018 (Feb, May< Sep, Nov 2018), with flow at the downstream site (CS01) on all dates in 2019 (Feb, May, Aug, Nov).

An overview of key surface water quality data include:

- Surface water pH is moderately acidic, ranging from 4.46 to 6.85.
- Total nitrogen (TN) concentrations were typically higher at the upstream surface water location CS02 (TN range of 2 mg/L to 6.5 mg/L) compared to the downstream location CS01 (TN range from 0.5 mg/L to 2 mg/L)
- Total phosphorus (TP) concentrations were higher at the upstream surface water location CS02 (TP range from 0.22 mg/L to 0.55 mg/L) reflecting the TP concentration of bores in proximity to CS02. TP concentrations were typically below detection levels at the downstream surface water location CS01.
- Dissolved metals parameters including aluminium, iron and zinc were elevated in several samples at downstream surface water location CS01. Site CS02 reported isolated elevated aluminium, iron and zinc.
- MBTEXN parameters reported below detection in all surface water samples.
- TRH fractions were detected in some surface water samples.
- PAH parameters reported below detection in all surface water samples.
- Microbial testing detected microbial parameters in the majority of surface water samples.

2.4.5.2 Ground water

A summary of groundwater level records is provided in Table 5.

Table 5Groundwater levels

		Northing (m)	Ground level – est. RL (mAHD)	Depth to	Depth to Groundwater (mBGL)						
Bore ID				Feb 2018	May 2018	Sep 2018	Nov 2018	Feb 2019	May 2019	Aug 2019	Nov 2019
SB01	567179	6133615	58.4	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB02	567404	6133889	49.6	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB03	567519	6134401	56.8	> 2.0	> 2.0	1.21	1.93	> 2.0	> 2.0	1.45	> 2.0
SB04	567700	6134179	48.2	> 2.0	0.91	0.30	1.07	1.66	1.11	0.37	1.48
SB05	568056	6134636	60.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB06	568131	6134478	53.6	0.87	0.70	0.00	0.59	1.03	0.73	0.06	0.73
SB07	567939	6134264	51.6	0.64	0.54	0.44	0.64	0.95	0.58	0.52	0.64
SB08	568308	6134637	56.5	> 2.0	1.55	0.18	1.27	1.58	1.42	0.38	1.29
SB09	568032	6134141	50.3	0.66	0.57	0.44	0.78	0.98	0.87	0.61	0.99
SB10	567886	6133756	62.7	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB11	568314	6134267	68.6	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB12	568474	6134781	60.2	> 2.0	> 2.0	1.04	> 2.0	> 2.0	> 2.0	1.1	> 2.0
DB01	-	-	-	-	-	-	-	-	7.10	6.95	6.97
Notes	BGL – below ground level - Where results shown as "> 2.0", this means the groundwater table was not intersected by the shallow groundwater monitoring bore (being only 2 m deep)						1				
	Results sl	Results shown in red font - groundwater table was intersected by the groundwater monitoring bore.									
	Deep bore	Deep bore (DB01) monitoring only commenced from May 2019.									

An overview of key groundwater quality data include:

- Groundwater pH is moderately acidic, typically ranging from 3.82 to 7.52. pH at SB06 and SB07 (2.5 and 2.8) were significantly lower in February 2018 sampling event.
- Total nitrogen (TN) concentrations were typically elevated across the Site (range from 2 mg/L to 28 mg/L), which may be attributed to the historic and current farming practices. Significantly elevated TN at some bores (SB06, SB07 and SB08) coincided with sampling following peak groundwater levels. Exceptionally elevated TN concentrations reported in bore SB08 in February and May 2019 (110 and 79 mg/L), and additional sampling is recommended to confirm concentrations.
- Total phosphorus (TP) concentrations were typically elevated in some bores (SB06, SB07 and SB08).
- Dissolved metals parameters including aluminium, iron and zinc were elevated in the majority of samples in all bores, suggesting background concentrations of these metals are elevated due to the local soil and geological profile. Dissolved chromium was also elevated above the default trigger value in some bores.
- With the exception of toluene MBTEXN parameters reported below detection in the majority of groundwater samples. Toluene was detected in bore SB04 on all sampling occasions, and in bores SB06, SB07, SB08, SB09 in some sampling occasions. Toluene was elevated above the ANZG (2018) default toxicant guideline value in samples from SB07 (770 ug/L) and SB08 (210 ug/L, 310 ug/L, 980 ug/L).
- TRH fractions were detected in some groundwater samples. Particularly elevated TRH fractions were reported for bore SB07 and SB08 in February 2019. It is recommended that additional TRH samples are collected, with silica gel cleanup requested from the laboratory where elevated samples are identified.
- With the exception of a single detection for Naphthalene (SB06, Sept 2019) PAH parameters reported below detection in all groundwater samples.
- Microbial testing detected microbial parameters in some groundwater samples at all bores

2.4.6 Conceptual hydrogeological model

A conceptual hydrogeological model was developed for the site to gain an initial understanding of surface and groundwater water flows and potential linkages. Soil landscape mapping and regional geology mapping were used to infer geological units and soil types in the absence of deeper borehole data. The outcomes of the model (see Appendix D) noted:

- The groundwater levels observed in the shallow bores indicate that groundwater is present in the lower lying
 areas nearer the creek and will be most likely be supplying the creek with groundwater inflow.
- The groundwater levels and gradient, inferred from topography, supports that groundwater discharges into the creek.
- Shallow/perched groundwater may discharge and resurface via sandier layers that sit on top of more impermeable lateritic, coffee rock or clay layers; especially when there is significant slope.
- The discharging groundwater either expresses as surface water, or migrates within the deeper more permeable deposits.

2.4.7 Existing hydrological regime

2.4.7.1 Pre-development hydrology

A catchment analysis was completed using CatchmentSIM to delineate pre-development catchments for the entire site, including upstream areas. Refer to Figure 6 in Appendix A.

A one-dimensional DRAINS model with ILSAX hydrology was used for calculation of runoff. Model parameters included:

- Paved (impervious) area depression storage = 1 mm
- Supplementary area depression storage = 1 mm
- Grassed (pervious) area depression storage = 5 mm
- Soil Type 3 (slow infiltration rates).

The assessment was determined in accordance with Australian Rainfall and Runoff (ARR) 2016 (Geoscience Australia, 2016), with design rainfall data from the ARR 2016 data hub and the Bureau of Meteorology (BoM, 2018). The estimated peak flows for pre-development from various catchments are shown below in Table 6. Further assessment of specific areas impacted by the project works are further detailed in section 5.2.5. These focus on predevelopment areas surrounding the western motocross development and the eastern race track development, where the majority of the changes to the site occur.

Catchment	Area (ha)	Impervious	Peak flows (n	Peak flows (m³/s)					
		fraction (%)	1EY (1 yr ARI)	0.5 EY (2 yr ARI)	10% AEP (10 yr ARI)	1% AEP (100 yr ARI)			
E1	19.8	3	0.06	0.08	0.43	2.44			
E2	17.4	3	0.08	0.10	0.39	2.24			
E3	15.3	3	0.01	0.02	0.36	1.97			
E4	13.9	0	0.00	0.00	0.45	2.27			
E5	36.4	60	0.00	0.00	0.00	0.67			
E6	17.4	0	0.00	0.00	0.33	1.81			
S1	14.1	0	0.00	0.00	0.31	1.64			
S2	23.4	0	0.00	0.00	0.57	3.30			
S3	41.6	0	0.00	0.00	1.02	6.07			
S4	33.6	0	0.00	0.00	0.65	3.64			

Table 6 Estimates of peak flows pre-development

Catchment	Area (ha)	Impervious	Peak flows (m³/s)						
		fraction (%)	1EY (1 yr ARI)	0.5 EY (2 yr ARI)	10% AEP (10 yr ARI)	1% AEP (100 yr ARI)			
S5	25.1	0	0.00	0.00	0.90	4.18			
TOTAL	262.7	-	0.03	0.03	1.82	17.0			
<u>Note:</u>		E denotes an external catchment, S denotes a catchment within the site or with a significant portion of the catchment within the site.							
	TOTAL denote catchments du	TOTAL denotes the flows leaving the site via the creek/wetland which may be different to the individual catchments due to routing and storage within the site/model.							

2.4.7.2 Flood modelling

To inform the design of site infrastructure, a site-wide modelling of the existing (or pre-development) flood conditions was undertaken. This entailed simulating the 1% AEP storm event over the site using TUFLOW (Build 2020-10-AA), which is a program for simulating depth-averaged, one and two-dimensional free surface flows (such as occurs from floods and tides). Calibration of the model was not performed, as there are no operational streamflow gauges in vicinity and/or relevant to the site.

2.4.7.2.1 Model setup and assumptions

Modelling was done using a 'rainfall-on-grid' approach, in which the design rainfall hyetograph is applied directly to a Digital Elevation Model (DEM) that describes the site topography. The DEM was generated with a 5 m cell resolution using 1 m surface contours from Landgate, which is the finest available topography data that is publicly available for the site.

Routing of surface runoff over the DEM is influenced by the surface roughness, which is characterised by assigning Manning's roughness values to each DEM cell. Characterisation of the surface roughness was done through manual interpretation of the latest aerial imagery, with each identified surface type assuming the roughness values listed in Table 7.

Surface type	Manning's roughness n*
Cleared and grassed	0.050
Forested	0.070
Bare earth	0.040
Paved/roof areas	0.020

 Table 7
 Adopted surface roughness values in flood modelling

* Note: Values determined based on Table 6.2.2 in Book 6 of ARR 2019.

Catchment hydrological losses were simulated using an initial and continuing loss approach. With the exception of existing impervious areas, an initial and continuing loss values of 27 mm and 3.4 mm/hour were globally applied to the model domain. For paved and roofed areas, the initial loss was set to 1 mm and no continuing loss was applied. The effects of rainfall pre-burst are also accounted for in modelling by subtracting the median pre-burst depths (extracted from the ARR Data Hub) from the initial loss value.

Culverts across Down Road West were simulated as one-dimensional elements within the greater twodimensional model. In the absence of detailed survey information, the culvert sizes were determined based on manual measurements taken by the Great Southern Motorplex Group on 17 June 2021; whilst culvert levels were set the same as the topographical low spots. Only two of the three culverts identified along the road were modelled. The culvert near the northeast corner of the site (i.e., Culvert E on Figure 7) could not be modelled due to the coarse resolution of the topography dataset, which did not accurately reflect the road geometry and adjacent table drains. An open flow boundary is assumed along the perimeter of the model domain. This effectively simulates free discharge of flood waters out of the model and towards low lying areas external to the domain.

2.4.7.2.2 Modelling outcomes

The simulated maximum flood depths and flow velocities for the 1% AEP storm event are provided in Figure 7 and Figure 8 in Appendix A. The results demonstrate that majority of the site drains to the central creek line via overland sheet flow and has very shallow or negligible flood depths; other than in obvious gullies or valleys.

Elevated floodwaters are simulated along the main creek that traverses the site, with localised spots where the flood depth and flow velocities exceed 1 m or 1 m/s in the 1% AEP storm event. Nevertheless, the simulated creek flood extents are largely contained within the proposed Protected Exclusion Area (which will be fenced off) and not expected to interfere with future site operations.

Concentrated flows are expected to occur across the centre of the motocross track, as well as the northern and southern portions of the multi-use racetrack. The simulated flood depths at these areas are generally less than 200 mm but will require provisioning of culverts and/or floodways to mitigate standing water on tracks.

Some flooding is simulated at two low spots north of Down Road West, with flood depths of up to 0.6 m at the western low spot and as high as 0.9 m at the eastern one in the 1% AEP storm event. Both low spots are drained via cross-carriageway culverts that discharge directly to the northern boundary of the site. In particular, the western culvert (i.e., Culvert W) discharges directly towards the proposed motocross track and diversion of these flows will need to be considered as part of this site's stormwater management. This is further discussed in Section 5.

Table 8 summarises the simulated flows and velocities through each culvert.

Culvert details	Culvert W	Culvert C	Culvert E
Diameter (mm)	750	900	1050
Flow (m³/s)	0.48	1.07	3.54*
Velocity (m/s)	2.04	2.61	NA

Table 8 Simulated 1% AEP culvert flows and velocities

* Note: Culvert not modelled. Overland surface flow used as proxy for culvert flow.

Some external catchment runoff from the CBH Mirambeena grain receival site is also expected to flow across Down Road and into the site from the north-east corner, partially through Culvert E. The natural flow path of this external flow cuts across the northern tip of the multi-use track and will need to be diverted accordingly.

2.5 Water users

2.5.1 Surface water

Review of aerial photography identifies numerous small dams located within Marbelup Brook and riparian zone (as demarcated by the DWER South Coast Significant Wetlands coverage), and one potential surface water abstraction (pumping) site downstream of the Site. These locations are summarised in Appendix E.

2.5.2 Groundwater

Groundwater allocation in Western Australia is regulated by DWER. The DWER Water Register notes one groundwater license for the Site and five groundwater licenses downgradient / downstream of the Site along the Marbelup Brook. The groundwater licences are summarised in Appendix E.

2.6 Environmentally sensitive areas

2.6.1 DWER Environmentally sensitive areas

The DWER maintains a dataset of Environmentally Sensitive Areas (ESA). ESAs are areas of land deemed to support conservation, heritage or ecological value, or an area protected through existing State Policy. There are no mapped Environmentally Sensitive Areas (ESA) within 5 km of the Project Site (DWER-046).

As per DWER guidance (DER 2014) a conservation category wetland is "*a defined wetland and the area within* 50 m of the wetland" and is declared to be an ESA under the *Environmental Protection Act 1986.* The Conservation Class wetland within the Project Site (Section 2.4.3, Figure 4) is identified as an ESA.

2.6.2 Groundwater dependent ecosystems

A search of the online *Groundwater Dependent Ecosystems (GDE) Atlas* (BoM 2020) does not identify any terrestrial or aquatic groundwater dependent ecosystems within the Project Site boundary.

2.6.3 Flora and fauna

Bio Diverse Solutions (2019) completed a Level 1 Fauna Survey and a reconnaissance level flora survey in spring 2018. The reconnaissance level flora survey did not identify any EPBC Act, BC Act or State Priority listed flora species within the Project Site.

The Level 1 fauna survey observed four conservation significant fauna species directly and indirectly within the broader survey area including:

- Baudin's Cockatoo (*Calyptohynchus baudinii*) (Vulnerable, Schedule 2)
- Forest Red-tailed Black Cockatoo (*Calyptohynchus banksia naso*) (Vulnerable, Schedule 3)
- Western Brush Wallaby (Notamacropus irma) (Priority 4)
- Southern Brown Bandicoot, Quenda (Isoodon fusciventer) (Priority 4).

Marbelup Brook was identified to have high aquatic fauna species richness from monitoring for the study *Ecological values of waterways in the south coast region, Western Australia* (Cook, Janicke, & Maughan, 2008). The high aquatic fauna species richness was partly attributed to the high number of samples collected, comprising 28 sites including three sites (MAR07, MAR08 and MAR09) located within and immediately downstream of the Site.

2.7 Sewage sensitive areas

The Department of Planning Lands and Heritage Map of Sewage Sensitive Areas identifies that the majority of the site is located within a sewage sensitive area (within 1 km of significant wetlands).

3. Design criteria and objectives

This section outlines the design criteria and objectives that the Water Management Plan (WMP) for the site must achieve. The design criteria have been developed with reference to the principles and objectives and guidance in the following:

- AMP Feasibility Study (GHD, 2018)
- Stormwater Management Manual for Western Australia (DoW, 2007)
- Decision process for stormwater management in Western Australia (DWER 2017)
- Subdivision and Development Guidelines 2018 (CoA, 2018)
- WQPN 100: Motor sport facilities near sensitive waters (DoW, 2007)
- WQPN 28: Mechanical servicing and workshops (DoW, 2013)
- WQPN 52: Stormwater management at industrial sites (DoW, 2006).

Water and wastewater supply and servicing

This WMP proposes the following water supply design criteria for the site:

- Criteria WS1: Potable water will be supplied through collection and treatment of rainwater to potable standard. Non-potable water will be supplied via bore, site dam and rainwater tanks.
- Criteria WS2: Shortfalls in potable water supply will be imported to the site.

Further detail is provided in Section 4.1.

The wastewater management strategy proposes the following design criteria for the site:

- Criteria WW1 (Stage 1A): Domestic wastewater will be serviced using a combination of transportable toilets (with waste disposal managed by a waste management contractor) and a permanent on-site treatment and disposal system, in accordance with the *Government Sewerage Policy* (DoH, DPLH, DWER, 2019) for a PDWSA and Sewage Sensitive Area.
- Criteria WW1 (Stage 1B): Domestic wastewater will be serviced using transportable toilets (with waste disposal managed by a waste management contractor)
- Criteria WW2: Wastewater from vehicle maintenance, refuelling and washdown areas will be managed in accordance with WQPN 28.

Further detail of domestic wastewater servicing is provided in Section 4.2.1, with detail of vehicular maintenance servicing areas provided in Section 4.2.2.

Stormwater management

This WMP proposes the following stormwater design criteria for the site:

- Criteria SW1: Maintain the hydrological regime of the site and surrounds.
- Criteria SW2: Maintain serviceability of motorsport tracks for the 10% AEP event.
- Criteria SW3: Provide adequate drainage to achieve 300 mm separation from the 1% AEP event for key infrastructure (e.g. vehicle maintenance areas, buildings, wastewater facilities).

Water quality management

This WMP proposes the following water quality design criteria for the site:

- Criteria WQ1: Manage stormwater from the Site to ensure no deterioration in surface and groundwater quality.
- Criteria WQ2: Retain and treat stormwater runoff from constructed impervious surfaces generated by the first 15 mm of rainfall at source, prior to discharge or disposal to groundwater.
- Criteria WQ3: Manage stormwater quality from the Site in accordance with WQPN 100, WQPN 28 and WQPN 52.

4. Water supply and servicing

4.1 Water supply

4.1.1 Potable water

The Water Corporation's Lower Great Southern Towns Water Supply Scheme (LGSTWSS) runs along Albany Highway, with the nearest connection point approximately 4 km to the east at 66 Down Road (fertiliser distribution warehouse) (Water Corporation, 2018). Hence, it is proposed to service Site drinking water needs through a combination of collected rainwater and water carts.

Uncontaminated rainwater from the Site roof runoff (AMP buildings) will be collected in standard 110,000 litre rainwater tanks. At source treatment by household-scale filtration and ultraviolet disinfection will be undertaken. This will allow a safe drinking water supply to the AMP facilities (i.e. clubrooms, canteen, etc.) and ablutions.

A preliminary water balance for the site suggests that rainfall alone will be insufficient to meet expected demand for regular attendance of 500 people. Where there is a shortfall, the venue operator will purchase and cart water to the Site. Similarly for large-scale events, additional potable water will need to be carted to site.

4.1.2 Non-potable

Water demands for other external, non-potable uses (i.e. garden irrigation, toilet flushing, vehicle washdown, dust suppression, etc.) will be met from Site bore, dams and rainwater tanks (where possible). The GSMG is negotiating with Plantation Energy for access to their 4,000 kL Bremer West superficial groundwater allocation (licence number 168308).

4.1.3 Fire water

Fire water supply will be through on-site resources via bore extraction to tank storage and pumped to facilities around the site. Storage of water dedicated for firefighting will be located in the north and the eastern precincts and tanks are to be a minimum of 110,000 L (as shown on Masterplan).

4.2 Wastewater servicing

4.2.1 Domestic wastewater

The Water Corporation's Albany sewerage scheme is not in close proximity to the Site, with the nearest connection point being at Lancaster Road, McKail (being some 10 km distant).

Stage 1A of the development will be serviced by a combination of transportable toilet units (Plate 2) and permanent toilets in the multi-purpose building (sized for 300 patrons). The permanent toilets are connected to an on-site treatment and disposal system, designed in accordance with the *Government Sewerage Policy* (DoH, DPLH, DWER, 2019) for a PDWSA and Sewage Sensitive Area. A full site and soil evaluation report is attached in Appendix H. The transportable toilet units will be maintained and regularly serviced by a local waste disposal contractor. For large-scale events additional portable hire toilet units will be used to accommodate peaks in wastewater production.

Stage 1B of the development will be serviced by transportable toilet units only (Plate 2). The transportable toilet units will be maintained and regularly serviced by a local waste disposal contractor. For large-scale events additional portable hire toilet units will be used to accommodate peaks in wastewater production.



Plate 2 Example portable toilet unit

4.2.2 Vehicular maintenance wastewater

The Site is proposed to be used for motor sport activities. All vehicle maintenance and servicing including vehicle washdown and refueling, will be undertaken in dedicated refueling and pit areas.

To minimise the risk of contamination to sensitive receptors the refueling and pit areas will be designed and constructed in accordance with WQPN 100 and WQPN 28, including the following attributes:

- Have a low permeability sealed concrete pad to minimise seepage and assist cleanup of spills.
- Will be covered and weatherproofed to prevent stormwater intrusion.
- Designed with floors graded to a pit and pipe network that will be serviced by a sediment trap and oil water separator, to ensure stormwater and wastewater are managed separately from other parts of the Site.
- Be double bunded to contain water and spills within the internal drainage network.
- No fuel or combustible chemicals will be stored on-site.

On-site personnel will complete regular inspection and maintenance of the vehicle maintenance areas wastewater infrastructure to ensure they are operating as required.

Sediment from the sediment trap will be removed as required and disposed of at a registered waste facility. Any hydrocarbons removed from the oil water separator will collected and stored within appropriate sealed containers for disposal at a registered waste facility.

Spill kits will be held at the vehicle maintenance areas in the event of any hydrocarbon spill. When spill kits are used the material will be disposed of at a registered waste facility.

On-site personnel will be trained in the use and disposal of spill kits.

A separate Hydrocarbon Management Plan is included as part of the Environmental Management Plan.

5. Stormwater management plan

5.1 Overview

Stormwater management across the Site has been developed based on an understanding of the key site risks. The design of the Site and stormwater management elements has been iterative and developed with regard to key site characteristics including nature of the proposed activities, external catchment flows, steep terrain over parts of the Site, shallow groundwater conditions over parts of the Site, high surface/groundwater connectivity and downstream receptors and water users.

The key components of the Stormwater Management Plan for the site include:

- Flows that originate upstream of the site will be diverted around motorsport park infrastructure to maintain pre-development hydrology, and to keep externally generated flows separated from stormwater runoff from the motorsport park infrastructure.
- The Site has been designed to ensure key infrastructure (vehicle maintenance areas, buildings, bioretention basins) are sited outside of the modelled 1% AEP flood area (Section 2.4.7.2).
- Key stormwater management controls and best management practices have been considered for various parts of the Site infrastructure to reduce or minimise risk to surface and groundwater quality.
- Stormwater generated from areas considered to have a higher risk of discharging potential contaminants of concern (vehicle maintenance areas) will be managed separate to stormwater runoff from the remainder of the site.
- The first 15 mm of runoff generated from car parking, hardstand areas, motocross track and race track will be treated in bioretention areas.
- Runoff generated from Site buildings will be directed to rainwater tanks, with overflow infiltrated close to source or diverted to swales.

The following sections provide a further detail of the design of the stormwater management system for Stage 1A and 1B of the proposal, with Section 5.2 detailing the management of stormwater quantity and Section 5.3 detailing the management of stormwater quality.

5.2 Stormwater quantity

5.2.1 Principles and objectives

The management of stormwater quantity is proposed in accordance with the principles and objectives of the technical feasibility study (GHD, 2018), the *Stormwater Management Manual for Western Australia* (DoW, 2007); the *Decision Process for Stormwater Management in Western Australia* (DoW 2017), WQPN and the *Subdivision and Development Guidelines 2018* (CoA, 2018).

For vehicle maintenance areas (refueling, washdown and pit areas) stormwater and wastewater generated in these areas for all events up to the 1% AEP will be managed internally as detailed in Section 4.2.2. The stormwater system within this area is further described in Section 5.2.3.2. Vehicle maintenance areas will not be used during events exceeding the 10 year ARI event (10% AEP).

For all other parts of the Site the following principles apply with detail provided for Stage 1A in Section 5.2.2 and Stage 1B in 5.2.3.

1-year ARI event and smaller (1EY)

To retain and treat the 1-year ARI (1EY) event:

- Runoff from impervious areas will be managed via a range of measures including:
 - Small event runoff from impervious areas will be directed to bioretention basins for treatment, prior to infiltration where there is sufficient separation to groundwater.

- Targeted rainwater (roof water only) capture for potable (i.e. drinking) and non-potable water supply (refer Section 4.1). Overflow from rainwater tanks will be infiltrated close to source using soakage pits or infiltration galleries, or directed to swales.
- Drainage swales will be sited downstream of the tracks, conveying stormwater to bioretention basins and allowing stormwater infiltration as close to source as practical, in accordance with WSUD principles.
 Vegetation, rock weirs and/or check dams (in steep sloped areas) will slow flows and contribute to achieving WSUD objectives. Culverts will be installed to allow crossings of access tracks, carparking (where required) and racetrack pavement, with some piped sections where site topography doesn't allow overland flow.
- Direction of runoff to bioretention basins targeting peak flow management to pre-development levels, where
 possible.
- Where possible, bioretention basins are positioned to ensure 2 m vertical clearance from the maximum groundwater level. Where bioretention basins are located within 2 m vertical clearance from maximum groundwater level the base of the basin will be lined with local clay to reduce permeability, with subsoil drains installed to provide drainage function.

10-year ARI event (10% AEP)

To maintain site serviceability in the 10-year ARI (10% AEP) event:

- Drainage swales will convey stormwater to bioretention basins and will allow stormwater to be infiltrated as close to source as practical in accordance with WSUD principles. Vegetation and check dams (in steep sloped areas) will slow flows and contribute to achieving WSUD objectives. Culverts will be installed to allow crossings of access tracks and raceway pavements.
- The bioretention basins are designed to compensate peak flows to pre-development levels, and maximise opportunities for infiltration prior to discharge from the site.
- Appropriate erosion control and energy dissipation will be implemented at the outlet of piped drainage structures.

100-year ARI event (1% AEP)

To protect from flooding in the 100-year ARI (1% AEP) event:

- Key site infrastructure (vehicle maintenance areas, habitable buildings) are sited outside the 1% AEP flood area (Section 2.4.7.2). A minimum freeboard of 300 mm is provided to prevent ingress of water.
- Stormwater flows will exceed the capacity of the internal drainage swales, but will be contained within the swale freeboard, or via overload flow along roadways or grassed flow paths.
- The bioretention basins will compensate peak flows to levels that will not adversely impact the downstream
 receiving areas, and maximise opportunities for infiltration prior to discharge from the site.
- Overland flow paths are provided to minimise the potential for exposure of publicly accessible areas to flood waters.
- Basins will be designed with appropriate emergency overflow weirs and structures to ensure controlled discharge wherever possible.

5.2.2 Stage 1A

Stage 1A of the Albany Motorsport Park comprises the motocross track and 4WD driver training, ATV area and associated infrastructure. Figure 9 in Appendix A presents the proposed stormwater management plan for Stage 1A. An overview of key stormwater management infrastructure is described in the following sections. Details of the hydraulic and hydrologic modelling, including sizing of key stormwater infrastructure are provided in Section 5.2.4.

5.2.2.1 Diversion of external flows

Flood modelling of the site (Section 2.4.7.2) has identified external flows generated from the catchment of the Albany Plantation Export Company (APEC) site to the north of the Stage 1A area. Under current conditions it is assumed that stormwater runoff passes through existing culverts along Down Road West (refer Table 8), with occasional overtopping of the road in larger events and sheeting across the road verge and down into the existing valley.

It is proposed to divert flow from this external catchment via a vegetated diversion drain that traverses around the western edge of the motocross track. Culverts will be located to convey flows under the carpark area and under the motocross track where required.

A second diversion drain is sited along the central hillslope, on the eastern side of the motocross track, as a cut off drain to divert any flows from the hillslope area away from the track.

It is proposed to direct flows from the diversion drains to the central creekline along gently sloping areas. A level spreader weir is proposed to dissipate flows as sheetflow over a vegetated overland pathway. Where slopes are steep or level spreader weirs are not used, the base of swales will be rock protected and feature regular rock weirs and/or check dams to reduce velocity.

Diversion drains have been sized to manage all runoff from the external catchments in accordance with predevelopment discharge.

5.2.2.2 Refuelling and washdown area

All servicing, washdown and refuelling associated with the motocross track will be completed within the designated refuelling and washdown area. This area will be a covered concrete area with double perimeter bund and internally draining pit and pipe network. The pit and pipes will direct all water to a sediment trap and an oil water separator, as described in Section 4.2.2.

Treated water from the oil water separator will be directed into the stormwater drainage system.

5.2.2.3 Access road and carpark

In small runoff events stormwater runoff generated from the access roads and carparks will be directed towards distributed bioretention basins to treat stormwater, and infiltrate where possible. Flow in excess of the capacity of the bioretention basins will connect to surface drainage (e.g. diversion drain, swale drainage).

5.2.2.4 Motocross track

The motocross track is sited across the northern valley of the Site. Fill sourced from the Site is used to provide adequate separation (\geq 2.0 m) of the track from the maximum groundwater level. The track is constructed using locally sourced sandy/clay. Refer to the motocross track drawings (plan and longitudinal sections in Appendix F).

Stormwater runoff from the motocross track is directed to a series of vegetated drainage swales that capture and convey stormwater flows to distributed bioretention basins.

Swale dimensions are summarised in Section 5.2.4.

5.2.2.5 4WD driver training and ATV area

The location of the 4WD driver training and ATV area has been identified as a local source of sand/clay and gravel, which will be used for the construction of the motocross track, access road, carparking areas and race track at the Site.

Following removal of sand/clay and gravel the 4WD driver training and ATV area will comprise the natural surface. No formal stormwater management is proposed in this area. Stormwater runoff from this area will be directed to a bioretention basin at the natural low point to aid settling of sediment, with flow in excess of the bioretention basin volume directed via a vegetated overland flowpath towards the central creekline.

5.2.3 Stage 1B

Stage 1B of the Albany Motorsport Park comprises the race track and associated infrastructure. Figure 10 in Appendix A presents the proposed stormwater management plan for Stage 1B. An overview of key stormwater management infrastructure is described in the following sections. Details of the hydraulic and hydrologic modelling, including sizing of key stormwater infrastructure are provided in Section 5.2.4.

5.2.3.1 Diversion of external flows

Flood modelling of the site (Section 2.4.7.2) has identified external flows generated from the north-east catchment, with flows crossing Down Road West from the APEC site to the north, the CBH Mirambeena site to the north-east, and agricultural land to the east of the Stage 1B area.

Flows from part of the northern part of this external catchment accumulate in a roadside drain on the north side of Down Road West, and flow via a culvert (1050 mm dia.) under Down Road West to the Site. External flows originating along the northern boundary of Stage 1B will follow their natural flowpaths with minor culvert crossings (300 mm culvert) provided under access roads where required. A culvert crossing of the Down Road West roadside drain will be provided at the entry to the Site.

External flow originating from the eastern agricultural land will follow its natural flowpath, with minor culvert crossings provided under the access road and race track where required. This diversion drain will also receive some race track stormwater runoff, and flows will be directed to a bioretention basin prior to discharge from the Site.

The flows originating from the north-east (CBH site) will be diverted around the race track using a cut off drain, with minor culvert crossings provided under the access road and race track where required.

Where slopes are steep or level spreader weirs are not used, the base of swales shall be rock protected and feature regular rock weirs and/or check dams to reduce velocity and provide water treatment.

Diversion drains are sized to manage all runoff from the external catchments in accordance with predevelopment discharge.

5.2.3.2 Pit area

All servicing, washdown and refuelling associated with the race track will be completed within the designated pit area. The pit area will be covered and weatherproofed to prevent stormwater intrusion, with an impervious perimeter bund and floors graded to an internally draining pit and pipe network. The pit and pipe drainage network in this area may comprise perimeter trench drains with trafficable covers located within the perimeter bund to prevent egress of any surface water drainage or spills generated within this area.

The pit and pipe drainage network will direct all water to a sediment trap and an oil water separator, as described in Section 4.2.2. Treated water from the oil water separator will be directed into the stormwater drainage system.

5.2.3.3 Access road, spectator carpark, competitor carpark and emergency muster area

Runoff from these areas will be managed as follows:

- Access roads and tracks stormwater runoff generated from the access roads will drain to vegetated areas alongside the roads. Where this cannot occur, roadside drains will be implemented which will feature regularly spaced rock weirs/check dams to slow flows and promote sedimentation. Where required, suitable culvert pipes or overflow points either under the roadway or over the roadway will be provided to target controlled discharge to the surrounding environment.
- Spectator carpark small event stormwater runoff generated from carpark area will be directed towards the bioretention swales distributed throughout the carpark. These will be connected via minor culverts under the carpark to the adjacent drainage swales.
- Competitor parking and marshalling area it is proposed that the emergency muster area will feature a crest to direct stormwater runoff to vegetated swale drains located around the perimeter of the competitor carpark and marshalling area. The southern and eastern portions of the carpark and emergency muster area will be

designed to direct flows to a bioretention basin in the south-east corner of the Site. The north-western portion of the carpark and emergency muster area will divert flows to drainage swales and bioretention basins located to the north and south of the Pit area.

5.2.3.4 Race track

Runoff from the race track is designed to capture and convey stormwater flows in a series of shallow vegetated swales (1V:6H) sited downstream of race track cross-fall (assumed on inside of corners). The shallow vegetated swales will feature regularly spaced interceptor traps, and will convey flows to bioretention basins.

5.2.4 Hydrologic and hydraulic assessment

Sizing of key stormwater infrastructure for Stage 1A and Stage 1B including diversion drains, swales and bioretention basins was completed through development of a post-development hydrologic and hydraulic model, using inputs from the existing site hydrology (Section 2.4.7) and the Site infrastructure plans (Figure 2 in Appendix A).

5.2.4.1 Diversion drains

Design of the diversion drains is based on the following:

- Where space and topography permit the drainage swales will be broad and shallow. Side slopes of 1V:6H are proposed to ensure safe vehicle run-off in proximity to the motocross track and race track, as well as ease of maintenance.
- Maximum side slopes of 1V:3H may be required in areas restricted by space or topography.
- Diversion drains will have a freeboard of 0.3 m (over the 10% AEP design event level) to allow additional storage and conveyance to distributed bioretention basins.
- Drains with typical slopes that are greater than 3% longitudinal grade will require erosion protection surfacing either in the form of rock lining or other similar measures.

Typical diversion drain dimensions are summarised in Table 9. Further information on drains with similar requirements are detailed on Figure 9 and Figure 10.

Swale example	Shape and side slope (V/H)	Average slope (%)	Max depth* (m)	Length (m)	10% AEP flow (m³/s)			
Stage 1A								
W-EXT02	1:6 swale	0.38	0.542	140	0.172			
W-EXT04	1:6 swale	1.56	1.423	100	0.186			
Stage 1B	Stage 1B							
E-B9-07	1:4 swale	1.64	0.781	350	0.072			
E-B9-08	1:4 swale	0.94	0.781	120	0.024			

Table 9	Diversion drain	n dimensions

* The max. depth is driven by providing adequate freeboard for the 10% AEP event while also considering the depths in the 1% AEP event. The depth varies along the drain and would generally increase from a minimum depth of 300 mm at the upstream end, unless receiving water from upstream drains or culverts.

5.2.4.2 Drainage swales

Design of the drainage swales is based on the following:

Where space and topography permit the drainage swales will be broad and shallow. Side slopes of 1V:6H are proposed to ensure safe vehicle run-off in proximity to the motocross track and race track, as well as ease of maintenance.

- Maximum side slopes of 1V:3H may be required in areas restricted by space or topography.
- Drainage swales will have a freeboard of 0.3 m (over the 10% AEP design event level) to allow additional storage and conveyance to distributed bioretention basins.
- Drains with typical slopes that are greater than 3% longitudinal grade will require erosion protection surfacing either in the form of rock lining or other similar measures.

Key swale dimensions are summarised in Table 10, while the modelling results for each swale drain are contained in Appendix G.

Swale example	Shape and side slope (V/H)	Average slope (%)	Max depth*** (m)	Length (m)	10% AEP flow (m³/s)
Stage 1A					
W-B4-01	1:6 swale	1.80	0.909	170	0.088
W-B4-02	1:6 swale	4.81	0.909	200	0.110
W-B5-04	1:6 swale	3.00	0.811	40	0.188
W-B5-05	1:6 swale	4.89	0.798	45	0.018
W-S1	1:6 swale	5.07	0.478	300	0.265
Stage 1B					
E-B4-01*	K300**, 0.4 m deep	0.50	0.57	150	0.090
E-B4-02	1:4 swale	0.90	0.586	220	0.248
E-B6-01	1:6 swale	3.87	0.699	150	0.094
E-B9-01	1:6 swale	3.60	0.447	160	0.129

Table 10 Swale dimensions

* Further development in detail design will likely require a pit and pipe system to be installed in combination with this trench drain.

** K300 is an assumed 300 mm wide with varying depth Class D Covered Trench Drain

*** The max. depth is driven by providing adequate freeboard for the 10% AEP event while also considering the depths in the 1% AEP event. The depth varies along the drain and would generally increase from a minimum depth of 300 mm at the upstream end, unless receiving water from upstream drains or culverts.

5.2.4.3 Culverts

Different crossing locations were determined to manage discharge to the surrounding environment. Preliminary sizing of proposed culverts was done using DRAINS software and results are shown in Table 11. Further assessment of these culverts are suggested in future design stages to determine structural suitability, should there be reduced cover as limited by resulting earthworks.

Culverts	Length (m)	Slope (%)	No. of barrels	Diam (mm)
Stage 1A				
W-B1-CULV1	30	1.17	1	450
W-B5-CULV1	13	2.00	1	450
W-B5-CULV2	12.5	3.00	1	450
W-B5-CULV3	19.2	1.56	2	450
W-B5-CULV4	14.5	2.76	1	450

Table 11 Culvert dimensions

Culverts	Length (m)	Slope (%)	No. of barrels	Diam (mm)
W-B5-CULV5	12.6	7.06	1	450
W-B5-CULV6	20	1.00	1	450
W-EXT-CULV	150	2.13	1	450
W-EXT-CULV1	20	0.50	1	450
Stage 1B				
E-B5-CULV1	15	6.07	1	450
E-B7-CULV1	55.2	2.55	1	450
E-B7-CULV2	13.4	3.06	1	450
E-B7-CULV3	97.1	0.50	1	450
E-B9-CULV1	13.7	7.30	1	450
E-B9-CULV2	28.3	3.22	1	450
E-B9-CULV3	49	1.86	1	450

5.2.4.4 Bioretention basins

A series of shallow distributed bioretention basins are sited to provide both water quality treatment as well as stormwater compensation/detention/infiltration throughout the Site.

The bioretention basins are sized such that the total post-development flow off the site was equal to or less than the pre-development flow for the minor (10% AEP) design event and targeted appropriate compensation and management of major storms (i.e. the 1% AEP or 100 year ARI). Bioretention basin parameters included:

- Sited outside the 1% AEP event from the major creek through the site.
- Construction should use the natural topography of the Site where possible.
- Basin base levels set to be 2 m above the assumed groundwater level when used for infiltration. If within 2 m of the groundwater the base of the basin is to be lined to prevent infiltration; these basins will require the implementation of a subsoil drainage system.
- Basins equipped with low flow outlet/s (pipe/orifice), high flow bypass pit and a mortared/rock protected overflow spillway that has sufficient capacity to handle 1% AEP flow, where possible.
- Nominal depths ranging from 0.35 m to 1.2 m to spillway levels; and 0.5 m to 1.5 m to top of wall.
- 1V:6H side slopes where space permits to allow for vegetation to stabilise side slopes and reduce erosion risk. Where geotechnical conditions permit, basin side slopes may be increased a max. of 1V:3H to facilitate increased base infiltration surface (may require fencing and/or signage for safety where fencing is not appropriate).
- An average 2 m/day infiltration rate has assumed, noting that testing has found varying rates of between 0.41 and 3.29 m/day across the site. Detailed design of each basin should be informed by the site-specific permeability test results in Appendix B.
- Bioretention basins feature a low flow piped discharge, designed to be:
 - Set above the peak 1EY basin water level, such that no discharge occurs for water quality management, where possible (basins requiring lining will need to discharge the 1EY event).
 - Set and sized so as to ensure that the basin overflow spillway does not activate in events up to and including the 10% AEP.
 - Contributing catchments would be directed into each of the basins as detailed in Section 5.2.2 and Section 5.2.3.
- Post development flows are those of the combined catchment areas that contribute to the basin location and are shown in Appendix G.
- The results of the bioretention basin sizing for Stage 1A and Stage 1B are summarised in Table 12.

Table 12 Bioretention basin sizing *

Basin	Slope (1V:_H)	Base Elevation (m)	Base Area (m²)	Top Elevation (m)	Top Surface Area (m ²)	Depth (m)	Max Volume (m³)	By-pass level (m)	Low Flow Outlet	Overflow weir level (m)
Stage 1A										
West-B1	3	66.0	90	67.0	265	1.0	170	66.60	N/A	66.75
West-B2	6	62.0	150	62.5	640	0.5	180	62.35	3 x 70	62.35
West-B3	3	62.5	160	64.0	475	1.5	450	63.20	N/A	63.70
West-B4	6	59.0	100	60.5	450	1.5	400	59.50	2 x 70, 1 x 100	59.60
West-B5	3	53.5	105	54.5	260	1.0	175	54.00	3 x 90	54.25
West-B6	6	58.0	100	59.0	500	1.0	275	58.50	N/A	58.75
West-B7	3	51.5	430	52.5	980	1.0	700	52.20	3 x 70	52.50
Stage 1B										
East-B1	6	58.0	145	59.5	950	1.5	750	58.75	1 x 90	59.50
East-B2	6	57.0	500	58.0	1150	1.0	800	57.50	1 x 90	57.75
East-B3	6	70.0	350	71	950	1.0	625	70.60	3 x 100	71.00
East-B4	6	71.0	250	71.5	550	0.5	200	71.25	N/A	71.38
East-B5	6	66.0	300	67.5	1300	1.5	1100	67.00	2 x 80, 1 x 100	67.20
East-B6	6	61.0	600	61.5	1000	0.5	400	61.20	3 x 90	61.50
East-B7	6	65.0	300	66.0	850	1.0	550	65.50	180, 1 x 90, 1 x 90	65.75
East-B8	6	70.5	250	71.5	750	1.0	475	71.00	N/A	71.25
East-B9	6	63.0	950	64.0	1800	1.0	1350	63.50	N/A	64.00
East-B10	6	62.0	430	62.5	800	0.5	300	62.25	3 x 110	62.50

* The levels detailed in the above table are subject to change during detailed design however base areas and volumes will need to be generally achieved.

5.2.5 Pre- and post-development discharge

The outlet locations to the downstream watercourse were determined, and the contributing catchments from Stage 1 works assessed for the treatment and management of stormwater runoff within the site. Due to the proposed layout of the tracks, minor changes in catchment areas were present when comparing both predevelopment and post-development scenarios. A summary of this comparison is shown in Table 13.

All outlet locations on Stage 1B are shown discharging on a 1EY event and must be treated within the basin prior to discharge, to mitigate any adverse water quality outcomes. The modelling determined it is impractical to manage some flows to below pre-development discharge (i.e. East-3 and East 4) for the 10% AEP. However overall the post-development discharge from all eastern catchments is below pre-development discharge. For the western catchments, the total post-development discharge is only 0.007 m³/s above pre-development, which is only 1.5% and considered insignificant.

Discharge	Pre-develo	Pre-development flows (m3/s)				Post Development flows (m3/s)				
location	Area (ha)	1EY	10% AEP	1% AEP	Area (ha)	1EY	10% AEP	1% AEP		
Stage 1A	Stage 1A									
West-1	14.10	0	0.270	1.64	14.10	0	0.263	1.600		
West-2	11.17	0	0.214	1.36	6.86	0	0.132	0.286		
*West-3	*	*	*	*	4.31	0.013	0.096	0.498		
TOTAL	25.27	0	0.484	3.00	25.27	0.013	0.491	2.384		
Stage 1B										
East-1	12.13	0	0.244	1.58	11.04	0.020	0.158	0.450		
East-2	13.30	0	0.296	1.83	15.53	0.016	0.290	1.080		
East-3	9.76	0	0.177	1.06	10.28	0.031	0.193	0.919		
East-4	7.35	0	0.118	0.65	5.72	0.021	0.174	0.494		
TOTAL	42.54	0	0.835	5.12	42.57	0.088	0.815	2.943		

Table 13 Combined site discharge

*additional outlet location taken from West-2

5.3 Stormwater quality

5.3.1 Overview

The hydrogeological conceptual model (Appendix D) indicates high surface/ groundwater connectivity within the Site, with potential for impacted groundwater to migrate towards the creekline and off-site towards the major drainage in the area, the Marbelup Brook. If not responsibly managed, the development has the potential to negatively affect stormwater quality discharging from the catchment and impact on the potential receptors and water users.

Based on the proposed site activities the key stormwater quality issues requiring management include:

- Sediment load: Erosion caused by high flow velocity can result in a loss of soil, damage to drainage swales, and increased sediment load to the receiving water body.
- Nutrient load: Increased nutrient loading to the receiving water body may result from over- application of fertilisers to landscaped areas.
- Gross pollutants: Suspended and dissolved pollutants, and rubbish.
- Toxicants: Key pollutants associated with motor sport facilities include leaks and spills of chemical or petroleum hydrocarbons from vehicle maintenance areas, hydrocarbon storage areas and racetracks. Other potential toxicants of concern include dissolved metals and pesticides.

5.3.2 Best management practices

Management of stormwater quality is focused on providing appropriate treatment of stormwater runoff generated by the various parts of the Site based on an understanding of the key site risks. A range of key controls and best management practice WSUD elements will be utilised to manage stormwater quality across the site.

Best management practices (BMPs) are design strategies targeted to manage total suspended solids, gross pollutants, nutrients (TP and TN) within stormwater discharged from urban catchments (DoW, 2007). Frequently occurring rainfall events are targeted, using source, in-transit and end-of-pipe controls to improve water quality. BMPs considered appropriate for the Site include:

- The Site stormwater drainage system has been designed to separate good quality stormwater from potentially contaminated stormwater.
- Flows generated from external catchments will be diverted around the Site infrastructure, with external drainage separated from Site drainage where possible.
- Stormwater runoff from hydrocarbon-impacted areas including the refuelling and washdown area (Stage 1A) and pit (Stage 1B) will be isolated from stormwater generated for other parts of the Site. These areas are covered, double bunded, with internal stormwater pit and pipe network connected to sediment trap and oil water separator.
- Maximising infiltration by adopting a stormwater retention system to contain, and as a minimum, treat the first 15 mm of rainfall on site.
- Flows generated from Site buildings are considered to be uncontaminated and will be diverted to rainwater tanks for reuse as discussed in Section 4.1.1, or infiltrated at source.
- Use of suitable soils within swales and compensation basins that target the uptake of nutrients.
- Construction of combined bioretention and compensation basins to allow water quality treatment of small events (including metals and hydrocarbons), encourage infiltration and reduce peak flow rates.
- Swale drains shall be planted with grass for filtering of particulates and uptake of dissolved nutrients. Grass
 will be mowed with clippings removed from site.
- Additional sediment management measures include regularly spaced interceptor traps on swale drains, with check dams and rock protection used on steeper slopes where required.
- First-flush diversion will be installed for the pit area as well as the adjacent extensive hardstand area of the competitor parking and marshalling area, to capture initial stormwater run-off after an extended dry period.

5.3.3 Spill control and pollution management

To achieve spill control and pollution management in the high risk areas of the AMP, the following practices from WQPN 28: *Mechanical workshops and servicing* (DoW, 2013), *WQPN 52: Stormwater management at industrial sites* (DoW, 2006) and *WQPN 100: Motor sport facilities near sensitive waters* (DoW, 2007) will be implemented:

- Separation of uncontaminated stormwater from potentially contaminated stormwater (particularly roof water from other trafficked hardstands).
- Fuel / chemical handling areas (i.e. pits and maintenance areas) shall be located within secondary containment areas that allow maximum recovery of any spilt materials.
- Paved areas exposed to rainfall where dust, litter or spilt substances accumulate will be regularly cleaned by AMV Inc. personnel with methods that prevent fluid drainage or leaching into the surrounding environment.
- Oil and sediment traps (as appropriate to the site) will be installed at vehicle maintenance areas, and managed by AMV Inc. personnel (Section 4.2.2). First-flush water diversion to be installed for the pit area as well as the adjacent extensive hardstand area of the competitor parking and marshalling area to capture initial stormwater run-off after any extended dry period.
- Wash down of vehicles to occur in vehicle maintenance areas only. These areas feature a bunded impervious pad that is weatherproof to minimise stormwater access. Chemical solvents and non-degradable detergents used to clean equipment or pavements should not be released into stormwater systems. High pressure, steam cleaning, scrubbing or quick break detergents are the preferred methods of cleaning vehicles.

Spill kits (permanent and mobile) will be located throughout the Site, comprising absorbent materials. AMV Inc. personnel will have necessary training on the handling of, and disposal of, hydrocarbons and spill kits. Any fuel/ chemical spills will be contained and remediated in accordance with the management strategies and actions outlined in the Hydrocarbon Management Plan prepared for the Site (GHD, 2021).

Water contamination barriers

The following water contamination barriers are proposed, to prevent any loss of hydrocarbons and chemicals from the site:

- A 50 m grassed buffer (Development Exclusion Buffer) from the unnamed watercourse and Conservation Class wetland.
- A 200 m buffer from the unnamed water course and Conservation Class wetland to vehicle maintenance areas (as per DoW WQPN 100).

No permanent fuel, oil or chemical storage will occur on the Site. Temporary storage of fuel, oil and chemical solvents within the Site will occur within the bunded vehicle maintenance areas / pits.

- Covered, double bunded impervious vehicle maintenance areas with spill controls in place for hydrocarbon management. Runoff from these areas will be internally draining to a pit and pipe network connected to treatment devices including a sediment trap and pol water separator. Treated water shall outlet to the Site drainage network of swales and bioretention basins. Wastes and oily residue will be disposed to an approved off-site location (Section 4.2.2).
- Interceptor traps shall be installed and maintained throughout the swale network for treatment of track stormwater runoff.

It is noted that a swale exists within 200 m of the vehicle pits in the south-east of the site. Whilst water conveyance through the swale will improve water quality when compared to piped conveyance, it can also be considered a direct connection to the watercourse. It is proposed that all runoff from the pits and maintenance areas in this location should pass through an oil/water separator to remove contaminants before they enter the watercourse. Furthermore, the runoff from this area will pass through a compensating basin before entering the watercourse. This retarding effect on the runoff will allow a chance for the contaminants to settle and/or break down.

5.3.4 Emergency response plan

In the event of a vehicle crash and/or fire, first response extinguishment will be via standard, portable dry chemical fire extinguishers (ABE type). The multipurpose ABE powder is a versatile extinguishant, which is used to extinguish Class A (carbonaceous), Class B (flammable liquid) and Class E (electrical) fires. When dry, the powder may be cleaned up with a vacuum cleaner, or similar. No larger firefighting apparatus are proposed for the AMP, and no firefighting foams are proposed.

As part of Motorsports Australia Regulations, each flag point (attended by a trained marshal) on a racetrack is required to have 2 × 9 kg fire extinguishers available. The AMP racetrack will likely have 5-6 flag points.

In the case of an emergency in the high risk areas of the AMP, the following actions from WQPN 100: Motor sport facilities near sensitive waters (DoW, 2007) will be implemented:

- A contingency plan shall be developed before the operational phase and be available on the Site in order to address emergency situations such as accidents, fires and chemical spills that could put local water resources including surface water and groundwater at risk. Relevant AMV Inc. personnel and contractors shall be familiar with the Site emergency response procedures.
- During larger events (potentially up to 20,000 for national race events), adequate emergency response services (e.g. firefighting, security, communications, medical personnel and emergency vehicle access) shall be provided.
- Portable spill kits and containment booms (land socks or similar) shall be kept at various locations, including flag points within the Site with absorbent material to soak up spilt oil, chemicals and/or fuel. Additionally, sand bags or coir logs will be used in the case of a vehicle accident to block flow to drains.

 The plan should be submitted to Water Corporation, City of Albany and Department of Fire and Emergency Services for advice before implementing.

5.3.5 Non-structural measures

There are a number of temporary and non-structural measures are also key management measures for the development and operation of the Site.

Construction

Construction sites can be a major source of silt and other pollutants. Proponents and builders shall be encouraged to undertake good practice on building sites through preparation of a site-specific Construction Environmental Management Plan (Section 6).

A separate Construction Management Plan is also included the in the AMP Environmental Management Plan.

Maintenance

Regular maintenance of the Site drainage system shall be undertaken prior to the start of the wet season. Cleaning of the drainage system, including base of swale drains, interceptor traps in swale drains and bioretention basins will provide an opportunity to remove gross pollutants and silt build up that may enter the receiving water bodies after heavy rainfall. Any vegetation disturbed in the swales and bioretention basins will be re-established to ensure water quality treatment.

In addition to transporting pollutants, drains with accumulated pollutants may also overflow, leading to localised flooding and erosion, and risks to human safety and constructed assets. Maintenance may also include erosion control measures such as rock pitching if required.

Revegetation and landscape management

- Revegetation of the Protected Exclusion Area (Figure 2), which encompasses the Conservation Class wetland and creek line, shall be undertaken as part of the development. Revegetation shall comprise suitable wetland species identified by Bio Diverse Solutions (2019), including Unit 13, Unit 47 and Unit 49 from the *Albany Regional Vegetation Survey Extent* (Sandiford & Barrett, 2010). The proposed native wetland revegetation species will assist in uptake of nutrients and trap sediment in surface runoff and shallow groundwater discharging to the wetland area. These native species include *Baumea juncea* and *Baumea rubiginosa* which are frequently used in bioretention areas for their nutrient uptake abilities.
- A 50 m wide, low fuel 'Development Exclusion Buffer' comprising a managed grass area will provide a further buffer for stormwater runoff from the development, and any overflow from bioretention basins. The managed grass buffer will assist to filter and trap sediments and nutrients in overland flow discharged to the unnamed creek line / wetland.
- Use of pesticides and fertilisers shall be limited, and completely excluded within the Protected Exclusion Area and Development Exclusion Buffer. Refer to the Protected Exclusion Area Management Plan in the AMP Environmental Management Plan. Use of herbicides shall be in accordance with the Use of herbicides in water catchment areas (Circular No: PSCBB, Department of Health).

Erosion and sediment control

A range of measures will be implemented throughout the Site to minimise erosion and prevent sediment loss from the Site impacting on downstream receptors. Erosion and sediment control measures during construction are detailed in Section 6.

During operation of the Site the erosion and sediment control measures include:

- Sediment traps installed in vehicle maintenance areas.
- Drainage swales that convey stormwater runoff will be vegetated with grass to promote sedimentation and feature regularly spaced interceptor traps.
- The base of drainage swales and diversion drains in higher slope areas will be rock protected and feature regular rock weirs and/or check dams to reduce flow velocity.

6. Construction management

Potential impacts to water resources during construction activities include:

- Soil erosion construction would result in the exposure of the natural ground surface and subsurface through the removal of vegetation, and excavation and landforming works within the Site which may increase the potential for soil erosion to occur. There is further potential for mobilisation of dust associated with the construction works.
- Surface water quality construction of the project has the potential to impact surface water quality through the pollution of runoff with sediments, fuel and other hazardous materials from the construction site.
- Disturbance of acid sulfate soils potential for construction activities to disturb acid sulfate soils.

6.1 Construction Environmental Management Plan

The AMP Environmental Management Plan includes a specific Construction Management Plan, which outlines objectives, broad strategies and actions required to minimise environmental impacts associated with construction of the AMP. The Construction Management Plan applies to the GSMG and all appointed contractors during the construction of the AMP.

It is recommended that a site-specific Construction Environmental Management Plan (CEMP) be prepared for the Site that addresses the management of construction works to ensure no detrimental impacts to the receptors. The CEMP should be referred to DWER for approval. The CEMP shall be maintained during the construction period and Site establishment period and include:

- Temporary bunds, coir logs and silt fences to prevent silt runoff into the drainage system
- Litter and waste storage bins to prevent litter to be blown by wind or washed by rainfall
- Establishing a washing-down area behind the bund or silt fence
- Provide a stabilised entry and exit point to prevent vehicle tracking of soil from the building site onto roads
- Position stockpiles of sand and soil stockpiles to prevent material being tracked, washed, of blown into roads, and then into existing surface drainage or constructed stormwater systems.

6.2 Acid Sulfate Soil Management Plan

Surface and/ or groundwater may also become contaminated through the exposure of ASS during construction (excavation). ASS disturbance may have a range of impacts including enhanced phosphorus leaching, death of vegetation irrigated with affected water, the smothering of benthic aquatic animals by the precipitation of iron, and metal bioaccumulation in aquatic plants and animals. However, based on the ASS assessments to date (refer to Section 2.3.3), inorganic sulfidic sources capable of rapid acid release upon disturbance were not observed. Other, more slow releasing acidity sources were observed in the ASS assessment and will require management if disturbed in volumes greater than 100 m³.

The following ASS management recommendations are made with regards to the proposed redevelopment:

- Topsoil (0-300 mm) appears acceptable to be stripped and stockpiled for reuse without treatment (pH on average above 4 across the site).
- Neutralisation treatment and validation of soils <u>will be required</u> for silty sand soil units disturbed in the proximity of the watercourse area given that there are exceedances of the DWER action criteria (coarse textured soils) and if the proposed disturbance of greater than 100 m³ of soil.
- An ASS management plan will be required (in accordance with DWER guidelines) to enable to the effective excavation, treatment and disposal/reuse of the materials during construction works.
- Soil excavations should only occur during the periods of the year where groundwater is at its lowest point (i.e. outside of winter and post-winter periods) to eliminate the need for temporarily lowering the groundwater table (dewatering). If dewatering is determined to be required, then site specific dewatering risk assessment, management strategies and criteria are required to be developed, approved and implemented.

7. Monitoring

7.1 Monitoring requirements

The objective of the surface water and groundwater monitoring is to assess the operation of the Site against the design criteria (Section 3) and baseline water quality (Section 2.4.5).

Monthly monitoring of surface and groundwater conditions will be completed during the construction and operational period. The monitoring data will be compared to baseline data (Section 2.4.5) to ensure no adverse impacts from construction and operation of the Site on the surface water and groundwater quality and levels.

Event based monitoring will be completed at key locations of drainage infrastructure (bioretention basins) to assess stormwater drainage performance in improving stormwater quality. It is assumed the first flush events will have the highest level of nutrients and chemicals, therefore sampling should occur at the time/after the first significant rainfall event of each wet season, and after extended dry periods. Field notes should include details of the rainfall events, site conditions, time of sampling and time of sample testing.

Additional sampling should also be undertaken in response to any spill events.

A summary of the proposed surface water monitoring program is provided in Table 14. The proposed groundwater monitoring program is provided in Table 15, and the groundwater monitoring sites are shown on Figure 6.

Site	Frequency	Duration	Parameters
Surface water	Monthly	On-	In-situ: pH, EC, temperature
- Upstream of the site (TBC)		going,	
- Mid-stream (CS02)		with annual	Unfiltered sample: pH, EC, TN, FRP,
- Downstream of the site (CS01)		reporting	TKN, ammonia, TP, TRH, PAH, BTEXN, surfactants, microbial analysis
Compensating basin	3-4 events per		
- Inlet (6 No.) and Outlet (6 No.)	year following		Filtered sample: Filtered total nitrogen
West-B1	1EY rainfall events or		and filtered total phosphorus (to
West–B7	greater		quantify organic component),
East-B3			NO ₂ /NO ₃ , PO ₄ , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)
East-B5			(, , , , , , , , , , , , , , , , , , ,
East-B6			
East-B10			
Sub-catchment Inlets and Outlets			
West 1 Outlet Only (4WD training area)			
West 3 (DS Culvert W-EXT-CULV & DS Culvert W-CULV1)			
East 3 Outlet			
East 1 Outlet (DS of East-E9)			

Table 14: Summary of surface water monitoring

Table 15: Summary of groundwater monitoring program

Site	Frequency	Duration	Parameters
Monitoring bores	Monthly	On-going,	Water level
(up to 6 bores across the site locations to be confirmed)		with annual reporting	In-situ: pH, EC, temperature
To include SB04, SB03, SB08, SB09 and 2 others			Unfiltered sample: pH, EC, TN, FRP, TKN, ammonia, TP,
Production bore/s (location to be confirmed)			TRH, PAH, BTEXN, surfactants, microbial analysis
to be commed)			Filtered sample: Filtered total nitrogen and filtered total phosphorus (to quantify organic component), NO ₂ /NO ₃ , PO ₄ , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)

7.2 Quality assurance and quality control

A surface and groundwater monitoring plan will be prepared to support ongoing monitoring of the Site for submission and approval by DWER and Water Corporation.

Monitoring will be completed in accordance with the requirements of the *Australian and New Zealand guidelines for fresh and marine water quality* (ANZECC, 2018). Sample collection, processing, transportation, storage, preservation and labelling of water samples will be conducted in accordance with the appropriate industry standards and general water sampling guidance (AS/NZS 5667.1:1998), with collected samples analysed in a NATA accredited laboratory.

Post-development, permanent groundwater monitoring bore locations and sites should be identified and constructed in accordance with industry standards (ASTM D5092/ D5092-16, *Standard practice for design and installation of groundwater monitoring bores*).

7.3 Contingency plan

Should monitoring of groundwater and/ or surface water identify that water quality objectives are not being met the following contingency measures will be implemented:

- Investigate the source or cause of elevated contaminants through site investigation and/or additional monitoring if required.
- Review installation of stormwater management BMPs to ensure they are designed, installed and maintained as required.
- Review implementation of Site procedures for incident management to ensure appropriate measures are undertaken to respond to incidents such as spills and accidents.
- Should further monitoring identify that water quality objectives are not being met, AMV Inc. will notify DWER and the City of Albany to determine requirements further site investigation or remediation actions.

A water quality response and contingency plan will be developed in consultation with the Water Corporation, City of Albany and DWER. The water quality response and contingency plan shall be included in the surface and groundwater monitoring plan.

7.4 Reporting

The AMV Inc. will prepare an annual water quality monitoring report for submission to the DWER and Water Corporation. The annual water monitoring report will summarise surface water and groundwater monitoring results for the calendar year, including comparison to baseline data and previous years of monitoring. The annual report will include summary reporting of any water quality exceedance, including parameters exceeding water quality objectives, measures taken to investigate exceedances, results of additional monitoring and any further actions undertaken.

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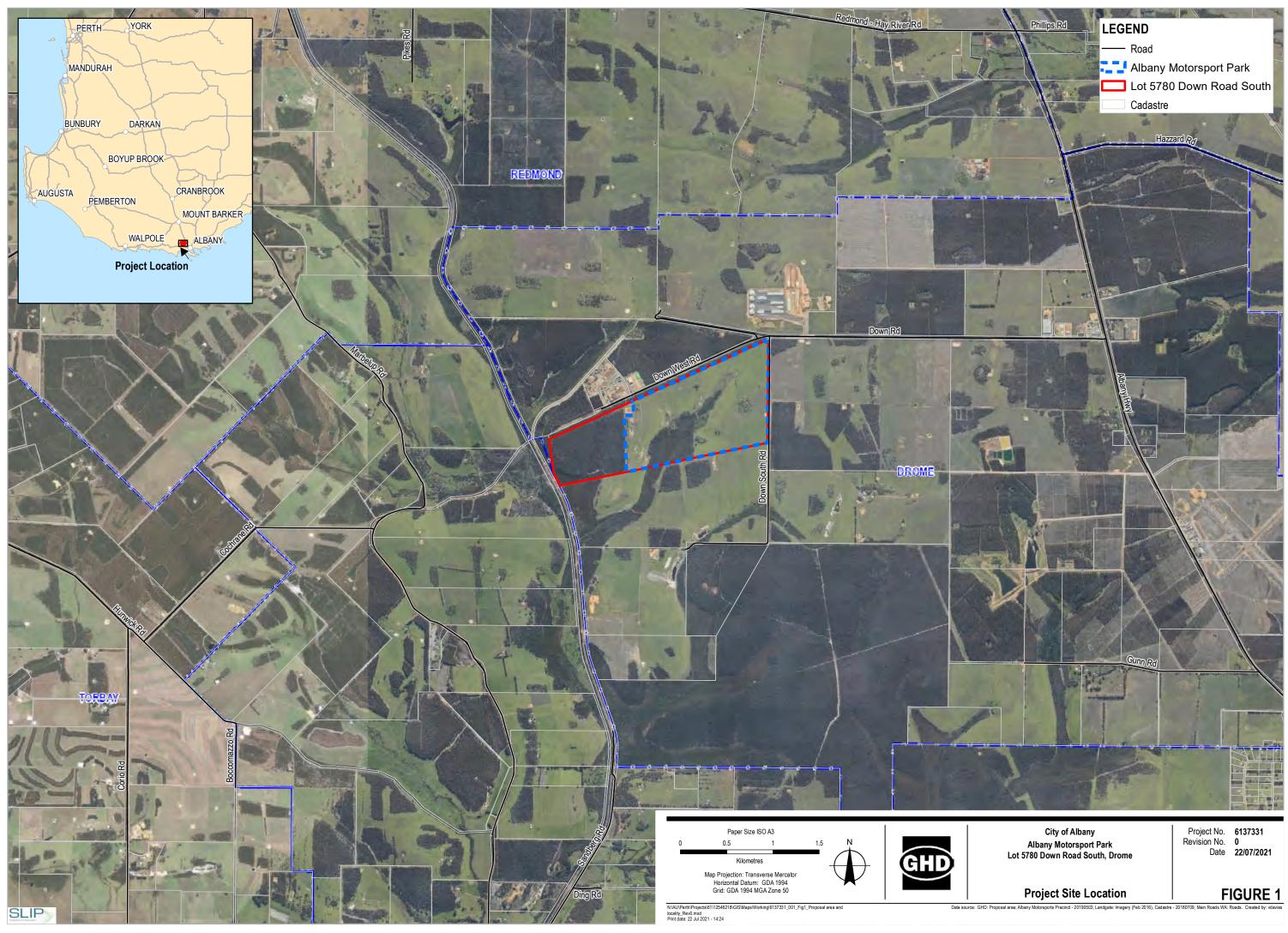
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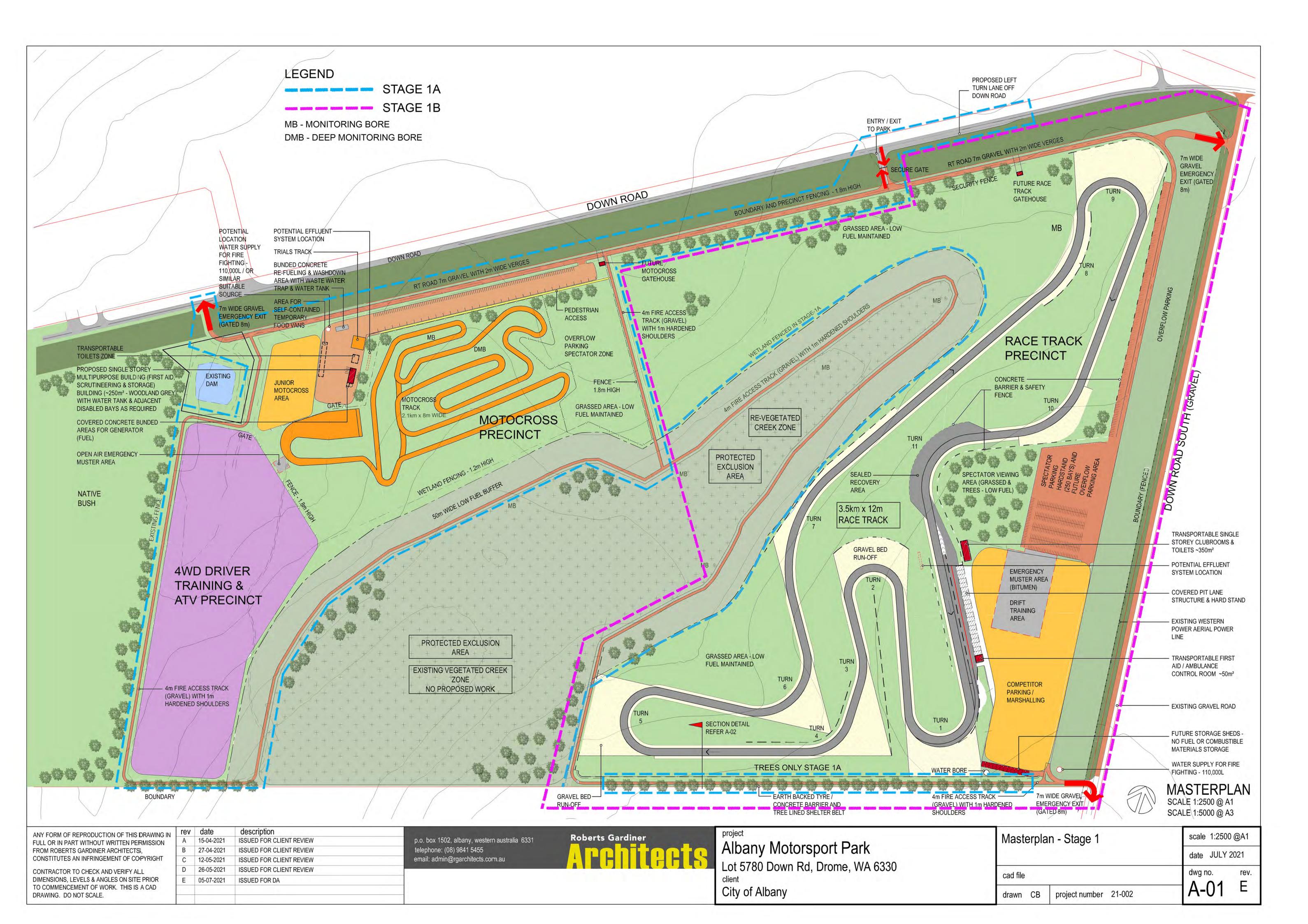
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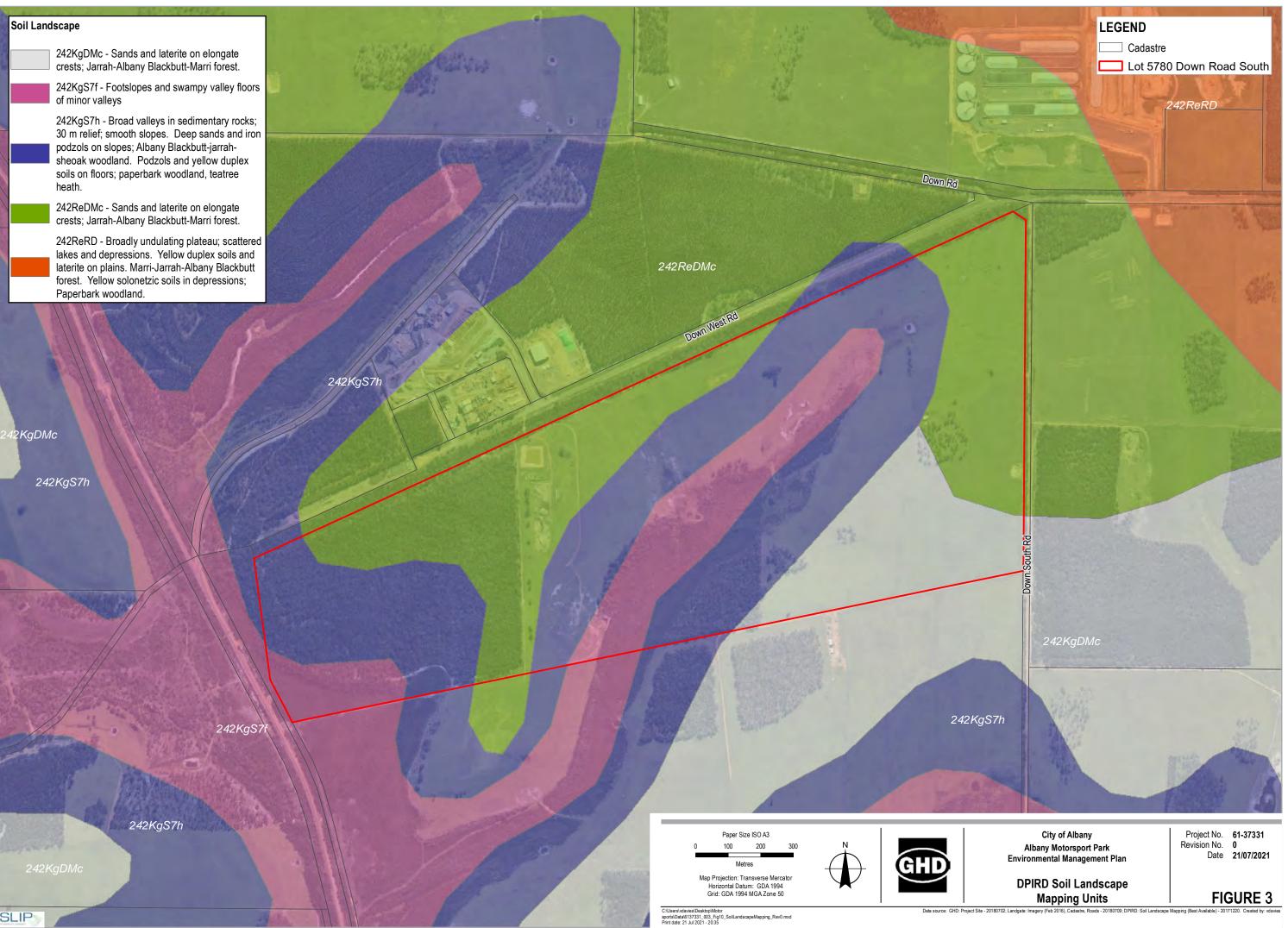
Appendices

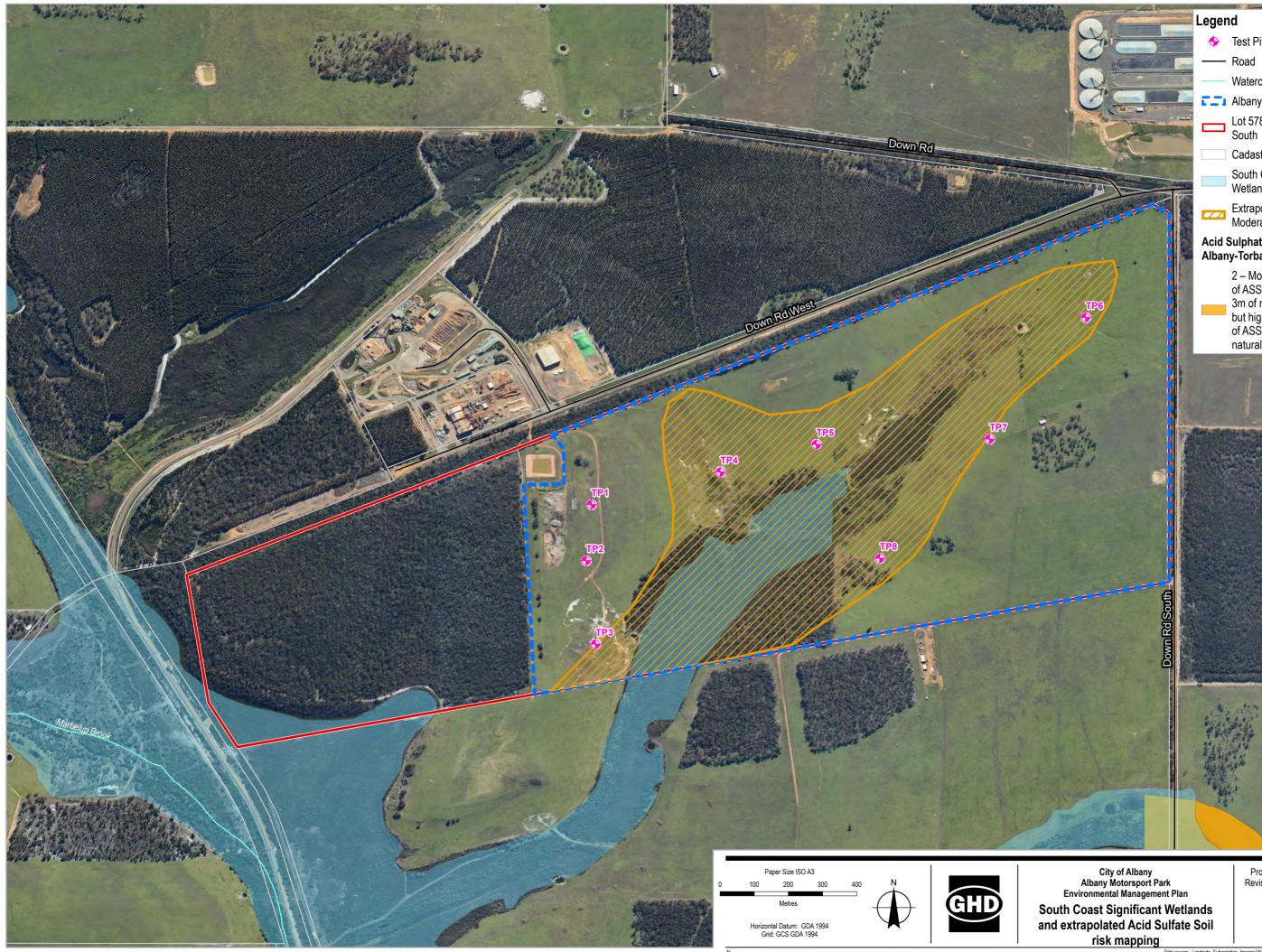
Appendix A Figures

Figure 1	Project site location
Figure 2	Master Plan
Figure 3	DPIRD soil landscape mapping
Figure 4	South Coast Significant Wetlands and extrapolated ASS risk mapping
Figure 5	PDWSA and Water Management Areas
Figure 6	Pre-development catchment plan
Figure 7	1% AEP pre-development maximum flood depths
Figure 8	1% AEP pre-development maximum flow velocities
Figure 9	Stormwater Management Plan – Stage 1A
Figure 10	Stormwater Management Plan – Stage 1B









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- Test Pits
- Watercourse
- **L** Albany Motorsport Park
- Lot 5780 Down Road South
- Cadastre
- South Coast Significant Wetlands
- Extrapolated ASS Moderate to Low Risk

Acid Sulphate Soil Risk: Albany-Torbay

2 – Moderate to low risk of ASS occurring within 3m of natural soil surface but high to moderate risk of ASS beyond 3m of natural soil surface

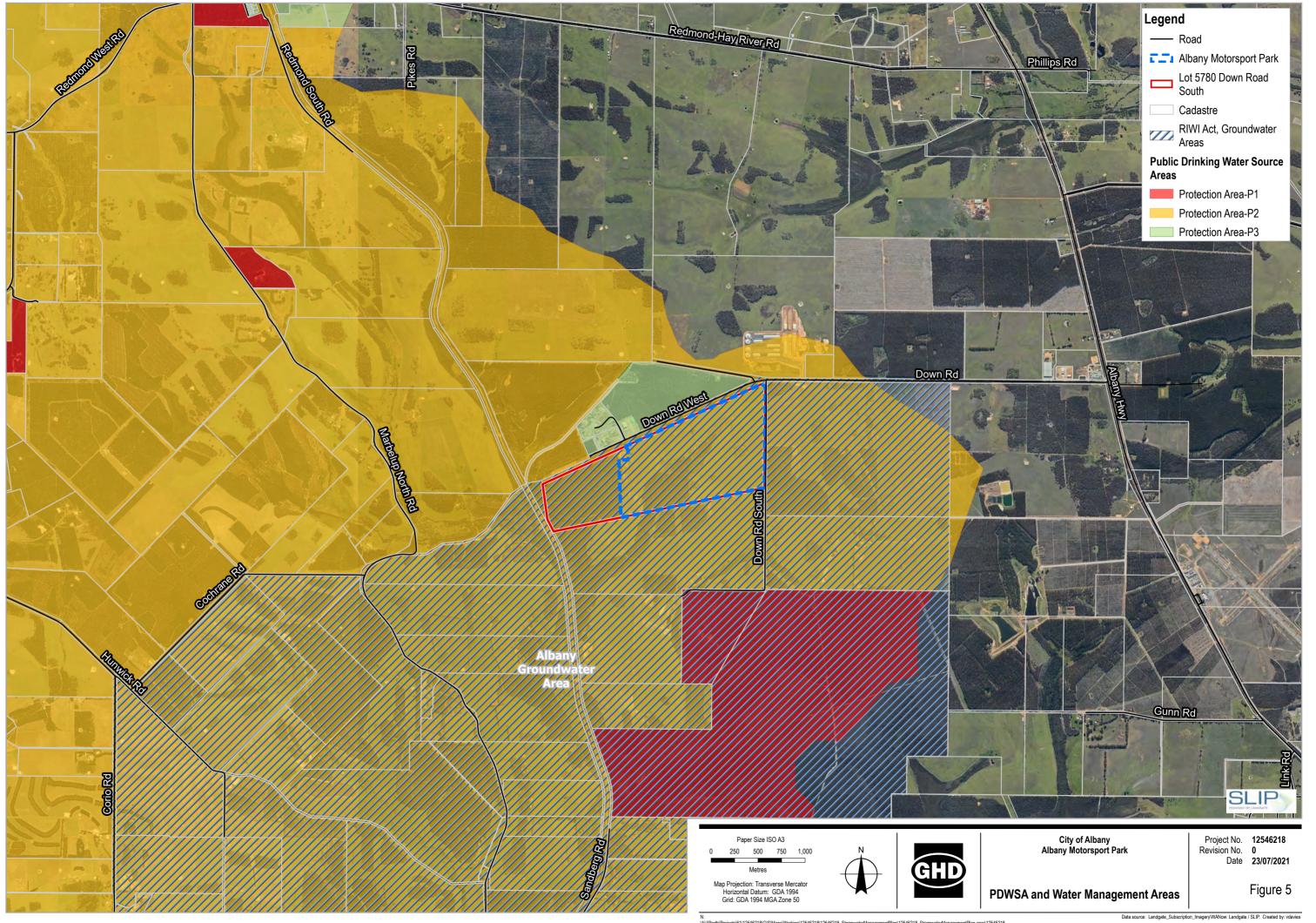
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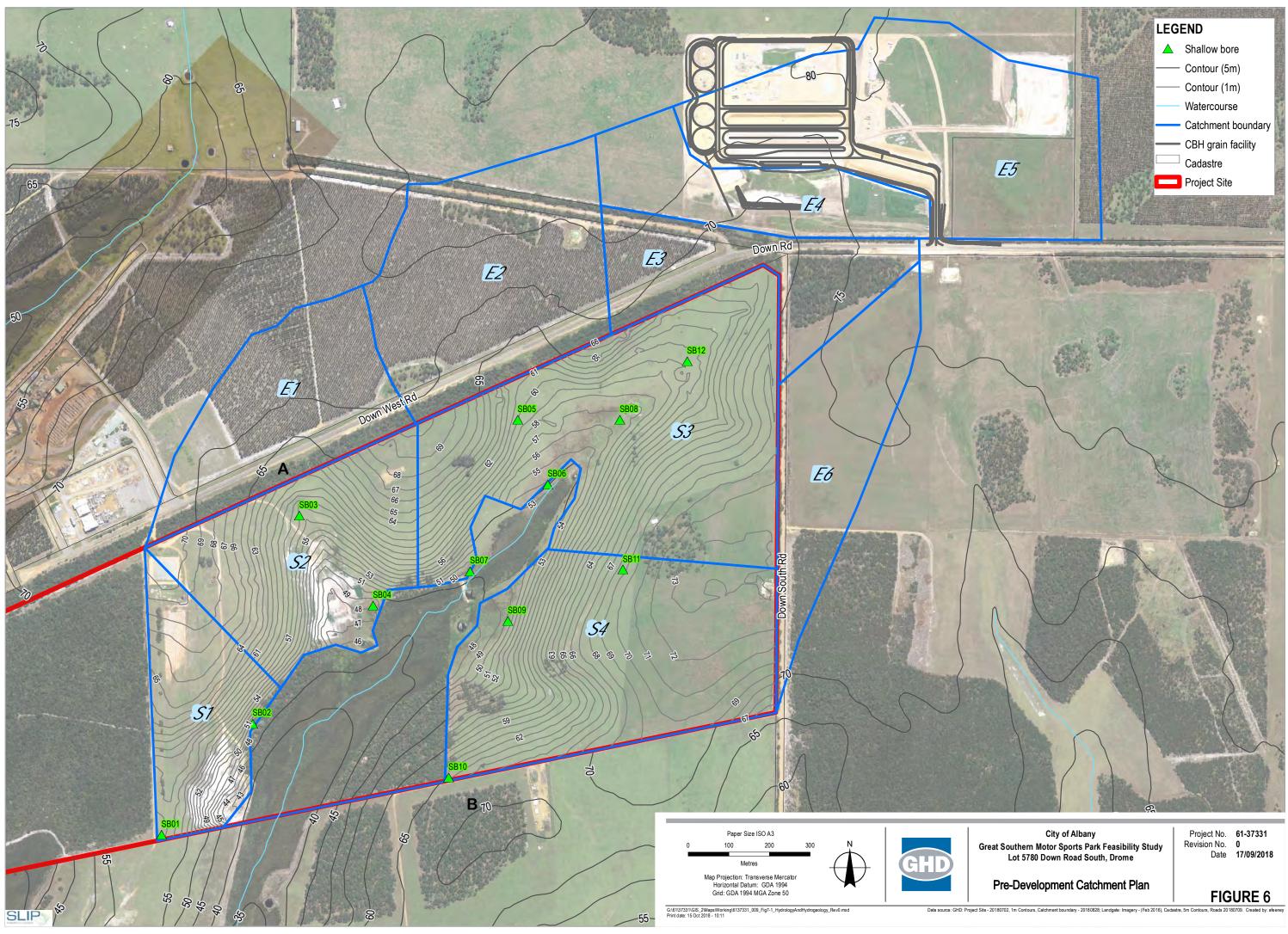
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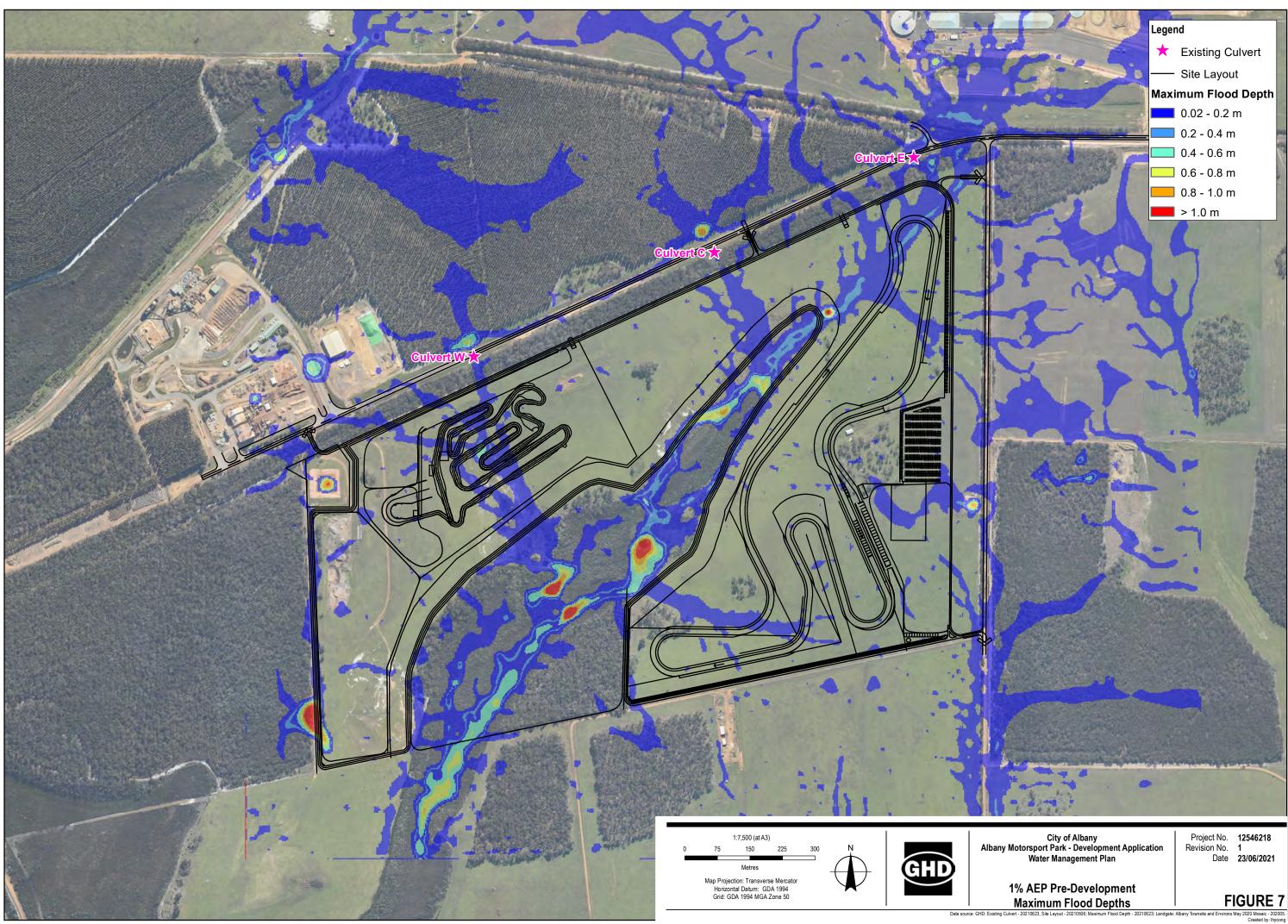
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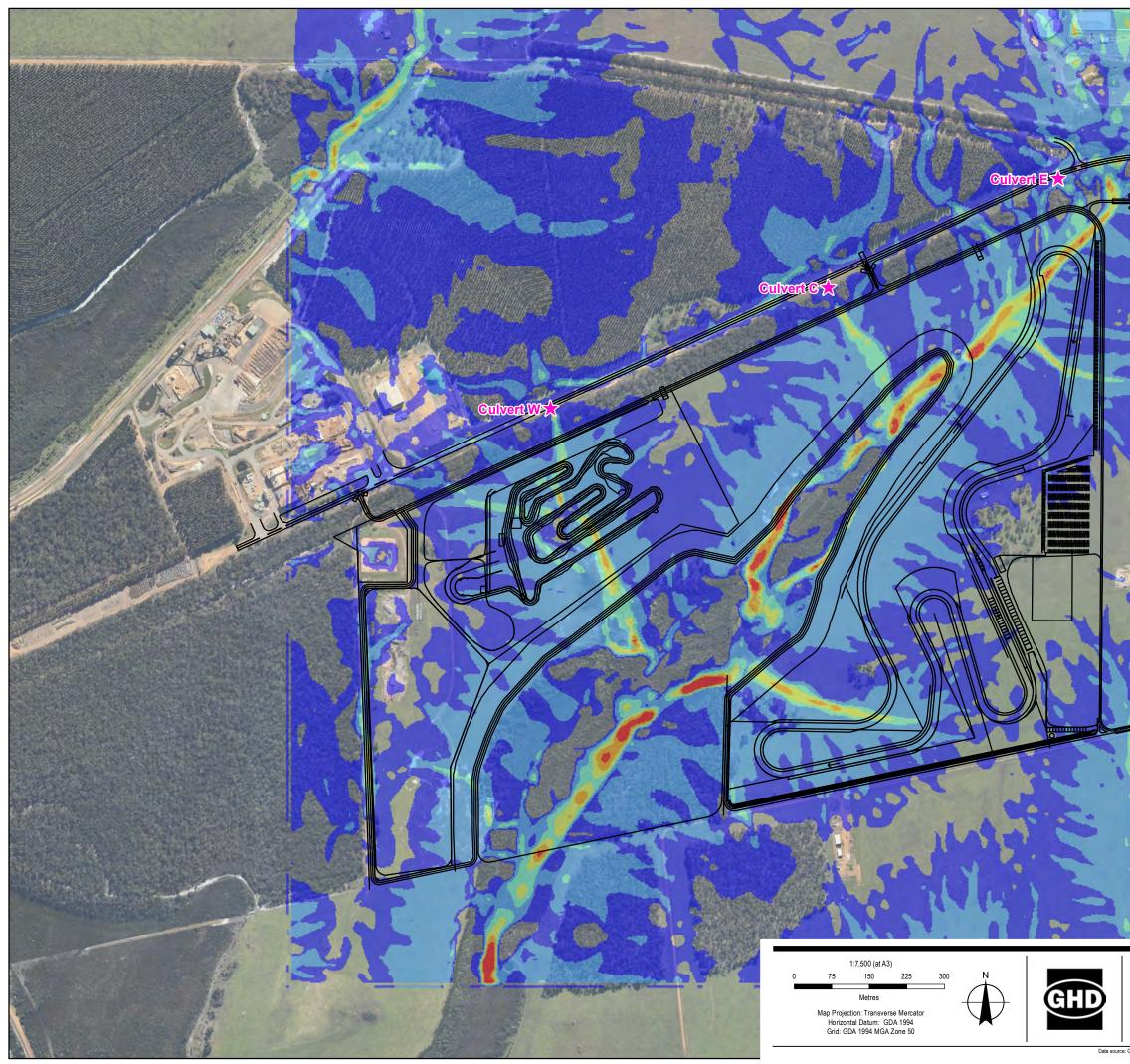
Figure 4



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★ Existing Culvert Site Layout Maximum Flow Velocity 0.1 - 0.2 m/s 0.2 - 0.4 m/s 0.4 - 0.6 m/s ___ 0.6 - 0.8 m/s 0.8 - 1.0 m/s

> 1.0 m/s

Legend

City of Albany Albany Motorsport Park - Development Application Water Management Plan

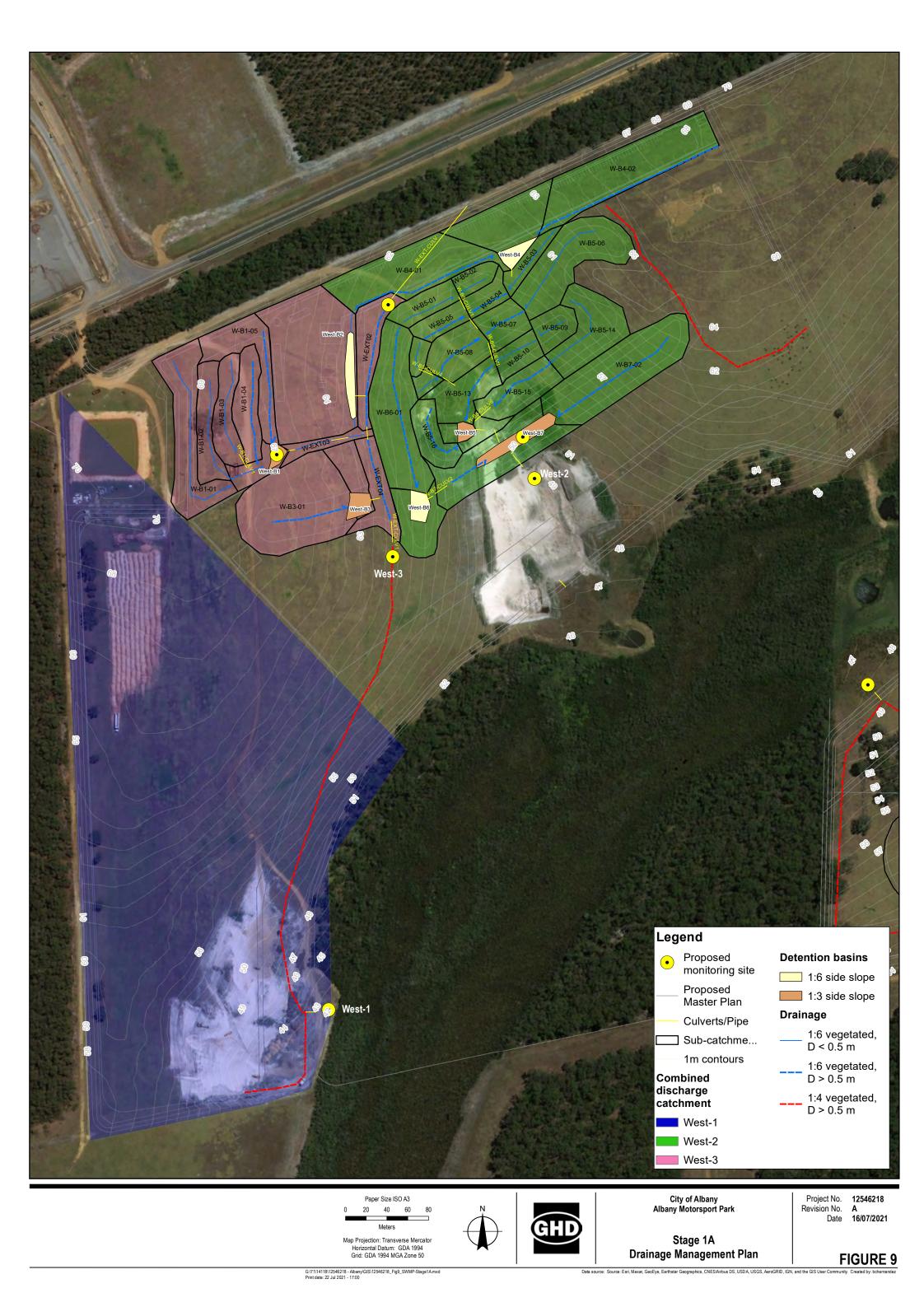
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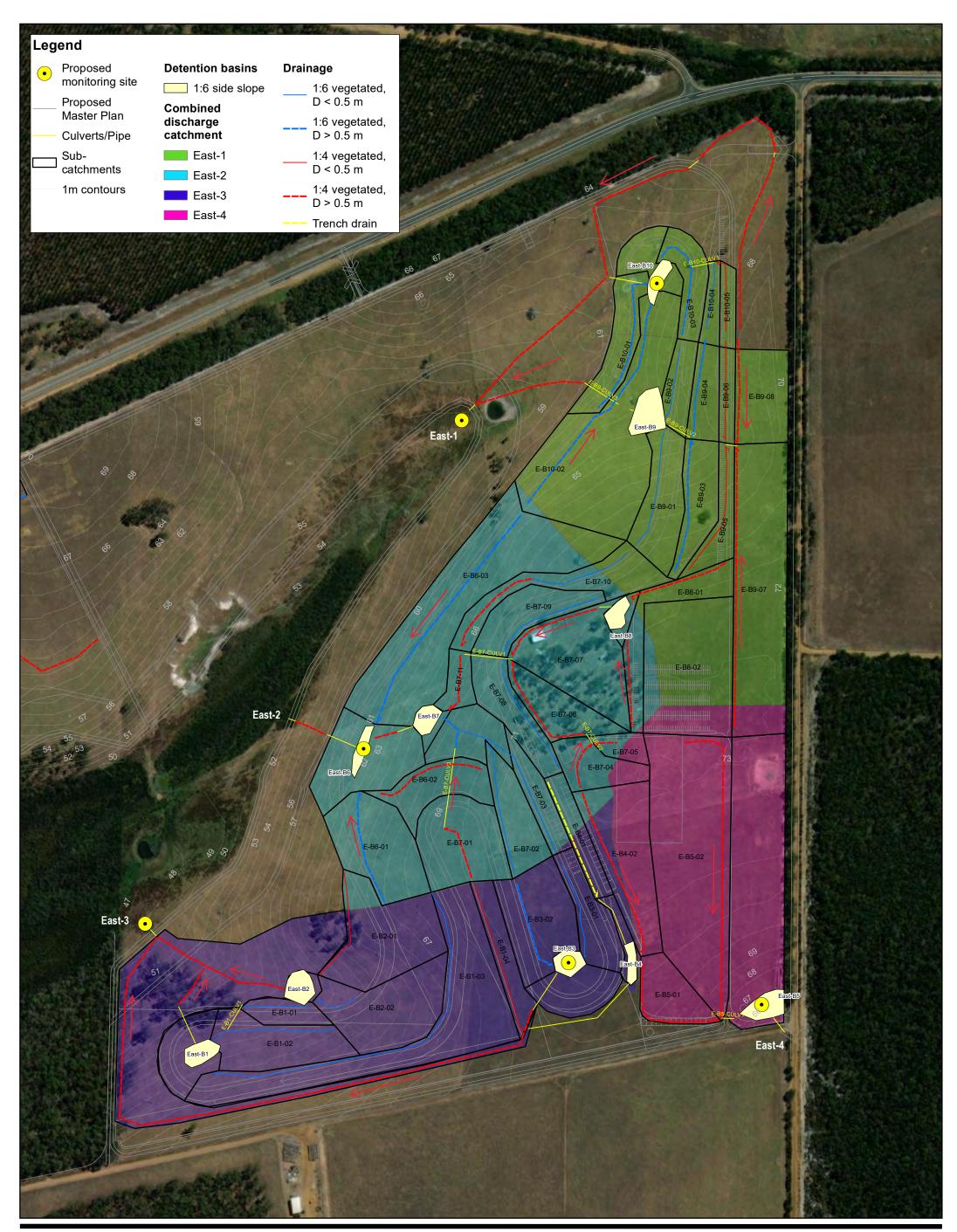
 Revision No.
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 Date
 23/06/2021

1% AEP Pre-Development Maximum Flow Velocities

FIGURE 8 0623; Landgate: Albany Townsite and Environs May 2020 Mosaic - 202005. Created by: Ihyoong Data source: GHD: Existing Culvert







Data source: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community. Created by: bchernandez

Appendix B

Albany Motorsport Park Development, Pavement Investigation (Great Southern Geotechics, 2021)



GREAT SOUTHERN GEOTECHNICS CONSTRUCTION MATERIALS TESTING

Pavement Investigation

Report 4212/1 Friday, 9 April 2021



Albany Motorsport Park Development

GREAT SOUTHERN GEOTECHNICS

1.0 INTRODUCTION

As authorised by GHD

an ivestigation for the proposed Albany Motorsport Park Development adjacent to Down Rd, Mirambeena was performed on the 25/03/2021

2.0 GENERAL

The intent of the investigation was to determine the following:

- Soil types and profiles.
- Characteristics of soil properties on select samples including Particle Size and Consistency Limits. (Liquid Limit, Plastic Limit, Plasticity Index & Linear Shrinkage).
- In Situ pearmeability rates. (Where applicable)
- Groundwater levels at time of investigation.

3.0 SITE INVESTIGATION

Site conditions and test pit locations were recorded and are displayed in Appendix A - Maps. Test pits logs various materials types are noted in Appendix B - Test Pit Logs

The field investigation consisted of 8 Boreholes excavated on-site to depths of up to 2.5 meters using a Kubota KX41-3V mini excavator with a 300mm Auger.

Test pits were spread across the extent of the proposed development and locations were predetermined by GHD.

All soil layers encountered were visually assessed and classified on-site.

Samples gathered from site were the taken back to Great Southern Geotechnics Albany Laboratory For further processing and analysis.

IMPORTANT NOTE: The test pits have been spread so that they are representative of the subsurface materials across the intended reconstruction area, however, soil conditions may change dramatically over short distances and our investigations may not locate all soil variations across the site.

4.0 LABORATORY TESTING

Results of any relevant Laboratory testing preformed are shown in Appendix C. (Test Results Report 4212/2)

This report and associated documentation was undertaken for the specific purpose described in the report and shall not be relied on for other purposes.

This report was prepared solely for the use by GHD any reliance assumed by other parties on this report shall be at such parties own risk.



Appendix A Maps

Figure 1 Test Pits 1 to 8

Test Pit Locations





Job No:4212Client:GHDProject:Albany Motorsport Park Development





Appendix B

Test Pit Logs

5	GREAT SO GEOTEC	UTHERN HNICS TERIALS TESTING	Job 42 ⁻		Test Pit N 1	ło.	Sample No. 4212G1		Sheet	1	of	16	
Client: Project: Project No. Location:	12546218	otorsport Park De } 4"S 117°44'13.1"	-		Date Comme 25/03/202 Logged B M.Coffey	21 3y	Operator/Contract Equipment type: Excavation Methor Position:		Kubota KX41-3V				
Depth Below Surface (mm)	Layer Depth (mm)	F	Particle charac	SOIL TYP	ial Description PE, Plasticity, Colo condary and other		nponents	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 200	200	(Topso	oil) SAND wit	h silt: Dark g	grey, fine to mediu	m. Roots	and root fibres.	М	MD				
200 - 550	350	SA	NDY gravel:		o coarse, sub-rou		ub-angular.	М	MD-D				
				Fine to me	edium grained san	d.							
550 - 2500	1950	San		, to medium r	plasticity, light brow	wn/orang	mottled red	м	F				
550 - 2500	1950	Sand	UY CLAT. LOW		edium grained san		e mouled red.	IVI	F				
					Janan granica can						т.		
											No water table encountered.		
											coun		
											le en		
											' tabl		
											vatei		
											No		
									. =		1	-	
								Target Depth ✓ Cave In Refusal				25	500
								N	ear Refus				
Cohesi	ve	Non-Coh	esive	F	Rock	C	ementation		Flooding				
VS - Very		VL - Very			tremely Low		N - Indurated		ck of Rea				
S - So		L - Loc			Very Low						eral		
F - Firr		MD - Mediur			- Low	PC - I	Poorly Cemented						
		D - Der			Medium	МС	- moderately		D - Dry	M - N	/loist	W - We	et
St - Sti						•		N/A - Not Applicable					
St - Sti VSt - Very	Stiff	VD - Very	Dense	Н	- High		Cemented		N//	A - Not	Applica	ble	
		VD - Very CO - Con			- High Very High		Cemented Well Cemented				Applica Determi		



Excavation



Spoil



Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 2 **of** 16

5	GREAT SOU GEOTECH	THERN HNICS RIALS TESTING	Job No 4212	Test Pit No 2).	Sample No. 4212G2		Sheet	3	of	16	
Client: Project: Project No. Location:	12546218	orsport Park De 'S 117°44'12.6"		Date Commence 25/03/2021 Logged By M.Coffey	,	Operator/Contracto Equipment type: Excavation Method Position:		GSG Kubota KX41-3V 300mm Auger Refer to site plan				
Depth Below Surface (mm)	Layer Depth (mm)	F		rial Description PE, Plasticity, Colour condary and other mi		ponents	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 100	100	(Topso	bil) SAND with silt: Dark	grey, fine to medium.	ı. Roots a	nd root fibres.	М	MD				
100 - 500	400	SA	NDY gravel: Brown, fine			o-angular.	Μ	MD-D				
			Fine to me	edium grained sand.								
500 - 2500	2000	San	dy CLAY: Low to medium	plasticity light brown	n/orange	mottled red	N.4	-				
500 - 2500	2000	Sand		edium grained sand.		mottied red.	М	F				
				salam grainea bana.	•					т.		
										No water table encountered.		
										Icour		
										le en		
		1								er tab		
										wate		
										Ň		
		 										
		+						+				
		-						+				
		1										
							1	Гarget Dep	th	✓	25	500
								Cave In				
								Refusal				
							1	Vear Refus	al			
Cohesiv		Non-Coh		Rock		ementation		Flooding				
VS - Very		VL - Very		xtremely Low	IN	I - Indurated	L	ack of Rea		and l		
S - Sof		L - Loo		Very Low	PC - P	oorly Cemented			Ger	ieral		
F - Firm		MD - Mediun		Low						Anist "		
St - Stif		D - Der		- Medium	MC - moo	derately Cemented		D - Dry		Aoist V		
VSt - Very H - Hare		VD - Very CO - Con		I - High Very High						Applicab Determin		
п - наг	u	CO - CON	ipaci VH -	very migri	WC -	Well Cemented		íN/	ו זטאו - יי	Jerennin	eu	



Excavation



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Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 4 **of** 16

	REAT SOU EOTECH	THERN INICS RIALS TESTING	Job No 4212	Test Pit 3	No.	Sample No. 4212G3		Sheet	5	of	16	
Client: Project: Project No. Location:	12546218	orsport Park De S 117°44'13.5"		Date Comm 25/03/20 Logged M.Coffe	21 By	Operator/Contractor Equipment type: Excavation Methoor Position:			1-3V ger plan			
Depth Below Surface (mm)	Layer Depth (mm)	F		terial Description YPE, Plasticity, Co Secondary and othe		mponents	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 160	160	(Topsoil) Gravelly SAN	D with silt: Grey/bro	own, fine to	o medium.	DM	L-MD				
	<u> </u>		Fine to medium, su	ıb-rounded to sub-a	ngular, gra	avel.						
160 - 2100	1940	(FIL	L) Sandy GRAVEL with	h clay: Low to medi	um plastic	ity, brown/red	М	MD				
		Fine to co	parse, sub-rounded to su	ub-angular gravel. F	ine to med	lium grained sand.						
2100 - 2500	400		SAND	with silt: White, fir	ie.		М	L-MD				
										ered.		
										water table encountered.		
										e enc		
		1								table		
										vater		
										Ň		
		 										
		 										
		┨────										
								1				
							Г	Farget Dep	oth	✓	25	500
							Cave In					
								Refusal				
							١	Vear Refus	al			
Cohesive		Non-Coh	esive	Rock		Cementation		Flooding				
VS - Very So	ft	VL - Very I		Extremely Low		IN - Indurated	La	ack of Rea				
S - Soft		L - Loo		L - Very Low	PC -	Poorly Cemented			Ger	neral		
F - Firm		MD - Mediun		L - Low		-						
St - Stiff		D - Der		M - Medium	MC - m	oderately Cemented		D - Dry		Moist V		
VSt - Very St	iff	VD - Very I		H - High	1					Applicab		
H - Hard		CO - Con		H - Very High	wc	- Well Cemented		N	/D - Not I	Determin	ed	
			EH -	Extremely High								



Excavation



Spoil



Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 6 **of** 16

GR GI	REAT SOUT EOTECH	THERN INICS IALS TESTING	Job No 4212	Test Pit 4	No.	Sample No. 4212G4		Sheet	7	of	16	
Client: Project: Project No. Location:	12546218	orsport Park De S 117°44'25.3"		Date Comm 25/03/20 Logged M.Coffe)21 By	Operator/Contract Equipment type: Excavation Methor Position:			Kub 30 Refe			
Depth Below Surface (mm)	Layer Depth (mm)	F		aterial Description TYPE, Plasticity, Co Secondary and othe		nponents	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 50	50	(Тор	osoil) SAND with silt:	Grey, fine to mediun	n. Roots ar	id root fibres.	D	L				
50 - 850	800		SAND with silt:	Light grey/white, fin	e to mediu	n.	D-M	L-MD				
850 - 2500	1650		SAND with	silt: Brown, fine to	medium.		М	D	WC			
										No water table encountered.		
										count		
										e enc		
										tabl		
										vater		
										Ň		
		ļ										
							-	Farget Don	th	✓	21	500
							Target Depth ✓ Cave In					
								Refusal				
							1	Vear Refus	al			
Cohesive		Non-Cohe	esive	Rock		Cementation		Flooding			1	
VS - Very So	ft	VL - Very I	Loose EL	- Extremely Low		IN - Indurated	L	ack of Rea	h			
S - Soft		L - Loo	se V	/L - Very Low	PC	Poorly Cemented			Ger	neral		
F - Firm		MD - Mediun	n Dense	L - Low	PG-							
St - Stiff		D - Den	ise	M - Medium	MC - m	oderately Cemented		D - Dry	/ M - N	Noist V	V - Wet	
VSt - Very Sti	iff	VD - Very I	Dense	H - High	100 - 111	Cashalory Centented		Ν	I/A - Not	Applicab	le	
H - Hard		CO - Com	npact V	H - Very High	WC	- Well Cemented		N	/D - Not I	Determin	ed	
			EH	- Extremely High								



Excavation



Spoil



Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 8 **of** 16

GR GE CONST	EAT SOUT OTECH	THERN NICS ALS TESTING	Job No 4212	Test P 5		Sample No. 4212G5		Sheet	9	of	16	
Project: Project No.	12546218	rsport Park De 3 117°44'34.4"	·	Date Com 25/03/ Logge M.Co	2021 d By	Operator/Contract Equipment type: Excavation Methor Position:		GSG Kubota KX41-3V 300mm Auger Refer to site plan				
Depth Below Surface (mm)	Layer Depth (mm)	F		Material Descriptio DIL TYPE, Plasticity, (cs, Secondary and ot	Colour,	mponents	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 240	240	(Тор	osoil) SAND with si	ilt: Grey, fine to medi	um. Roots a	nd root fibres.	D	L-MD				
240 - 1100	860		SAND with s	ilt: Light grey/white, f	ine to mediu	ım.	М	L-MD				
1100 0500	1400		0		<u> </u>							
1100 - 2500	1400		-	with silt: Light brown, sub-rounded to sul			М	MD	PC			
			Fille to media		-angulai gra	avei.						
										ъ		
										No water table encountered.		
										Icour		
										ole er		
										er tab		
										wate		
										٩		
								-		-	-	-
							Target Depth ✓					500
							Cave In					
								Refusal				
Cohesive		Non-Coh	osivo	Rock		Cementation	· · ·	Near Refus				
VS - Very Soft	t	VL - Very I		EL - Extremely Low		IN - Indurated	1	ack of Rea				
S - Soft	·	L - Loo		VL - Very Low						neral		
F - Firm		MD - Mediun		L - Low	PC ·	- Poorly Cemented						
St - Stiff		D - Der		M - Medium			1	D - Dry	/ M-N	Moist V	V - Wet	
VSt - Very Stif	ff	VD - Very I		H - High	MC - n	noderately Cemented				Applicab		
H - Hard		CO - Con		VH - Very High		Woll Comostad	1			Determin		
			E	EH - Extremely High		- Well Cemented						



Excavation



Spoil



Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 10 **of** 16

S	EAT SOUT	THERN NICS IALS TESTING	Job No 4212	Test Pit N 6	ło.	Sample No. 4212G6		Sheet	11	of	16	
Client: Project: Project No. Location:	12546218	rsport Park De 8 117°44'59.9"		Date Comme 25/03/202 Logged B M.Coffey	21 3y	Operator/Contract Equipment type: Excavation Method Position:			Kub 30 Refe			
Depth Below Surface (mm)	Layer Depth (mm)	F		erial Description YPE, Plasticity, Colo econdary and other		nponents	Moist. Condition	Consistency / Strength	Classification Symbol	Sample/Test		
0 - 180	180	(Tops	oil) SAND with silt: Gre	ey, fine to medium.	Roots an	d root fibres.	М	L-MD				
180 - 1400	1220		SAND with silt: ∟	ight grey/white, fine	to mediur	n.	М	L-MD				
1400 - 2500	1100		SAND with silt:	Light brown, fine to	medium.		М	MD-D	MC			
										No water table encountered.		
	1									count		
										e enc		
										table		
										vater		
										No		
	*	Cobbles note	d on outer edge of test	nit in shouldor						1		-
			a on outer eage of test	Pri in Shouldel.			Т	Target Depth ✓ Cave In Refusal				500
							N	Refusal	sal			
Cohesive		Non-Coh	esive	Rock	(Cementation		Flooding				
VS - Very Sol	ft	VL - Very I		Extremely Low		N - Indurated	La	ack of Rea				
S - Soft		L - Loo		- Very Low						neral		
F - Firm		MD - Mediun		L - Low	PC -	Poorly Cemented						
St - Stiff		D - Den		I - Medium				D - Dry	/ M-N	Moist V	V - Wet	
VSt - Very Sti	ff	VD - Very I		H - High	MC - mo	oderately Cemented				Applicab		
H - Hard		CO - Com		- Very High	1410					Determin		
				Extremely High	wc	- Well Cemented						



Excavation



Spoil



Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 12 **of** 16

G RI GE	EAT SOUT OTECH	THERN NICS ALS TESTING	Job No 4212	Test Pit	No.	Sample No. 4212G7		Sheet	13	of	16	
Project: Project No.	12546218	rsport Park De \$ 117°44'50.8"		Date Comm 25/03/20 Logged M.Coffe	21 By	Operator/Contractor Equipment type: Excavation Methoor Position:			GSG Kubota KX41-3V 300mm Auger Refer to site plan			
Depth Below Surface (mm)	Layer Depth (mm)	F		terial Description YPE, Plasticity, Col econdary and other		nponents	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 170	170	(Тор	osoil) SAND with silt: G	irey, fine to medium	. Roots ar	d root fibres.	D	MD				
170 - 450	280		SAND with sil	t: Light grey, fine to	medium.		D	L-MD				
450 0400	4050	0		4		uch an and an						
450 - 2100	1650	Sar	ndy GRAVEL: Brown, fir	medium grained sa		sub-angular.	D	MD-D				
				ficularit grained sa	iu.							
2100 - 2500	400		Gravelly SAND with	n silt: Light brown, f	fine to me	lium.	D	MD		pg		
			Fine to medium, su	b-rounded to sub-a	ngualr gra	vel.				water table encountered.		
										ncon		
										ble e		
										ter ta		
										o wat		
										Ž		
												-
										1		
							Target Depth ✓				25	500
							Cave In Refusal					
							١	Vear Refus	al			
Cohesive		Non-Cohe	esive	Rock		Cementation		Flooding				
VS - Very Soft	:	VL - Very l	Loose EL -	Extremely Low		N - Indurated	L	ack of Rea	ich			
S - Soft		L - Loo	se VL	- Very Low	PC	Poorly Cemented			Ger	neral		
F - Firm		MD - Medium	n Dense	L - Low	PG-							
St - Stiff		D - Den	se N	1 - Medium	MC - m	oderately Cemented		D - Dry	/ M - N	Moist V	V - Wet	
VSt - Very Stiff	f	VD - Very I		H - High		, comoniou		Ν	I/A - Not	Applicab	le	
H - Hard		CO - Com		I - Very High	wc	- Well Cemented		N	/D - Not I	Determin	ed	
			EH -	Extremely High								



Excavation



Spoil



Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 14 **of** 16

GRE/	AT SOUTHER DTECHNIC	C	b No 212	Test Pit N 8	10.	Sample No. 4212G8		Sheet	15	of	16	
Project: Al Project No. 12	HD bany Motorsport F 2546218 I°56'03.5"S 117°4	Park Development 4'40.4"E		Date Comme 25/03/202 Logged E M.Coffey	21 3y	Operator/Contractor Equipment type: Excavation Methoor Position:		GSG Kubota KX41-3V 300mm Auger Refer to site plan				
Depth Below Surface (mm)	Layer Depth (mm)	Particle chara	SOIL TYF	rial Description PE, Plasticity, Colc condary and other		nponents	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 200	200	(Topsoil) SAND) with silt: Gre	ey, fine to medium.	Roots an	d root fibres.	D	MD				
200 - 950	750	SA	AND with silt:	Light grey, fine to	medium.		D	MD				
050 0500	4550	0					_					
950 - 2500	1550	Sandy GRAVE		to coarse, sub-rou		sub-angular.	D	MD-D				
			Fille to file	euluill grailleu sail	u.							
										ъ.		
										water table encountered.		
										Icour		
										ole er		
										er tab		
										wate		
										Ň		
												<u> </u>
							Т	arget Dep	oth	~	25	500
							Cave In					
								Refusal				
Cohesive	No	n-Cohesive		Rock		Cementation	N	lear Refus Flooding				
VS - Very Soft		- Very Loose		ktremely Low		N - Indurated	1:	ack of Rea				
S - Soft		L - Loose		Very Low						eral		
F - Firm		Medium Dense		Low	PC -	Poorly Cemented						
St - Stiff) - Dense		Medium				D - Dry	/ M-N	<i>l</i> loist V	V - Wet	
VSt - Very Stiff		- Very Dense		I - High	MC - m	oderately Cemented				Applicab		
H - Hard) - Compact	1	Very High	14/0	Woll Competed				Determin		
				tremely High	wc	- Well Cemented						

Test Pit No.8



Excavation



Spoil



Job No:4212Client:GHDProject:Albany Motorsport Park Development

Sheet 16 of 16



Appendix C Test Results



Job No: 4212 Report No: 4212 / 2 Page No: 1 of 5

Client:	GHD
Project:	Albany Motorsport Park Development
Section:	Test Pit 4

Client Number: 12546218 Date of Test:

25/03/2021

Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs (Report 4212/1)
•			

Sample No.

4212G9

Saturated Hydraulic Conductivity (cm/min)	0.0913	
Saturated Hydraulic Conductivity (m/day)	1.31	
Saturated Hydraulic Conductivity (m/sec)	1.52E-05	



Comments:	The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics		
	Scope of Accreditation.	Name:	M.Coffey
		Function:	Quality Manager
Disclaimer:	Great Southern Geotechnics does not warrant data produced by use of this spreadsheet or any interpretation based on that data.	Date:	9/04/2021
Distribution:	Laboratory File / Vicki Davies - GHD	Approved	Ch
Document ID:	WS_1547_TalsmaHallam_Rev2_Mar2020	Ву:	



Job No: 4212 Report No: 4212 / 2 Page No: 2 of 5

Client:	GHD
Project:	Albany Motorsport Park Development
Section:	Test Pit 5

Client Number: 12546218 Date of Test:

25/03/2021

Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs (Report 4212/1)

Sample No.

4212G10

Saturated Hydraulic Conductivity (cm/min)	0.0342	
Saturated Hydraulic Conductivity (m/day)	0.49	
Saturated Hydraulic Conductivity (m/sec)	5.70E-06	



Comments:	The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics		
	Scope of Accreditation.	Name:	M.Coffey
		Function:	Quality Manager
Disclaimer:	Great Southern Geotechnics does not warrant data produced by use of this spreadsheet or any interpretation based on that data.	Date:	9/04/2021
Distribution:	Laboratory File / Vicki Davies - GHD	Approved	Ch
Document ID:	WS_1547_TalsmaHallam_Rev2_Mar2020	By:	



Job No: 4212 Report No: 4212 / 2 Page No: 3 of 5

Client:	GHD
Project:	Albany Motorsport Park Development
Section:	Test Pit 6

Client Number: 12546218 Date of Test:

25/03/2021

Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs (Report 4212/1)
-			

Sample No.

4212G11

Saturated Hydraulic Conductivity (cm/min)	0.2282
Saturated Hydraulic Conductivity (m/day)	3.29
Saturated Hydraulic Conductivity (m/sec)	3.80E-05



Comments:	The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics		
	Scope of Accreditation.	Name:	M.Coffey
		Function:	Quality Manager
Disclaimer:	Great Southern Geotechnics does not warrant data produced by use of this spreadsheet or any interpretation based on that data.	Date:	9/04/2021
Distribution:	Laboratory File / Vicki Davies - GHD	Approved	Ch
Document ID:	WS_1547_TalsmaHallam_Rev2_Mar2020	Ву:	



Job No: 4212 Report No: 4212 / 2 Page No: 4 of 5

Client:	GHD
Project:	Albany Motorsport Park Development
Section:	Test Pit 7

Client Number: 12546218 Date of Test:

25/03/2021

Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs (Report 4212/1)

Sample No.

4212G12

Saturated Hydraulic Conductivity (cm/min)	0.2282
Saturated Hydraulic Conductivity (m/day)	3.29
Saturated Hydraulic Conductivity (m/sec)	3.80E-05



Comments:	The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics		
	Scope of Accreditation.	Name:	M.Coffey
		Function:	Quality Manager
Disclaimer:	Great Southern Geotechnics does not warrant data produced by use of this spreadsheet or any interpretation based on that data.	Date:	9/04/2021
Distribution:	Laboratory File / Vicki Davies - GHD	Approved	Ch
Document ID:	WS_1547_TalsmaHallam_Rev2_Mar2020	By:	



Job No: 4212 Report No: 4212 / 2 Page No: 5 of 5

Client:	GHD
Project:	Albany Motorsport Park Development
Section:	Test Pit 8

Client Number: 12546218 Date of Test:

25/03/2021

Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs (Report 4212/1)

Sample No.

4212G13

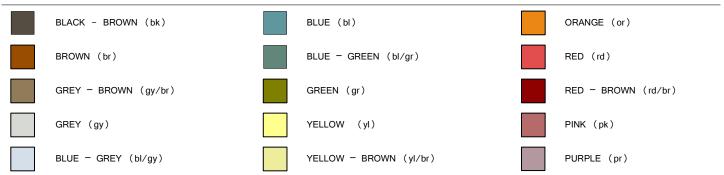
Saturated Hydraulic Conductivity (cm/min)	0.0285
Saturated Hydraulic Conductivity (m/day)	0.41
Saturated Hydraulic Conductivity (m/sec)	4.75E-06



Comments:	The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics		
	Scope of Accreditation.	Name:	M.Coffey
		Function:	Quality Manager
Disclaimer:	Great Southern Geotechnics does not warrant data produced by use of this spreadsheet or any interpretation based on that data.	Date:	9/04/2021
Distribution:	Laboratory File / Vicki Davies - GHD	Approved	ch
Document ID:	WS_1547_TalsmaHallam_Rev2_Mar2020	Ву:	



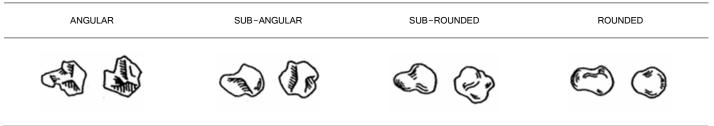
COLOURS



MOISTURE CONDITION OF SOIL

TERM	DESCRIPTION
Dry	Cohesive soils; hard and friable or powdery, well dry of plastic limit. Granular soils; cohesionless and free-running.
Moist	Soil feels cool, darkened in colour. Cohesive soils can be moulded. Granular soils tend to cohere.
Wet	Soil feels cool, darkened in colour. Cohesive soils usually weakened and free water forms on hands when handling. Granular soils tend to cohere and free water forms on hands when handling.

PARTICLE SHAPES



PARTICLE SIZES

BOULDERS	COBBLES	COARSE GRAVEL	MEDIUM GRAVEL	FINE GRAVEL	COARSE SAND	MEDIUM SAND	FINE SAND	SILT	CLAY
>200mm	63- 200mm	20- 63mm	6- 20mm	2.36- 6mm	0.6- 2.36mm	0.2- 0.6mm	0.075- 0.2mm	0.002- 0.075mm	<0.002mm

GRAIN SIZE

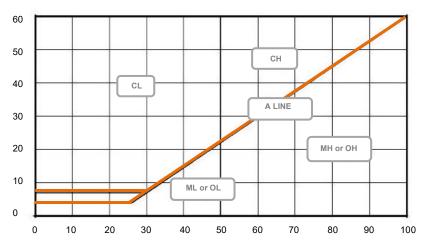
SOIL TYPE (ABBREV.)	CLAY (CL)	SILT (SI)	←	SAND (SA)	\longrightarrow	<	GRAVEL (GR)	\longrightarrow	COBBLES (CO)
SIZE	< 2µm	2-75µm	Fine 0.075- 0.2mm	Medium 0.2-0.6mm	Coarse 0.6-2.36mm	Fine 2.36-6mm	Medium 6-20mm	Coarse 20-63mm	63-200mm
SHAPE & TEXTURE	Shiny	Dull	<	a	ngular or sub an	gular or sub ro	unded or rounded	i ———	\longrightarrow
FIELD GUIDE	Not visible under 10x	Visible under 10x	Visible by eye	Visible at < 1m	Visible at < 3m	Visible at < 5m	Road gravel	Rail ballast	Beaching



CLASSIFICATION CHART

		(Excluding particle	GROUP SYMBOLS	TYPICAL NAMES				
E	fraction	CLEAN GRAVELS (Little or no fines)	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength					Well graded gravels, gravel-sand mixtures, little or no fines
han 0.075	GRAVELS 60% of coarse 1 er than 2.36mn	CLEAN GRAVEL (Little or fines)	Predominar		with some intermediate sizes rse grains, no dry strength	missing, not	GP	Poorly Graded gravels and gravel-sand mixtures, little or no fines, uniform gravels
COARSE GRAINED SOILS More than 50% of material less than 63 mm is larger than 0.075 mm	GRAVELS More than 50% of coarse fraction is larger than 2.36mm	GRAVELS WITH FINES (Appreciable amount of fines)	Dirty'n	naterials with excess of non-pla	astic fines, zero to medium dry	strength	GM	Silty gravels, gravel-sand-silt mixtures
GRAINED SOILS than 63 mm is	More t	GRAVEL WITH FIN (Apprecia amount fines)	'Dirty	materials with excess of plas	tic fines, medium to high dry s	trength	GC	Clayey gravels, gravel-sand-clay mixtures
COARSE GR erial less tha	fraction	CLEAN SANDS (Little or no fines)	Wide range	-	mounts of all intermediate sizes grains, no dry strength	s, not enough	sw	Well graded sands, gravelly sands, little or no fines
CC of materia	SANDS More than 50% of coarse fraction is smaller than 2.36mm	CLEAN (Little fine	Predominar		with some intermediate sizes se grains, no dry strength '	missing, not	SP	Poorly graded sands and gravelly sands; little or no fines, uniform sands
than 50%	SAr than 50% smaller th	is smaller th SANDS WITH FINES (Appreciable amount of fines)	Dirty' materials with excess of non-plastic fines, zero to medium dry strength				SM	Silty sands, sand-silt mixtures
More	More	SANDS FIN (Appr amou	'Dirty	irty' materials with excess of plastic fines, medium to high dry strength				Clayey sands, sand-clay mixtures
			IDENTIFICATION PROCEDURES ON FRACTIONS <0.2mm					
han		DRY STR	RENGTH	DILATANCY	TOUGHNESS			
FINE GRAINED SOILS material less than 63 mm is smaller than 0.075 mm	SILTS AND CLAYS Liquid limit less than 50	None t	to low	Quick to slow	None		ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with low plasticity. Silts of low to medium Liquid Limit.
solLs an 63 mn m	SILTS AND CLAYS uid limit less than	Medium	to high	None to very slow	Medium		CL, CI	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays.
FINE GRAINED SOILS material less than 63 0.075 mm	Liq	Low to	medium	Slow	Low		OL	Organic silts and organic silt-clays of low to medium plasticity.
oť	AYS er than	Low to	medium	Slow to none	Low to medium	Low to medium		Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, silts of high Liquid Limit.
More than 50%	SILTS AND CLAYS Liquid limit greater than 50	High to v	very high	None	High		СН	Inorganic clays of high plasticity.
M	SILT	Medium	to high	None to very slow	Low to medium		он	Organic clays of high plasticity
HIGHLY OR	GANIC SOILS	Readily ide	entified by colo	ur, odour, spongy feel and fre	quently by fibrous texture	Pt	Pe	at and other highly organic soils

PLASTICITY CHART



For laboratory classification of fine grained soils



PLASTICITY

DESCRIPTIVE TERM	OF LOW PLASTICITY	OF MEDIUM PLASTICITY	OF HIGH PLASTICITY
Range Of Liquid Limit (%)	≤ 35	> 35 ≤ 50	> 50

DESCRIPTION OF ORGANIC OR ARTIFICIAL MATERIALS

PREFERRED TERMS	SECONDARY DESCRIPTION
Organic Matter	Fibrous Peat/ Charcoal/ Wood Fragments/ Roots (greater than approximately 2mm diameter)/ Root Fibres (less than approximately 2mm diameter)
Waste Fill	Domestic Refuse/ Oil/ Bitumen/ Brickbats/ Concrete Rubble/ Fibrous Plaster/ Wood Pieces/ Wood Shavings/ Sawdust/ Iron Filings/ Drums/ Steel Bars/ Steel Scrap/ Bottles/ Broken Glass/ Leather

CONSISTENCY - Cohesive soils

TERM	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD	
Symbol	VS	S	F	St	VSt	Н	
Undrained Shear Strength (kPa)	< 12 12 - 25 25 - 50 50 - 100		50 - 100	100 - 200	> 200		
SPT (N) Blowcount	0 - 2	2 - 4	4 - 8	8 - 15	15 - 30	> 30	
Field Guide	Exudes between the fingers when squeezed	Can be moulded by light finger pressure	Can be moulded by strong finger pressure	Cannot be moulded by fingers. Can be indented by thumb nail	Can be indented by thumb nail	Can be indented with difficulty with thumb nail	

CONSISTENCY - Non-cohesive soils

TERM	VERY LOOSE	LOOSE	MEDIUM DENSE	DENSE	VERY DENSE	COMPACT
Symbol	VL	L	MD	D	VD	со
SPT (N) Blowcount	0 - 4	4 - 10	10 - 30	30 - 50	50 - 100	> 50/150 mm
Density Index (%)	< 15	15 - 35	35 - 65	65 - 85	85 - 95	> 95
Field Guide	Ravels	Shovels easily	Shovelling very difficult	Pick required	Pick difficult	Cannot be picked

MINOR COMPONENTS

TERM	TRACE	WITH
% Minor Component	Coarse grained soils: < 5%	Coarse grained soils: 5 - 12%
	Fine grained soils: <15%	Fine grained soils: 15 - 30%
Field Guide	Presence just detectable by feel or eye, but soil properties little	Presence easily detectable by feel or eye, soil properties
	or no different to general properties of primary components	little different to general properties of primary component



GEOLOGICAL ORIGIN

	TYPE	DETAILS
TRANSPORTED SOILS	Aeolian Soils	Deposited by wind
	Alluvial Soils	Deposited by streams and rivers
	Colluvial Soils	Deposited on slopes
	Lacustrine Soils	Deposited by lakes
	Marine Soils	Deposited in ocean, bays, beaches and estuaries
FILL MATERIALS	Soil Fill	Describe soil type, UCS symbol and add 'FILL'
	Rock Fill	Rock type, degree of weathering, and word 'FILL'.
	Domestic Fill	Percent soil or rock, whether pretrucible or not.
	Industrial Fill	Percent soil, whether contaminated, particle size & type of waste product, ie brick, concrete, metal

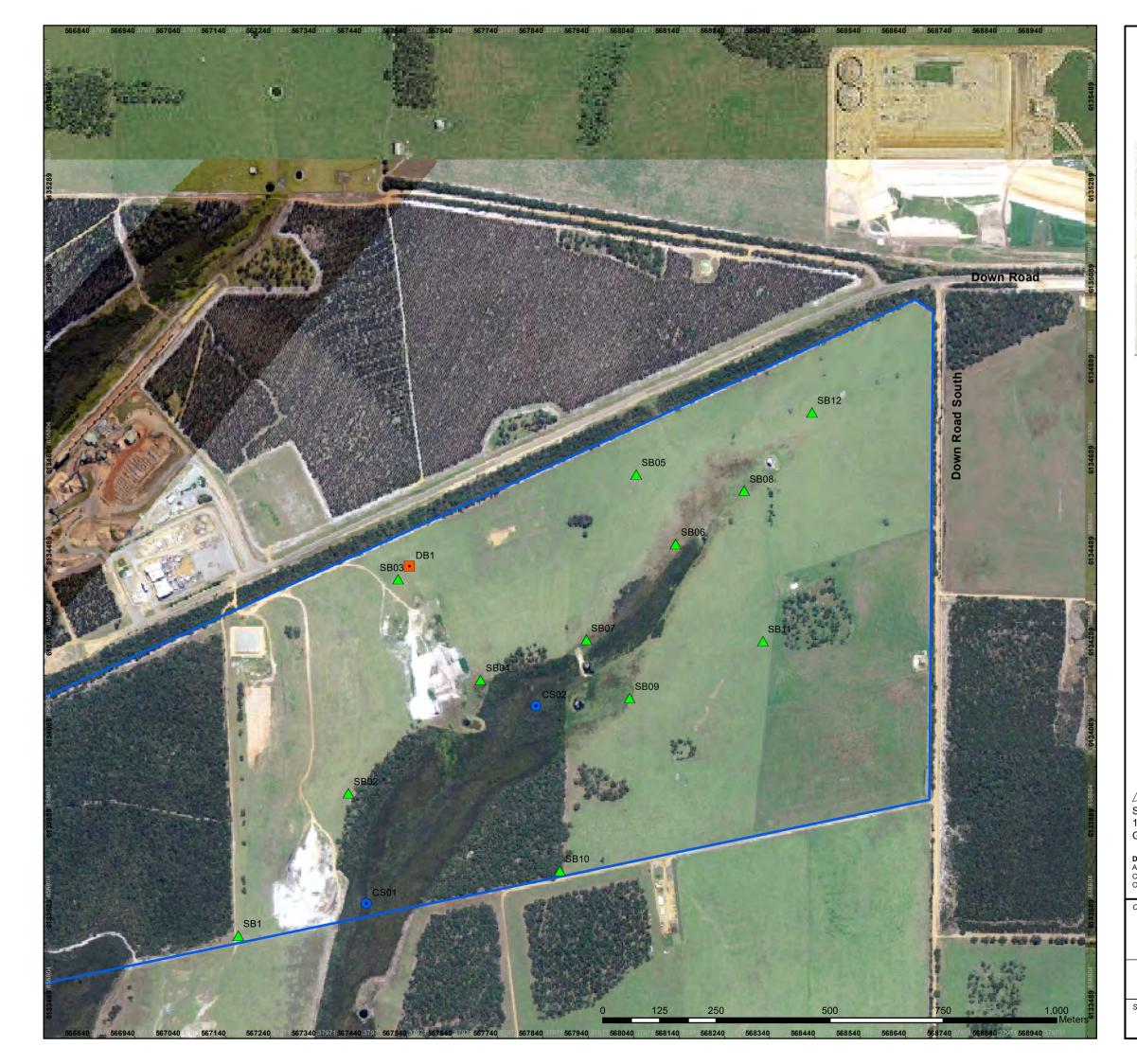
STRENGTH OF ROCK MATERIAL

TERM	SYMBOL	IS (50)	(MPA)	FIELD GUIDE TO STRENGTH
Extremely Low	EL	≤0.03		Easily remoulded by hand to a material with soil properties.
Very Low	VL	>0.03	≤0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxle sample by hand. Pieces up to 3 cm thick can be broken by finger pressure.
Low	L	>0.1	≤0.3	Easily scored with a knife; indentations 1 mm to 3 mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150 mm long by 50 mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.
Medium	Μ	>0.3	≤1.0	Readily scored with a knife; a piece of core 150 mm long by 50 mm diameter can be broken by hand with difficulty.
High	н	>1	≤3	A piece of core 150 mm long by 50 mm diameter cannot be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.
Very High	VH	>3	≤10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.
Extremely High	EH	>10		Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.

ROCK MATERIAL WEATHERING CLASSIFICATION

TERM	SYMBOL	DEFINITION
Residual Soil	RS	Soil developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported
Extremely Weathered Rock	XW	Rock is weathered to such an extent that it has 'soil' properties, i.e. it either disintegrates or can be remoulded, in water.
Distinctly Weathered Rock	DW	Rock strength usually changed by weathering. Rock may be highly discoloured, usually be iron staining. Porosity may be increased by leaching or may be decreased due to deposition of weathering products in pores.
Slightly Weathered Rock	SW	Rock is slightly discoloured but shows little or no change of strength from fresh rock.
Fresh Rock	FR	Rock shows no sign of decomposition or staining.

Appendix C Bio Diverse Solutions monitoring



Unit 5A, 209 Chester Pass Rd Albany, WA 6330 Australia Tel: 08 9842 1575 Fax: 08 9842 1575 Green-valley -Millbrook-Rd-Albany Airport Marbe lup Overview Map Scale 1:100,000 Legend Subject Site Cadastre 5m Contours Deep Bore ▲ Shallow Bore • Creek Sample ---- 50m Buffer <u>k</u> Scale 1:7,882 @ A3 GDA MGA 94 Zone 50 Data Sources Aerial Imagery: SLIP Virtual Mosaic WMS Service, Landgate 2016 Cadastre and Contours: Landgate 2016 Overview Map: World Topographic map service, ESRI 2012 CLIENT City of Albany Lot 5780 Down Road Drome, WA 6330 **Monitoring Plan** STATUS FILE DATE FINAL MSC0137 28/02/2019

29 Hercules Cres Albany WA 6330 98421575 kath@biodiversesolutions.com.au ABN 48 138 824 272



21st March 2018

Great Southern Motorplex PO Box 1905 Albany, WA 6330

Lot 5780 Down Road, Drome WA 6330 Water Quality Monitoring

Dear Great Southern Motorplex Group,

On the 27th February 2018 the shallow monitoring bores were installed at Lot 5780 Down Road, Drome. A total of 12 sampling bores were installed to a depth of 2m as per the DoW Approved Monitoring Plan.

A copy of details relating to this supplied:

- Field test bore logs;
- MPL Laboratory results; and
- BDS Field and Laboratory summary sheets.

Preliminary analysis of the land from the site soil testing indicates that the majority of the land will be sand over gravels/laterite rock. Low lying areas adjacent to the creek will have silty sands with coffee rock and will generally be waterlogged. Water table was only encountered at the lower lying bores of SB06, SB07 and SB09 which I would expect in summer conditions this to prevail. The creek was running albeit at a very low level which indicates there is groundwater movement into the creek system year round.

I am expecting given the soil results, that there will be limited groundwater in test pits SB11, SB03, SB02, SB05, and SB10 through the year. Marginal groundwater will most likely appear in SB04, SB08 and SB12. Refer to finalised Test Pit locations mapping.

Due to limited funds available the deep water bore is yet to be done but recommend this is done as soon as the full quote is approved.

Field analysis of the WQ at the creek indicates the creek is gaining acidity through the catchment. A higher pH in the upper reaches with a pH 6.34 at CS02 and lower (more acidic) pH in the lower catchment CS01 of 4.46, which is to be expected when cattle are entering the system to feed, water and defecating (generally disturbing the upper catchment).

Laboratory testing results are partially available, we are still waiting Salinity, hardness/alkalinity. Biological analytes are not available this round. Full analysis has not been undertaken of the laboratory results as yet.

This information is provided as preliminary, if you have any queries regarding this matter, please feel free to contact me via email on <u>kath@biodiversesolutions.com.au</u> or phone/fax on 9842 1575.

Kind regards,

Kathryn Kinnear Director, Bio Diverse Solutions

Soil Profile Sampling



Location: Lot 5780 Down Road

Date tested: 27/02/2018

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Sampled by: Kathryn Kinnear

Weather: Windy, cool 21 degrees Overcast

Location	Site	Depth of	Soil Description
	description	profile (mm)	
SB1	South west corner Open Paddock	0-150 150-300 300-500 500-1200 1200-1500 1500-2000	Dark grey sandy top soil, veg matter. Grey silty sand. Orange, light brown sandy gravel pebbles 10- 30mm. Laterite rock . Light brown pebbles 10-30mm, orange sandy silty gravel. Light brown sandy clay, slightly moist. No WT.
SB02	Paddock near creek west side Jarrah/Cas/Marri Forrest adjacent	0-50 50-200 200-800 800-1200 1200-1500 1500-2000 2000-2500	Dark grey sandy top soil, veg matter. Grey sandy silt. Light grey sandy silt, slightly moist. Cream sandy silt, slightly moist Laterite rock. Moist light brown orange sandy silt gravel, pebbles 10-30mm, minor clay. Light grey silty sand. No WT.
SB03	Open paddock North in minor Drainage swale	0-50 50-500 500-1000 1000-1200 1200-1600 1600-1800 1800-2000	Light brown slightly moist silty sand top soil, veg matter. Light brown silty gravel, pebbles 5-10mm. Brown silty gravel pebbles 20-30mm. Dark brown gravelly silt pebbles 20-30mm. Grey silty sand. Light grey moist silty sand. Light brown/orange silty sand, gravel pebbles 10-30mm. No WT.
SB04	Paddock near Creek in Depression area.	0-50 50-200 700-900 900-1300 1300-1500 1500-1800 1800-2000	Dark brown peaty organic matter. Dark grey silty sand slightly moist. Light grey silty sand moist. Laterite rock, moist dark brown gravelly silt (coffee rock) mottled orange. Light brown silty clay wet. Light grey moist clay. White clay not wet. No WT.
SB05	North paddock Area	0-50 50-200 200-700 700-900 900-1500 1500-1800 1800-1900 1900-2000	Slightly moist dark brown peaty sandy silt top soil, veg matter. Dry dark grey silty sand. Dry light grey silty sand orange pebbles. Dry cream quartz gravelly silty sand pebbles 30- 50mm. Pink/orange silty sand gravel, cemented compacted gavel pebbles 10-30mm. Moist dark clayey sand. Dry compacted silty gravel orange/pink. No WT.

Location	Site description	Soil Description	
SB06	Near creek North side In reed beds	(mm) 0-100 100-400 400-700 700-1800 1800-2000	Dark brown peaty organic matter moist. Dark grey silty sand moist. Grey silty sand moist. Light grey slty sand wet (smell). Wet brown silty sand (smell) WT 870mm BGL
SB07	Near creek Crossing North side	0-200 200-400 400-600 600-1800 1800-2000	Dark brown/black peaty moist. Black/dark grey peaty sand moist. Dark grey silty sand moist. Light brown silty sand smell. Cream wet silty sand smell. WT 640mm BGL
SB08	Mid creek near dam	0-50 50-200 200-500 500-900 900-1200 1200-1400 1400-1800 1800-2000	Slightly moist dark brown peaty silt, veg matter. Dark brown sandy peaty silt moist. Dark grey silty sand moist. Grey slightly moist silty sand. Dark brown cemented silt, coffee rock. Dark grey moist to wet silty sand. Grey silty sand wet. Dark brown silt minor pebbles 10mm. No WT.
SB09 South side of creek SB010 South boundary east of bush line in paddock		0-50 50-200 200-600 600-700 700-1100 1100-1300 1300-2000	Dark brown peaty organic matter moist. Dark grey silty sand. Grey silty sand. Light brown gravelly silt. Laterite rock. Wet silt pebbles 30-40mm. White moist clayey silt. WT 660mm BGL
		0-50 50-300 300-500 500-1200 1200-2000	Brown silty sand organic matter dry. Brown silty sand gravels 40-50mm, boulders 200mm Laterite, dry. Brown/orange silty sandy gravel cemented Laterite. Light brown/orange cemented silt. White mottles sandstone dry. Light brown/orange cemented silt. White mottles sandstone dry. No WT.
SB011	Mid paddock, top of hill eastern side of site	0-50 50-300 300-400 400-1200 1200-1800 1800-2000	Dark brown silty sand dry. Grey silty sand dry. Light brown silty gravel pebble 30-50mm. Light brown cemented silt Laterite. Light brown, mottles pink * white clay dry. Orange mottled red dry clay. No WT.
SB012		0-400 400-1000 1000-1500 1500-1800 1800-2000	Grey sandy silt organic matter dry. Light grey silty sand. Cream silty sand slightly moist. Dark brown sandy silt, slightly moist gravel minor pebbles. Light brown silty clayey slightly moist boulder Laterite gravels 40mm. No WT.

Groundwater Monitoring Data Record Sheet

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AND DUD

30/05/2018 Name of recorder					Kathryn Kinnear / Bianca Theyer					
Down Road			Project No.		MSC0137					SOLUTIONS
Time	всн	WD	WD-BCH	CW	pН	EC	DO	Temp	TDS	Additional Information
9:15	932	1500	568	N/A	6.28	0.25	4.84	18.13	0.161	Slight smell
8:30		6		N/A						Dry
8:35	1			N/A						Dry
8:50		1	1	N/A			5.51			Dry
		2480	1550	N/A	4.56	0.217	4.68	18.33	0.14	Sediment, tannins and smell
		1653	698	N/A	4.78	0.321	2.24	17.48	0.208	Sediment, tannins and smell
			535	N/A	4.77	0.28	5.34	19.89	0.181	Smell, coloured
				N/A						Dry
		1830	910	N/A	5.9	0.242	4.79	17.37	0.157	Slight colouration and smell
				40cm	5.78	1.05	4.66	14.22	0.675	20cm water depth, clear some sediments when disturbed
				N/A						Dry
				N/A						Dry
				1.5m	6.09	0.923	9.54	11.93	0.59	30cm Clear, slight tannin, flowin
	Down Road Time 9:15 8:30 8:35 8:50 9:45 10:00 10:25 9:22 10:55 10:10 10:20	Down Road Time BCH 9:15 932 8:30 8:35 8:35 930 9:45 930 10:00 955 10:25 965 9:22 9:22	Down Road Time BCH WD 9:15 932 1500 8:30 - - 8:35 - - 9:45 930 2480 10:00 955 1653 10:25 965 1500 9:22 - - 10:55 - - 10:10 - - 10:20 - -	Down Road Project No. Time BCH WD WD-BCH 9:15 932 1500 568 8:30	Down Road Project No. Time BCH WD WD-BCH CW 9:15 932 1500 568 N/A 8:30 N/A N/A N/A 8:35 N/A N/A 9:45 930 2480 1550 9:45 930 2480 1550 10:00 955 1653 698 10:25 965 1500 535 10:52 920 1830 910 10:55 40cm 10:10 N/A 10:20 N/A N/A 10:20	Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH 9:15 932 1500 568 N/A 6.28 8:30 N/A N/A 10:00 10:00 10:00 955 1653 698 N/A 4.56 10:25 965 1500 535 N/A 4.77 10:25 965 1500 535 N/A 4.77 10:52 920 1830 910 N/A 5.9 10:55 40cm 5.78 10:10 N/A N/A 10:20 N/A 10:20 <td>Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC 9:15 932 1500 568 N/A 6.28 0.25 8:30 N/A 1000 1000 1000 1000 1000 1000 1000 8:35 N/A N/A 10000 1000 1000 1000 1000 1000 1000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 100000 10000 10000</td> <td>Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC DO 9:15 932 1500 568 N/A 6.28 0.25 4.84 8:30 N/A N/A 8:35 N/A N/A</td> <td>Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC DO Temp 9:15 932 1500 568 N/A 6.28 0.25 4.84 18.13 8:30 N/A N/A</td> <td>Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC DO Temp TDS 9:15 932 1500 568 N/A 6.28 0.25 4.84 18.13 0.161 8:30 N/A N/A <</td>	Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC 9:15 932 1500 568 N/A 6.28 0.25 8:30 N/A 1000 1000 1000 1000 1000 1000 1000 8:35 N/A N/A 10000 1000 1000 1000 1000 1000 1000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 100000 10000 10000	Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC DO 9:15 932 1500 568 N/A 6.28 0.25 4.84 8:30 N/A N/A 8:35 N/A N/A	Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC DO Temp 9:15 932 1500 568 N/A 6.28 0.25 4.84 18.13 8:30 N/A N/A	Down Road Project No. MSC0137 Time BCH WD WD-BCH CW pH EC DO Temp TDS 9:15 932 1500 568 N/A 6.28 0.25 4.84 18.13 0.161 8:30 N/A N/A <

BCH = Bore Casing Height WD = Water Depth below casing WD-BCH = Groundwater level BGL

CW = Creek width

Notes:

Groundwater Monitoring Data Record Sheet

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Date	21	7/02/2018	Name of	recorder	Kathryn Kinn	ear				
Location	Down Road Project No. MSC0137								Solu	
Test ID	Time B	СН	WD	WD-BCH	pH E	С	DO	Temp	TDS	Additional Information
C502	1:10	N/A	N/A	N/A	6.34	0.623	5.14	21.89	0.4	10cm Depth running water.
SB09	1:35	1.0m	1660	660	4.03	0.296	2.22	19.87	0.192	
SB06	3:00	1.0m	1870	870	2.5	0.311	4.53	19.57	0.203	Coloured
SB07	3:10	1.0m	1640	640	2.82	0.337	3.9	19.69	0.224	Smell, coloured
C501	3:30	N/A	N/A	N/A	4.46	0.897	8.78	16.6	0.574	25cm Depth running water, clea
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BCH = Bore Casing Height WD = Water Depth below casing WD-BCH = Groundwater level BGL

Notes:



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Envirolab Services (WA) Pty Ltd trading as MPL Laboratories ABN 53 140 099 207 16-18 Hayden Court Myaree WA 6154 ph 08 9317 2505 fax 08 9317 4163 lab@mpl.com.au www.mpl.com.au

CERTIFICATE OF ANALYSIS 207409

Client Details Biodiverse Solutions Client Biodiverse Solutions Attention Kathyrn Kinnear Address Comparison of the second s

Your Reference	Biodiverse Solutions	
Number of Samples	5 Water	
Date samples received	01/03/2018	

Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

Please refer to the last page of this report for any comments relating to the results.

Report Details

Date results requested by

Date of Issue

09/03/2018

12/03/2018

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Results Approved By Joshua Lim, Operations Manager Michael Kubiak, Organics Supervisor

Authorised By

Todd Lee, Laboratory Manager

MPL Reference Revision No

207409 R00



Page | 1 of 15

Nutrients in Water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	S806	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date prepared	-	and 1996 (1997) (1997)	08/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
Date analysed	-		08/03/2018	08/03/2018	08/03/2018	08/03/2018	02/03/2018
Total Nitrogen	mg/L	0.1	1.0	3.0	1.1	0.2	0.3
Nitrate as N	mg/L	0.005	0.26	0.007	<0.005	0.024	0.27
Nitrite as N	mg/L	0.005	<0.005	<0.005	<0.005	<0.005	<0.005
Ammonia as N	mg/L	0.005	<0.005	<0.005	0.11	0.70	0.22
Total Phosphorus	mg/L	0.05	<0.05	0.26	<0.05	1.3	0.65
Phosphate as P	mg/L	0.005	<0.005	<0.005	<0.005	1.1	0.52

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Dissolved Metals in Water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	\$B09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date prepared	- -	i fem fruggi sug (gelerie).	07/03/2018	07/03/2018	07/03/2018	07/03/2018	07/03/2018
Date analysed	-		07/03/2018	07/03/2018	07/03/2018	07/03/2018	07/03/2018
Aluminium-Dissolved	mg/L	0.01	0.06	0.46	1.2	1.8	0.86
Arsenic-Dissolved	mg/L	0.001	<0.001	0.013	0.006	<0.001	<0.001
Cadmium-Dissolved	mg/L	0.0001	<0.0001	<0.0001	<0.0001	<0.0001	0.0002
Chromium-Dissolved	mg/L	0.001	<0.001	0.002	0.003	0.002	0.002
Copper-Dissolved	mg/L	0.001	<0.001	<0.001	0.002	<0.001	0.002
Iron-Dissolved	mg/L	0.01	0.86	40	2.8	0.90	1.1
Mercury-Dissolved	mg/L	0.00005	<0.00005	<0.00005	<0.00005	<0.00005	<0.00005
Manganese-Dissolved	mg/L	0.005	<0.005	<0.005	0.007	0.01	0.009
Nickel-Dissolved	mg/L	0.001	<0.001	<0.001	<0.001	0.003	<0.001
Lead-Dissolved	mg/L	0.001	<0.001	<0.001	<0.001	0.006	0.001
Zinc-Dissolved	mg/L	0.001	0.008	0.002	0.069	0.097	0.065

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vTRH(C6-C10)/MBTEXN in water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date analysed	-		02/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
TRH Cն - C₀	μg/L	10	<10	<10	<10	<10	<10
TRH C6 - C10	µg/L	10	<10	<10	<10	<10	<10
TRH C6-C10 less BTEX (F1)	μg/L	10	<10	<10	<10	<10	<10
МТВЕ	µg/L	1	<1	<1	<1	<1	<1
Benzene	μg/L	1	<1	<1	<1	<1	<1
Toluene	μց/Լ	1	<1	<1	<1	<1	<1
Ethylbenzene	μg/L	1	<1	<1	<1	<1	<1
m+p-xylene	µg/L	2	<2	<2	<2	<2	<2
o-xylene	µg/L	1	<1	<1	<1	<1	<1
Naphthalene	µg/L	1	<1	<1	<1	<1	<1 \
Surrogate Dibromofluoromethane	%		111	110	114	106	112
Surrogate toluene-d8	%		107	103	105	99	105
Surrogate 4-BFB	%		98	97	96	97	96

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Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwate
Date extracted	19 m 19 19 19 19 19 19 19 19 19 19 19 19 19		02/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
Date analysed	-		06/03/2018	06/03/2018	06/03/2018	06/03/2018	06/03/2018
TRH C10 - C14	µg/L	50	<50	<50	<50	<50	<50
TRH C15 - C28	µg/L	100	<100	<100	<100	<100	<100
TRH C29 - C36	µg/L	100	<100	<100	<100	110	330
TRH >C10 - C16	µg/L	50	<50	<50	<50	<50	<50
TRH >C10 -C15 less N (F2)	µg/L	50	<50	<50	<50	<50	<50
TRH >C16 - C34	µg/L	100	<100	<100	<100	140	280
TRH >C34 - C40	µg/L	100	<100	<100	<100	<100	220
Surrogate o-Terphenyl	%		84	85	94	37	19

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PAHs in Water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date extracted		en bri e te lete	02/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
Date analysed	-		07/03/2018	07/03/2018	07/03/2018	07/03/2018	07/03/2018
Naphthalene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Acenaphthylene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Acenaphthene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Fluorene	μg/L	0.1	<0.1	<0.1	<0.1	<0,1	<0.1
Phenanthrene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Anthracene	µg/L	0.1	<0,1	<0.1	<0.1	<0.1	<0.1
Fluoranthene	μg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Pyrene	μg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(a)anthracene	μg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Chrysene	μg/L	0,1	<0.1	<0.1	<0.1	<0,1	<0.1
Benzo(b,j+k)fluoranthene	µg/L	0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Benzo(a)pyrene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Indeno(1,2,3-c,d)pyrene	μg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Dibenzo(a,h)anthracene	μg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(g,h,i)perylene	μg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(a)pyrene TEQ	µg/L	0.5	<0.5	<0.5	<0.5	<0.5	<0.5
Total +ve PAH's	μg/L	0,1	<0.1	<0.1	<0.1	<0.1	<0.1
Surrogate p-Terphenyl-D14	%		78	76	88	24	14

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Method ID	Methodology Summary
INORG-055	Nitrite - determined colourimetrically. Soils are analysed from a water extract.
INORG-055	Nitrate - determined colourimetrically. Soils are analysed from a water extract.
INORG-055	Total Nitrogen by colourimetric analysis based on APHA 4500-P J, 4500-NO3 F.
INORG-057	Ammonia by colourimetric analysis based on APHA latest edition 4500-NH3 F.
INORG-060	Phosphate- determined colourimetrically. Soils are analysed from a water extract.
METALS-020	Metals in soil and water by ICP-OES.
METALS-021	Determination of Mercury by Cold Vapour AAS.
METALS-022	Determination of various metals by ICP-MS.
ORG-003	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-FID. F2 = (>C10-C16)-Naphthalene as per NEPM B1 Guideline on Investigation Levels for Soil and Groundwater (HSLs Tables 1A (3, 4)). Note Naphthalene is determined from the VOC analysis.
ORG-004	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS.
ORG-012	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS.
ORG-012	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS, Benzo(a)pyrene TEQ as per NEPM draft B1 Guideline on Investigation Levels for Soil and Groundwater.
ORG-016	Soil samples are extracted with methanol and spiked into water prior to analysing by purge and trap GC-MS. Water samples are analysed directly by purge and trap GC-MS. F1 = (C6-C10)-BTEX as per NEPM B1 Guideline on Investigation Levels for Soil and Groundwater.

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QUALITY	CONTROL	Nutrients	in Water			Duj	olicate		Spike Re	covery %
Test Description	Units	PQL	Method	Blank	#	Base	Dup,	RPD	LCS-1	[NT]
Date prepared	-			02/03/2018	:				02/03/2018	
Date analysed	-			02/03/2018	:				02/03/2018	
Total Nitrogen	mg/L	0,1	INORG-055	<0.1					96	
Nitrate as N	mg/L	0.005	INORG-055	<0.005					116	
Nitrite as N	mg/L	0.005	1NORG-055	<0.005					117	
Ammonia as N	mg/L	0.005	INORG-057	<0.005					100	
Total Phosphorus	mg/L	0.05	METALS-020	<0.05				And	103	
Phosphate as P	mg/L	0,005	INORG-060	<0.005					92	

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QUALITY	CONTROL: Dis	solved Met	als in Water			Du	olicate		Spike Re	covery %
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	207409-
Date prepared	-	,		07/03/2018	1	07/03/2018	07/03/2018		07/03/2018	07/03/201
Date analysed	-	A 100 Miles		07/03/2018	1	07/03/2018	07/03/2018		07/03/2016	07/03/201
Aluminium-Dissolved	mg/L	0.01	METALS-022	<0.01	1	0.06	0.06	0	109	77
Arsenic-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	103	108
Cadmium-Dissolved	mg/L	0.0001	METALS-022	<0.0001	1	<0.0001	<0.0001	0	104	109
Chromium-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	105	104
Copper-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	103	99
Iron-Dissolved	mg/L	0.01	METALS-022	<0.01	1	0.86	0.87	1	105	#
Mercury-Dissolved	mg/L	0.00005	METALS-021	<0.00005	1	<0.00005	<0.00005	0	102	104
Manganese-Dissolved	mg/L	0.005	METALS-022	<0.005	1	<0,005	<0.005	C	108	107
Nickel-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	103	98
Lead-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	٥	101	101
Zinc-Dissolved	mg/L	0.001	METALS-022	<0.001	1	0.008	0.008	0	103	104

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QUALITY CONTR	ol, vtrih(C	6-C10)/N	BTEXN in water		1	Duj	olicate		Spike Re	covery %
Test Description	Units	PQL	Method	Blank	#	Base	Dup,	RPD	LCS-1	[NT]
Date analysed	-			02/03/2018					02/03/2018	
TRH C₀ - C₀	µg/L	10	ORG-016	<10				an we want to be	95	and the second se
TRH C ₆ - C ₁₀	µg/L	10	ORG-016	<10					95	
мтве	µg/L	1	ORG-016	<1				-		
Benzene	µg/L	1	ORG-016	<1					110	
Toluene	µց/Լ	1	ORG-016	<1					103	
Ethylbenzene	μg/L	1	ORG-016	<1					89	
m+p-xylene	µg/L	2	ORG-016	<2					86	
o-xylene	μg/L	1	ORG-016	<1					87	
Naphthalene	µg/L	1	ORG-016	<1						
Surrogate Dibromofluoromethane	%		ORG-016	109					106	
Surrogate toluene-d8	%		ORG-016	107					105	
Surrogate 4-8F8	%		ORG-016	99					105	

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QUALITY CON	NTROL SVII	RH((C10=0	C40) in water			Duj	olicate		Spike Re	covery %
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	[NT]
Date extracted	-			02/03/2018	2	02/03/2018	02/03/2018		02/03/2018	
Date analysed	-			06/03/2018	2	06/03/2018	06/03/2018		06/03/2018	
TRH C10 - C14	µg/L	50	ORG-003	<50	2	<50	<50	0	73	
TRH C15 - C28	µg/L	100	ORG-003	<100	2	<100	<100	٥	88	
TRH C ₂₉ - C ₃₆	µg/L	100	ORG-003	<100	2	<100	<100	0	81	
TRH >C10 - C16	µց/Լ	50	ORG-003	<50	2	<50	<50	0	78	
TRH >C16 - C34	µg/L	100	ORG-003	<100	2	<100	<100	0	88	
TRH >C34 - C40	ին/Ր	100	ORG-003	<100	2	<100	<100	0	75	
Surrogate o-Terphenyl	%		ORG-003	97	2	85	101	17	80	

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QUALITY	CONTROL	: PAHs ir	Water			Dup	olicate		Spike Re	icovery %
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	[NT]
Date extracted	-			02/03/2018	2	02/03/2018	02/03/2018		02/03/2018	
Date analysed	-			07/03/2018	2	07/03/2018	07/03/2018		07/03/2018	
Naphthalene	μg/L	0,1	ORG-012	<0.1	2	<0,1	<0.1	0	94	
Acenaphinylene	រុច្វ/L	0,1	ORG-012	<0.1	2	<0.1	<0.1	0		
Acenaphthene	µg/L	0.1	ORG-012	<0.1	2	<0,1	<0.1	0		
Fluorene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	108	
Phenanthrene	μg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	115	
Anthracene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Fluoranthene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	114	
Pyrene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	112	
Benzo(a)anthracene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Chrysene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	100	
Benzo(b,j+k)fluoranthene	μg/L	0.2	ORG-012	<0.2	2	<0.2	<0.2	0		
Benzo(a)pyrene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	o	72	
Indeno(1,2,3-c,d)pyrene	μg/L	0,1	ORG-012	<0,1	2	<0,1	<0.1	0		
Dibenzo(a,h)anthracene	μg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		arrows a A car second
Benzo(g,h,i)perylene	hð\r	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	Name	
Surrogate p-Terphenyl-D ₁₄	%		ORG-012	91	2	76	77	1	74	

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Result Definiti NT	Not tested		:
NA	Test not required	÷	
INS	Insufficient sample for this test		
PQL	Practical Quantitation Limit		
<	Less than		
	Greater than		
RPD	Relative Percent Difference		
LCS	Laboratory Control Sample		
NS	Not specified		·
NEPM	National Environmental Protection Measure		:
NR	Not Reported		
Quality Contro	ol Definitions		
Blank	This is the component of the analytical signal which is not derived from the sample but from glassware etc, can be determined by processing solvents and reagents in exactly the same samples.		
			-

DuplicateThis is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected
should be one where the analyte concentration is easily measurable.A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike

Matrix Spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.

LCS (Laboratory This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified Control Sample) with analytes representative of the analyte class. It is simply a check sample.

Surrogate Spike Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

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2**0**7409 R00

Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.

Report Comments

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#4,5 - PAH: Surrogate recovery was low due to sample emulsifying during extraction

Percent recovery not available due to the analyte signal being much greater than the spike amount. An acceptable recovery was achieved for the LCS.

#4,5 for Nox PQL raised due to sample matrix. Very dark samples

MPL Reference: Revision No

207409 R00

13:00 | 15 of 15

Groundwater Monitoring Data Record Sheet

Date	4/09/2018	Name of recorder	Bianca Theyer / Chiquita Cramer	
Location	Down Road	Project No.	MSC0137	Solutions

Test ID	Time	BCH (cm)	WD (cm)	WD-BCH (cm)	pН	EC (mg/cm)	DO (mg/L)	Temp (C°)	TDS	Additional Information
SB9	9:35	92.7	136.8	44.1	5.86	0.389		17.2	0.253	Lightly coloured brown
SB12	10:28	85	189	104	7.52	0.077		16.55	0.05	Lots of sediment, lightly coloured brown
SB8	10:48	95	113	18	4.41	1.2	2.57	15.86	0.768	Moderate amount of sediment, brown in colou
SB6	11:17	93	93	0	4.16	1.07	8.95	14.23	0.686	Moderate amount of sediment, brown in colou
SB7	11:35	91	135	44	4.5	0.211		15.55		Moderate to high amount of sediment, brown in colour
CS1	12:02	N/A	10	N/A	5.68	0.885	3.93	14.91	0.566	Clear water, creek flowing
SB3	12:29	92	213	121	6.09	0.963	2.07	16.73	0.616	Lightly coloured brown
SB4	12:35	90.6	121	30.4	5.38	0.328	1.93	16.12	0.213	Lightly coloured brown
CS2	12:48	N/A	20	N/A	6.09	0.659	7.83	12.35	0.422	clear water, creek flowing

BCH = Bore Casing Height WD = Water Depth below casing WD-BCH = Groundwater level BGL

CW = Creek width

Notes:

Appendix D

Conceptual hydrogeological model

A-4 Conceptual hydrogeological model

A Conceptual Site Model was completed to assess the connectivity between shallow and deeper hydrogeological features of the Site and surrounds, and to identify key pathways for transport of potential contaminants in surface and groundwater, and potential receptors based on site

A-4-1 Sources of information

- Local shallow soil setting from Motorplex Development, Down Road Surface and Groundwater Monitoring 2018 Summary Report (Bio Diverse Solutions 2018)
- Regional hydrogeological setting from Albany hinterland prospective groundwater resources map (Ryan, Yesertener, Maughan, & Thornton, 2017)
- Shallow soil profile descriptions
- Deep groundwater bore

A-4-2 Local shallow hydrogeology

The typical local surficial geology is presented in Plate 3, and shows the following features:

- A thin shallow sandy/silty layer up to 1 meter thick overlies the Pallinup formation in areas leading to the creek, while on the upper-slopes lateritic gravels/cobbles predominate.
- Underlying the sandy/silty layer, the Pallinup formation comprises silty clays which appears to extend to 25 meters blow the ground level.
- Although not tested, the permeability of the upper sandy/silt is likely higher than the underlying Pallinup Formation (silty clays) which may result in temporary perching of shallow groundwater in the sandy/silt (particularly during winter rainfall).
- Shallow groundwater levels derived from the monitoring of the shallow bores indicates that the levels appear to vary seasonally up to 1 meter.
- Shallow groundwater flow within the sandy/silty layer (and upper parts of the Pallinup Formation) are inferred as towards the creek line where groundwater is inferred to discharge.

A-4-3 "Deeper" hydrogeology

The deeper hydrogeology setting is presented on the cross section and shows the following features:

- The site (shallow hydrogeology) is underlain by approximately 25 metres of the Pallinup formation, deemed to comprise silt, sand and clay (Ryan *et al.* 2017). The Pallinup aquifer is inferred to contain minor water resources and exhibits a low permeability.
- The Pallinup Formation is underlain by the Werillup Aquitard described as comprising clay, silt and sand and which is deemed to hydraulically separate the overlying Pallinup Formation with underling units (Ryan et al, 2017). The drilling logs indicates that the thickness of the Werillup aquitard is 31 meters and comprises predominantly clay. Based on map notes (Ryan *et al.* 2017) the Werillup aquitard is inferred as extensive throughout the King River area and likely lies below all areas of the site and beyond.
- Werillup aquitard is probably underlain by granite, based on evidence of minor cuttings returned to the surface exhibiting angular quartz and some mica.
- The groundwater levels of the Pallinup formation appears to be similar to the shallow groundwater levels.
 That is to say that, excluding times when winter rainfall may perch shallow groundwater, the shallow sandy silts are probably hydraulically connected with the Pallinup Formation.
- The groundwater flow direction of the Pallinup Formation is not well known, however, beneath the Site groundwater it is likely to follow the regional topography, and flow towards the south west where groundwater is likely to discharge into the rivers and creeks, such as dominant surface water feature in areas close to the Site - Marbelup Brook.

A-4-4 Discussion/interpretations on pathway

The hydrogeological setting indicates the following Conceptual Site Model:

- The depth to groundwater plan indicates that in areas adjacent to the surface water creek/ feature, the depth to groundwater is less than 2 metres. In these areas, it is considered that there is an increased risk of impacts to groundwater from surface contaminants and spills given the thin geological profile (e.g. low adsorptive capacity).
- The shallow groundwater migration direction (shallow sands/silt and Pallinup Formation) indicates that any Site based groundwater impacts should migrate towards the creek line (on Site) where groundwater (and any impacted groundwater) is inferred to discharge. Any impacted surface water will migrate towards areas offsite and discharge into the major drainage of the area, the Marbelup Brook.
- Any Site based groundwater impacts should preferentially migrate within shallow sands/silts (towards the creek lines) and not migrate downwards into the deeper levels of the Pallinup Formation given the similar groundwater levels between the Pallinup Formation and the overlying shallow sandy silts, and that the shallow sandy silts have a higher permeability than the Pallinup Formation
- Given the low permeability of the Pallinup Formation, any Site based groundwater impacts, which may
 migrate downwards into the Pallinup formation should be subject to attenuation processes, which should limit
 the extent and migration rate of the any impacts.
- It appears from the limited drilling information (one monitoring well) that the Pallinup Formation is underlain by the Werillup Aquitard and granite, which should constrain any potential groundwater impacts to the Pallinup Formation.

A-4-5 Potential receptors

The Conceptual Site Model indicates that Site groundwater impacts will migrate towards the on-site creek, the receptors comprise the following:

- the environment of the onsite creek (flora and fauna)
- creek systems down-gradient of the site (flora and fauna)
- groundwater bore users where bores are located close to, and are in hydraulic connection, with the creek system
- surface water users/abstraction of surface water; and
- livestock accessing creek.

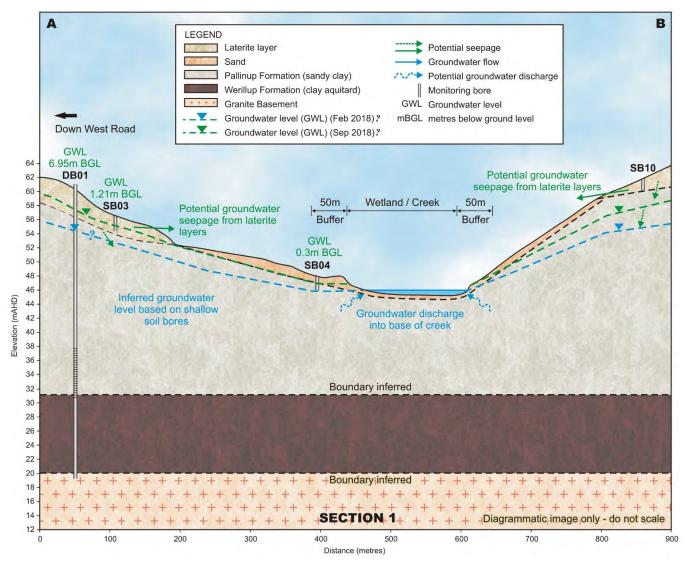


Plate 3 Preliminary hydrogeological section 1 (A-B)

Appendix E

Potential water users

- Figure E.1 Potential surface water users
- Table E.1 Licensed groundwater abstractions

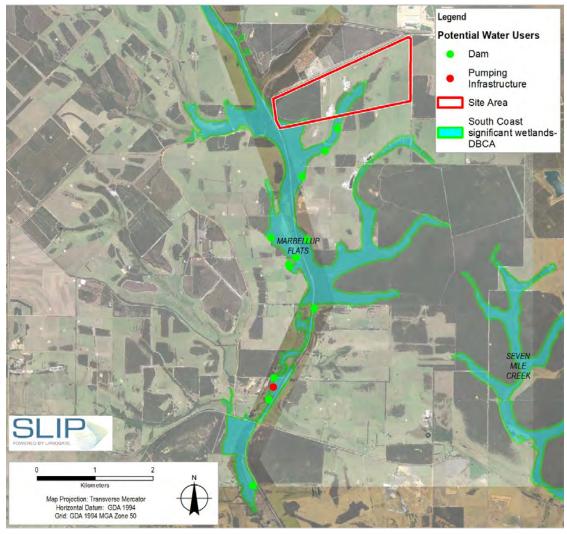


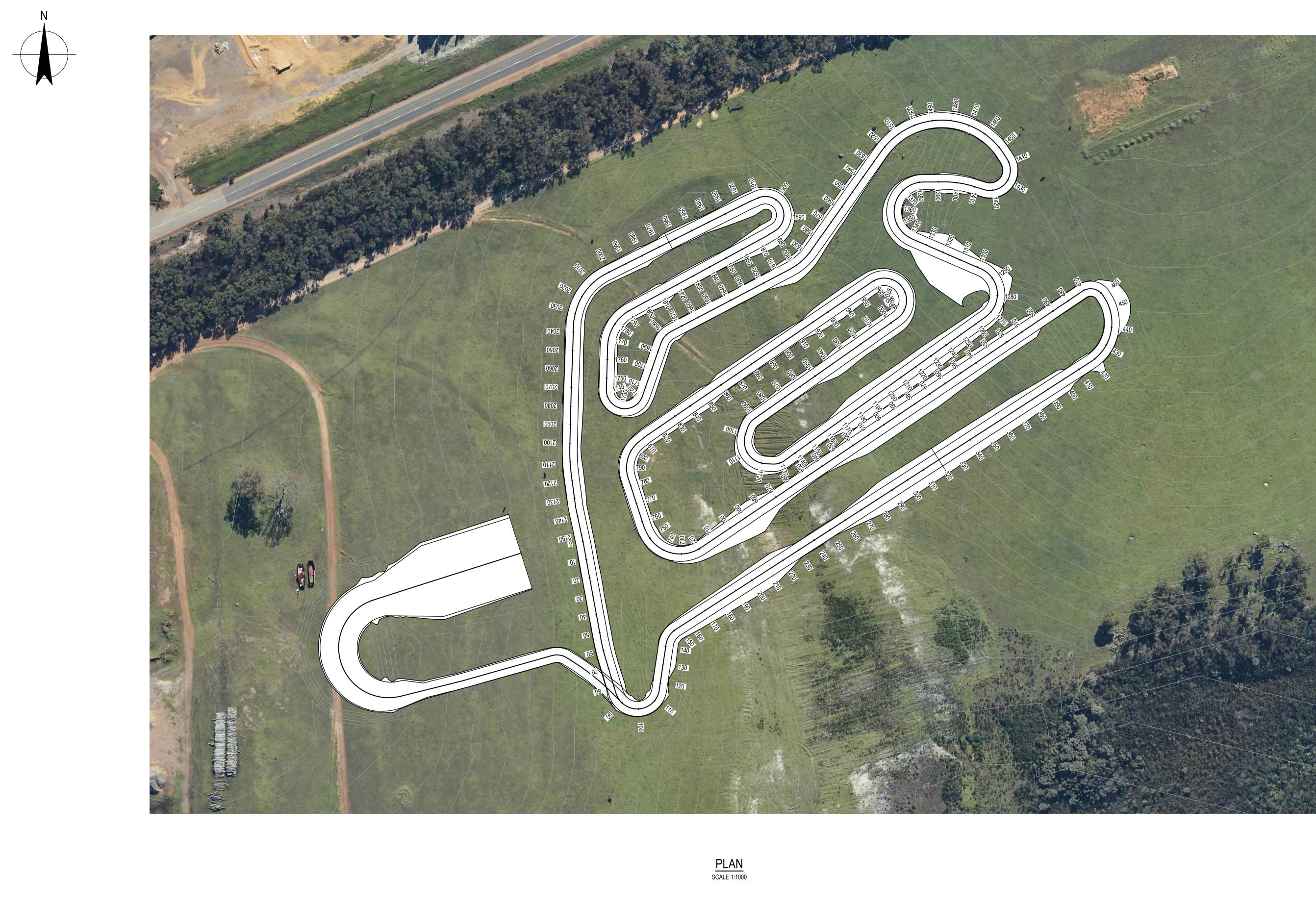
Figure E.1 Potential surface water users

Table E.1	Licensed arou	ndwater abstractions

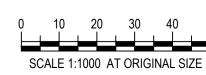
Licence No.	Licence allocation (kL/yr)	Expiry date	Location	Aquifer
168308	4000	31/8/2028	Project Site Lot 5780 Down Road, Drome	168308
156374	1400	30/09/2024	Lot 7235 Marbelup ~3.5 km downgradient	156374
76457	33200	8/04/2020	Lot 500 Marbelup ~6.5 km downgradient	76457
160280	1000	13/05/2026	Lot 86 Elleker Crown Reserve ~8 km downgradient	Bremer West <i>–</i> Superficial
155130	26000	20/10/2022	Lot 200 Lower Denmark Rd Elleker ~9.5 km downgradient	Bremer West – Sedimentary
173352	2100	16/05/2021	Wilgie Rd, Torbay	Bremer West <i>–</i> Superficial

Appendix F

Motocross track drawings



Rev Des	cription		Checked	Approved	Date
Author	B SHAW	Drafting Check			
Designer	B SHAW	Design Check			



Plot Date: 12 August 2021 - 1:34 PM Plotted by: Bradley Shaw

File Name: C:\12d\SW\data\P-00-12D-001\61-12546218 - Albany Motorsport Park DA_1367\CADD\Drawings\12546218-C001.dwg





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Client CITY OF ALBANY

Project No.

Project ALBANY MOTORSF MX TRACK Status PRELIMINARY

PORTS PARK	Drawing PLAN Title	Size A1
Status Code	Drawing No. 12546218-C001	Rev

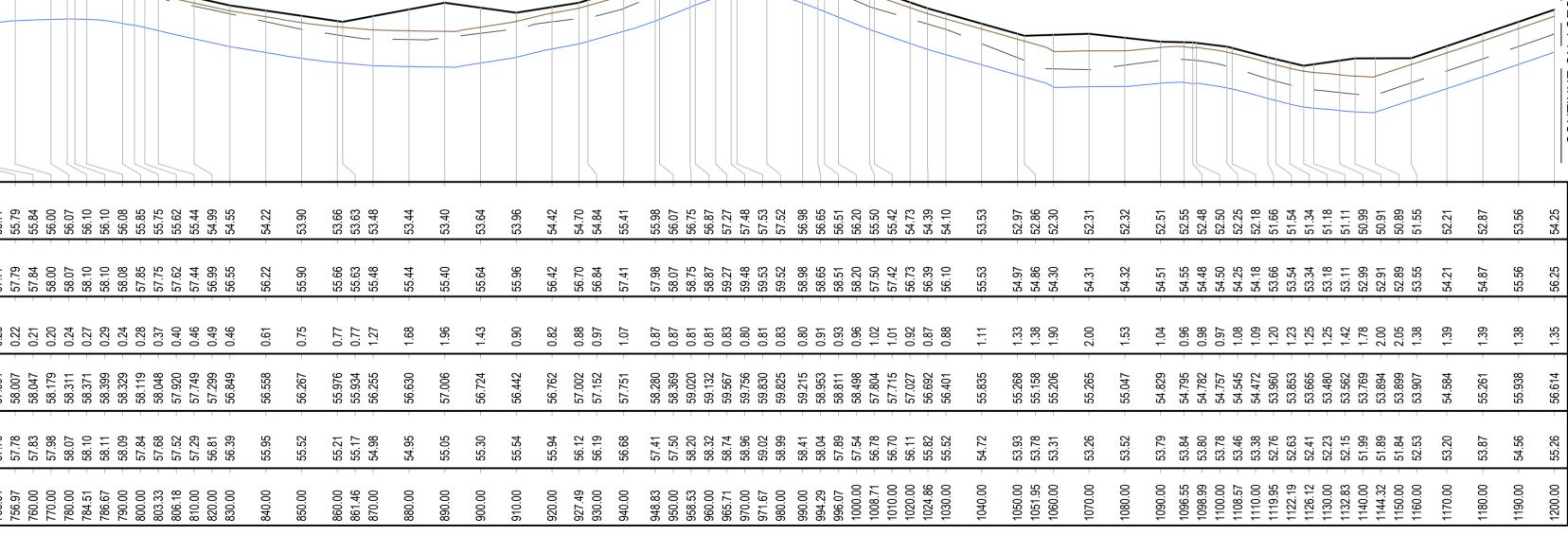
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GROUNDWATER	57.89 57.85 57.85 57.85 57.85 57.85 57.56 57.56 57.40 57.56 57.31 57.50 57.33 56.95 56.95 56.95 56.69 56.69 55.50 55.50 55.50 55.51 55.53 55.53 55.53 55.37 55.57	55.21 55.07 55.07 55.03 55.03 54.72 54.62 54.50 54.50 51.23	50.17 50.52 50.71 51.25 51.86 51.86 52.56 52.56 53.28 54.00 54.00	55.91 56.87 57.75 57.75 59.81 59.17 59.36 60.36 60.35 60.35 61.37 61.37 62.11 62.13 62.13 61.37 62.13 61.82 61.53
BULK EARTHWORKS SURFACE LEVEL		57.21 57.27 57.07 57.05 56.72 56.62 56.62 56.62 56.62 56.50 56.50 57.03 56.50 51.33 51.13 51.20 51.20 51.20 51.20 51.20		
LEVEL DIFFERENCE CUT - / FILL +	0.32 0.36 0.36 0.36 0.36 0.36 0.33 0.33 0.33		1.63 1.50 1.51 1.51 1.53 1.49 1.49 1.43 1.43 1.43 1.43 1.43 1.43 1.43 1.43 1.43	1.32 1.32 1.27 1.27 1.27 1.30 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.11 1.10 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.12 1.13 1.12 1.14 1.12 1.15 1.12 1.12 1.12 1.12 1.12 1.13 1.12 1.14 1.12 1.15 1.12 1.12
TRACK DESIGN SURFACE LEVEL	60.620 60.559 60.551 60.452 60.452 60.339 60.339 60.339 60.339 60.339 60.136 60.136 60.136 60.136 60.096 60.012 59.739 59.739 59.739 60.000 60.000 60.000 60.000 59.467 59.247 59.238 59.639 59.738 50.000	57.204 - 57.569 - 57.569 - 57.512 - 57.512 - 57.512 - 57.512 - 57.217 - 57.2039 - 57.2039 - 56.080 - 56.080 - 56.272 - 56.080 - 56.272 - 55.360 - 55.360 - 55.360 - 55.360 - 55.360 - 55.360 - 55.360 - 55.360 - 55.244 - 551.361 - 55.244 - 551.361 - 55.244 - 551.361 - 552.244 - 551.361 - 552.244 - 551.361 - 552.244 - 552.252 - 552.247 - 552.247 - 552.247 - 552.247 - 552.247 - 552.247 - 552.247 - 552.247 - 552.247 - 552.247 - 552.247 - 552.244 - 552.547 - 552.547 - 552.547 - 552.547 - 555.547 - 555.547 - 555.547 - 555.557 - 555.557 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.5575 - 555.55755 - 555.5575 - 555.5575 - 555.55755 - 555.55755 - 555.5575555755	52.593 - 52.820 - 53.048 - 53.700 - 54.352 - 55.005 - 55.298 - 56.298 - 57.246 -	58.178 - 59.110 - 59.110 - 60.043 - 60.043 - 60.715 - 60.715 - 61.377 - 61.377 - 61.377 - 61.000 - 67.
EXISTING SURFACE LEVEL	60.30 60.20 60.19 60.10 60.10 60.10 60.110 59.87 59.73 59.74 59.33 59.42 59.33 59.42 59.42 59.33 59.33 59.42 59.33 59.33 57.42 57.38 57.38	57.27 57.16 57.16 57.14 57.13 56.56 56.56 56.56 55.66 55.66 56.56 56.56 51.24 51.60 51.60 51.24 50.31 50.31 50.31 49.61 49.61 49.87 49.94	50.96 51.32 51.53 52.17 52.86 53.54 54.89 54.89 55.88	56.86 57.84 58.75 58.75 58.75 59.62 60.43 61.44 61.44 61.44 61.80 61.44 61.80 62.31 62.31 62.31 62.33 63.36 64.00 64.00 63.53 63.53 63.53 63.53
CHAINAGE	10.00 20.00 21.33 21.33 30.00 40.00 50.00 57.85 53.43 53.43 57.85 64.48 70.00 70.00 83.88 87.50 93.53 111.25 111.25 120.00	130.00 130.00 140.00 151.44 150.00 151.44 150.00 150.00 187.69 187.69 187.69 187.69 187.69 187.69 187.69 190.00 2216.00 2216.00 2216.00 2216.00 2216.00 2210.00 2210.00 2210.00 2210.00	270.00 276.51 280.00 300.00 310.00 329.84 3340.00	350.00
	IGITUDINAL SECTION - PART 1 1:1000 VERT 1:200			

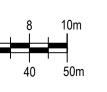
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DATUM RL. 47.00																						
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BULK EARTHWORKS SURFACE LEVEL	55.06	54.38	- 23.77	53.53	00.20 70 73	- SC.2C	52.18	52.40	52.59	52.63		53.61	54.10	54.65	55.14 55.20	56.06	56.57	56.87	57.55	57.64	57.71	- <u></u>
LEVEL DIFFERENCE CUT - / FILL +	1.32 -	1.33	1.34	1.34 -	1.47	- 17.1	1.84	1.57	1.30	1.24	49	1.01	1.20	0.82 -	0.56	0.34 -	0.21	0.20	0.35 -	0.37	0.30	0.23 -
TRACK DESIGN SURFACE LEVEL	- 55.471	54.798	54.125 -	53.833 -		53.143 	53.037 -	52.990 -	52.942	52.932 -	- 70.00	53.890	54.435 -	54.973 -	55.452 55.512	56.350 -	56.866 -	57.141 -	57.826 -	57.935	57.961 -	57.991 -
EXISTING SURFACE LEVEL	54.15 -	53.46	- 22.79	52.50 -	11.20	- ++·.1c	51.20 -	51.42	51.64	51.69 -	00.10	67.29	53.24 -	54.15 -	54.89 54 q8	56.01 -	56.66	56.94	57.48	57.57	57.66 -	57.76 -
CHAINAGE	- 00.009	610.00	620.00	624.32 -		040.00 	650.00 -	- 00.099	- 00.02	672.11 -		690.00	- 00.00	710.00	720.00	730.00	736.00 -	740.00	750.00	751.59 -	753.55 -	755.81 -

LONGITUDINAL SECTION - PART 2

HORZ 1:1000 VERT 1:200

Rev Des	scription	Checked Approved	Date	VERTICAL 1:200 0 2 AT ORIGINAL SIZE HORIZONTAL 1:1000 AT ORIGINAL SIZE 0 10	4 6 4 7 20 30	8
Author Designer	B SHAW B SHAW	Drafting Check Design Check				
Plot Date:	12 August 2021 - 11:4	6 AM Plotted by: Bradley Shaw		File Name: C:\12d\SW\data\P-00-12D-001\61-12546218 - Albany Motorsport Park DA_1367\CADD\Drawings	12546218-C	002.dwg







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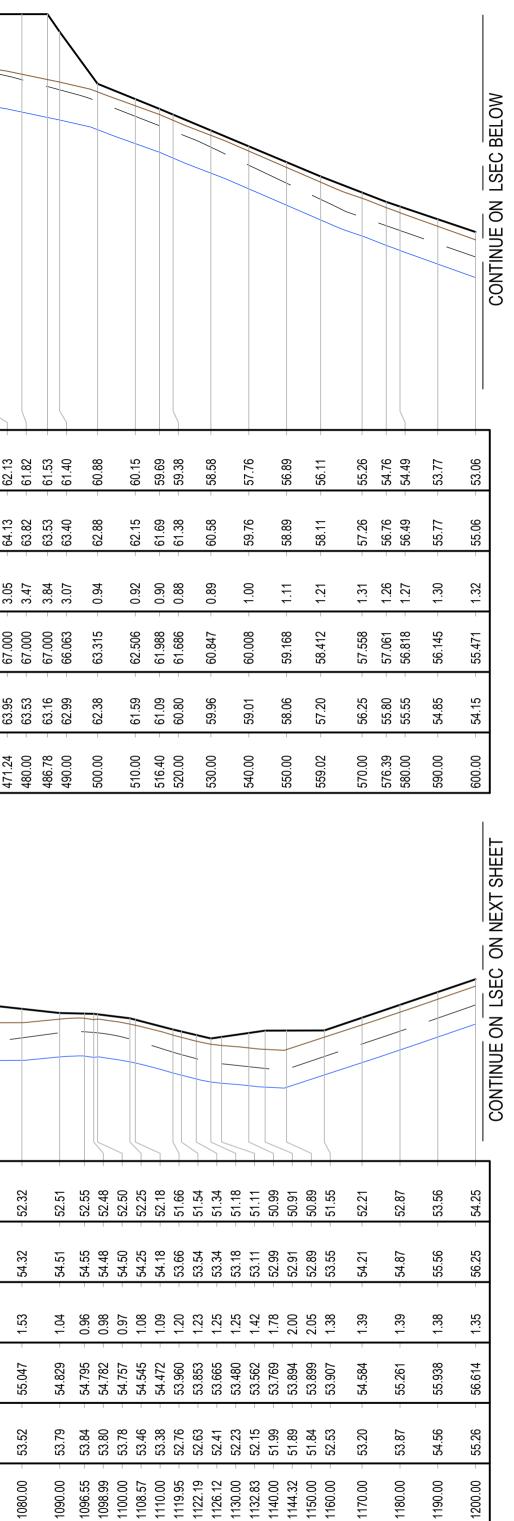
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Project ALBANY MOTORSPORTS PARK MX TRACK Status PRELIMINARY



Drawing LONGITUDINAL SECTION SHEET 1 OF 2

Status Code

Size **A1**

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LLACK DESIGN SUBLACE TEAT ADVERTING VOID 57.291 57.291 57.291 57.291 57.291 57.291 58.802 58.802 61.673 60.384 61.673 60.384 61.673 60.384 61.673 61.966 61.673 61.966 61.673 61.966 61.673 61.966 61.300 61.300	61.245 - 61.133 -
EXISLING Snute Field in the second se	60.81 - 60.71 -
CHAINAGE 1230.00 1250.00 1230.00 1230.00 1336.70 1336.70 1336.70	1340.00 - 1346.67 -

LONGITUDINAL SECTION - PART 3

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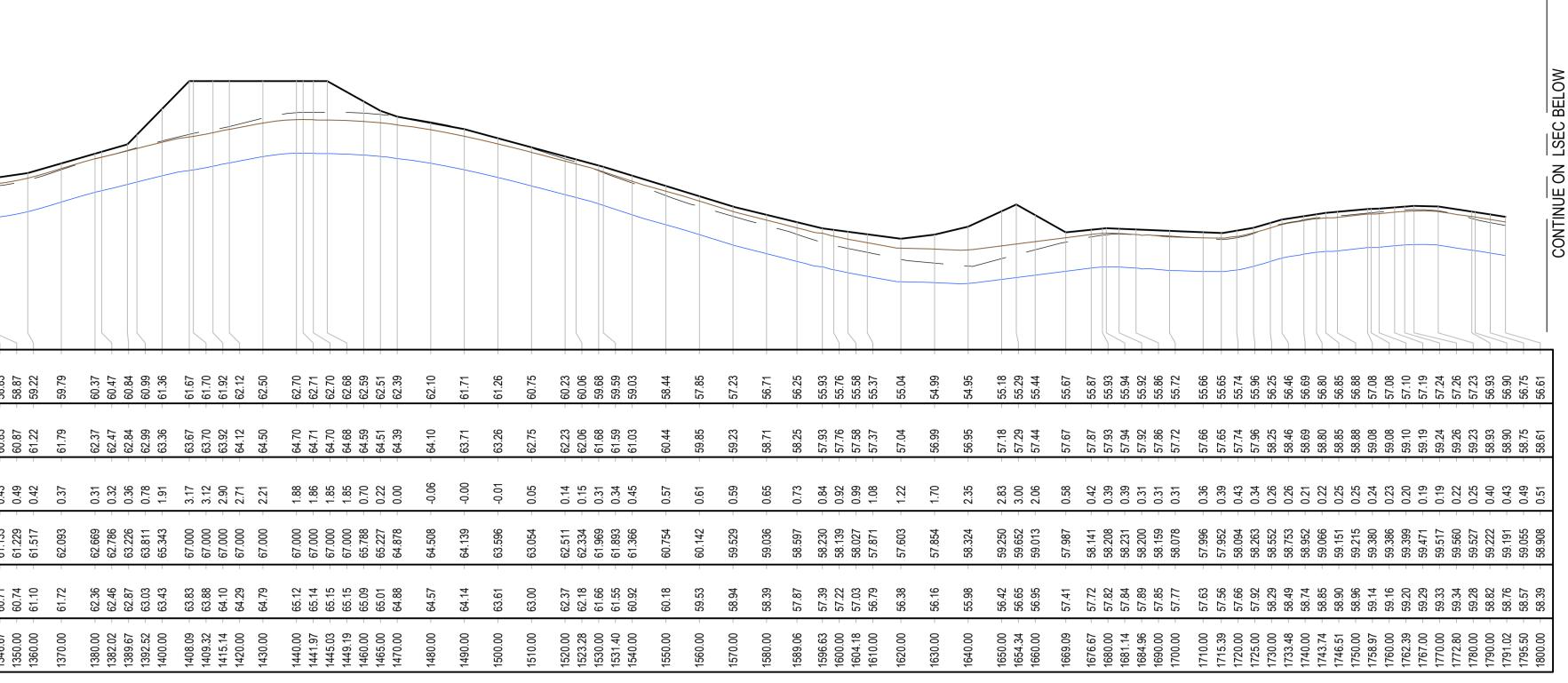
																			-						
DATUM RL. 52.00																									
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BULK EARTHWORKS SURFACE LEVEL	58.61 -	58.45 - 58.37 -	- 10.00	58.25 50.10	20.10	58.01 -	- 0.00	57.90 -	- CV./C	- 00.86	58.24 -	58.29	58.46	58.60 -	58.71 -	58.87 -	59 21	59.27	59.30	59 19	2	59.07 -	58.95 -	58.90 58.83	0.00
LEVEL DIFFERENCE CUT - / FILL +	0.51 -	0.55	0./3	1.09	00.1	3.00 2.88	22	2.44			1.55 -	1.50	1.27	1.03	0.89	0.82	0 59	0.63	0.67	0 88		1.33 –	1.78	1.99	7.01
TRACK DESIGN SURFACE LEVEL	58.908 -	58.754 -	- 07/.00	58.689	23.124 60.007	59.830	0000	58.921	- 404.02	- /94.40	58.541 -	58.578	58.750 -	58.922	59.008	59.168	50 487	59.567	59.602	59 484	2	59.366 -	59.249	59.195 59.708	00.1.80
EXISTING SURFACE LEVEL	58.39 -	58.20 -	- +6.10	57.60 -	- ++. /C	56.95	0.00	56.48 -	- /100	- /0.0C	56.99	57.08	57.48	57,89	58.12	58.35	58 QU	58.94	58.93	58 60		58.03 -	57.46	57.21 - 57.04 -	+0. JC
CHAINAGE	1800.00 -	1804.71 -	00.0101	1816.76	1020.00	182/.18 - 1830.00 -	0	1840.00 -	- 40.040.14		1857.84 -	1860.00	1870.00 -	1880.00	1885.00 -	1890.00 -	1900 00	1902 50 -	1910.00	1920.00		1930.00 -	1940.00	1944.53 - 1950.00 -	1 200.00

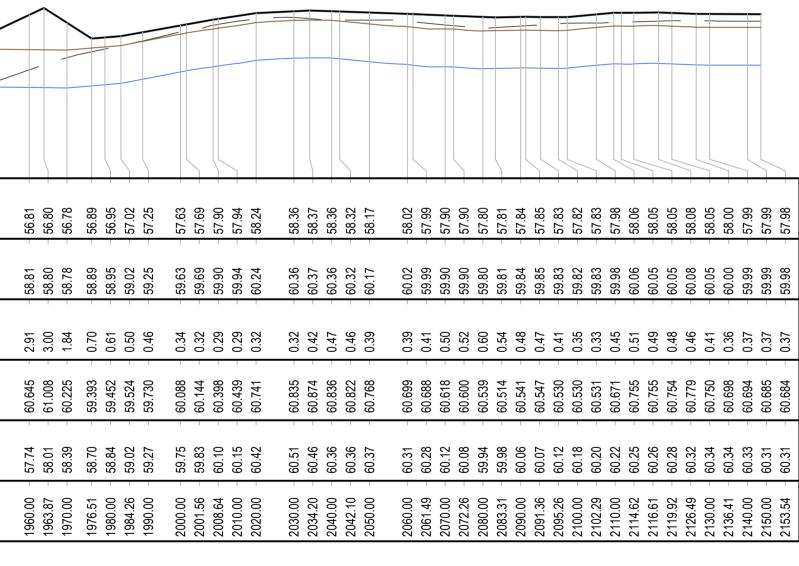
LONGITUDINAL SECTION - PART 4

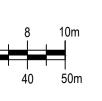
HORZ 1:1000 VERT 1:200

Poy Description
Description · B SHAW er B SHAW

Plot Date: 12 August 2021 - 11:46 AM Plotted by: Bradley Shaw









166 Stirling Terrace Albany WA 6330 **T** 61 8 9840 5100 **F** 61 8 6222 8555 **E** permail@ghd.com.au **W** www.ghd.com



Project No.

Client CITY OF ALBANY

Project ALBANY MOTORSF MX TRACK Status PRELIMINARY

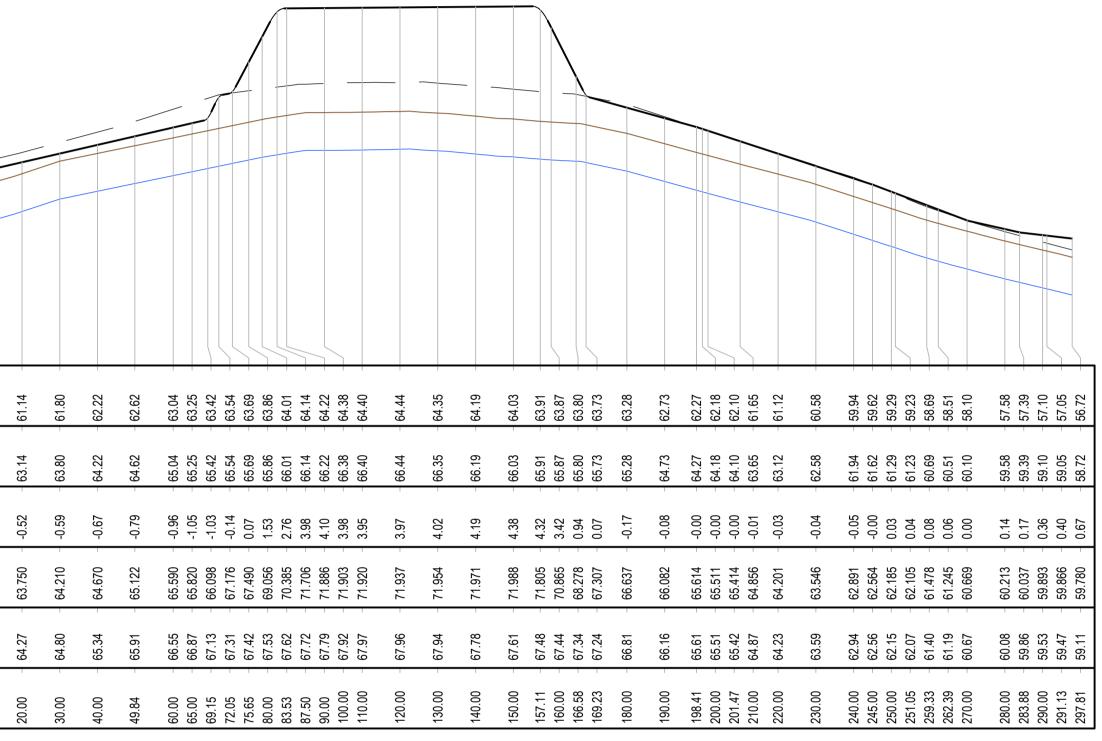
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PORTS PARK	Drawing PLAN Title LONGITUDINAL SECTION SHEET 2 OF 2	Size A1
Status Code	Drawing No. 12546218-C003	Rev

DATUM RL. 53.00			
GROUNDWATER	59.98	60.55	
BULK EARTHWORKS SURFACE LEVEL	61.98 -	62.55 -	
LEVEL DIFFERENCE CUT - / FILL +	-0.24 -	-0.62	
TRACK DESIGN SURFACE LEVEL	62.830 -	63.290 -	
EXISTING SURFACE LEVEL	63.07 -	63.91	
CHAINAGE	- 00.0	- 10.00	

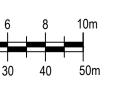
				VERTICAL 1:200 0 2 4 6 8 AT ORIGINAL SIZE HORIZONTAL 1:1000
Rev Des	scription	Checked Approved Date		AT ORIGINAL SIZE 0 10 20 30 40
Author	B SHAW	Drafting Check		
Designer	B SHAW	Design Check		
Plot Date:	12 August 2021 - 11	46 AM Plotted by: Bradley Shaw	File Name:	C:\12d\SW\data\P-00-12D-001\61-12546218 - Albany Motorsport Park DA_1367\CADD\Drawings\12546218-C005.dwg

Plot Date: 12 August 2021 - 11:46 AM Plotted by: Bradley Shaw



LONGITUDINAL SECTION - MX ENTRY STAGE HORZ 1:1000 VERT 1:200







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Client CITY OF ALBANY

Project No.

Project ALBANY MOTORSF

MX TRACK Status PRELIMINARY

PORTS PARK	Drawing Title LONGITUDINAL SECTION MX ENTRY STAGE	Size A1
Status Code	Drawing No. 12546218-C005	Rev

Appendix G DRAINS modelling results schematics

Summary of DRAINS R		Wetcal	ral .		ak Inflow			Book Out	low	.	k Store !!	 Vol	<u> </u>	ritical Dur	
Basin	1EY	Water Lev		1EY		40/ 450		Peak Outf		1EY	ak Stored				
East-B1	58.78	10% AEP 58.88	1% AEP 59.06	0.052	10% AEP 0.225	0.635	1EY 0.032	10% AEP 0.196	1% AEP 0.464	231	10% AEP 278		6hr	2hr	30n
East-B2	57.22	57.55	57.65	0.052	0.225	0.655	0.002	0.055	0.464	121	362			3hr	1hr
East-B3	70.27	70.56	70.75	0.072	0.272	0.647	0.000	0.031	0.282	110				1hr	1hr
East-B4	71.18	71.34	71.41	0.227	0.729	1.088	0		0.201	53	117				15n
East-B5	66.82	67.1	67.23	0.24	0.335	0.792	0.021	0.174	0.464	417	666		3hr	2hr	1hr
East-B6	61.19	61.4	61.61	0.032	0.534	1.834	0.018	0.405	0.628	127	300			2hr	30
East-B7	65.53	65.66	65.97	0.329	0.386	1.241	0.04	0.287	0.679	223	298			2hr	9h
East-B8	70.58	70.77	71.03	0.024	0.069	0.2	0	0	0.02	21	81	191	1hr	3hr	9h
East-B9	63.02	63.3	63.65	0.042	0.163	0.499	0		0.255	18	314			3hr	2h
East-B10	62.14	62.36	62.52	0.04	0.286	0.977	0.02	0.189	0.55	64				2hr	30
West-B1	66.21	66.69	66.7	0.014	0.115	0.32	0	0.083	0.113	22	97		9hr	9hr	9h
West-B2	62.3	62.39	62.43	0.137	0.269	0.435	0.014		0.116	79	121			45min	15
West-B3	62.91	63.25	63.31	0.057	0.145	0.269	0	0.038	0.146	79	168			3hr	30
West-B4	59.53	59.61	59.68	0.086	0.198	0.401	0.044		0.361	77	93			30min	15
West-B5	53.92	54.13	54.25	0.057	0.296	0.641	0.029	0.242	0.582	55			3hr	1hr	30
West-B6 West-B7	58 51.85	58.42 52.3	58.57 52.44	0.056	0.044 0.326	0.158	0	0.138	0.069	0	67 500		- 6hr	3hr 3hr	2h 2h
West-D/	51.05	52.5	52.44	0.050	0.320	0.724	0	0.130	0.529	101	500	027	OIII	311	211
							Flow		Water	Denth					+
Drains/swales	Shape	Slope	Depth	Length	10% flow	1EY	10% AEP	1% AEP	1EY	10% AEP	1% AEP				+
E-B1-01	1:6 swale	0.51	0.406	83	0.037	0.01	0.037	0.092	0.065	0.106	0.144				+
E-B1-02A	1:6 swale	0.54	0.448	130.5	0.052	0.003	0.052	0.212	0.052	0.148	0.244				-
E-B1-02B	1:6 swale	2.78	0.41	28.8	0.057	0.005	0.057	0.233	0.045	0.11	0.186				
E-B1-03A	1:6 swale	2.1	0.501	142.8	0.189	0.077	0.189	0.352	0.149		0.253		1		
E-B1-03B	1:6 swale	2.08	0.474	312.1	0.17	0.047	0.17	0.431	0.108		0.247				
E-B1-04	1:4 swale	0.54	0.44	184.8	0.024	0	0.024	0.104	0	0.14	0.23				
E-B1-04-CONNECT	Dummy OF	3.25	0.428	92.4	0.02	0	0.02	0.077	0		0.201				
E-B2-01	1:4 swale	4.23	0.459	142	0.125	0.027	0.125	0.338	0.089	0.159	0.231				T
E-B2-02	1:6 swale	5.28	0.428	56.8	0.116	0.027	0.116	0.317	0.074	0.128	0.185				
E-B3-01	1:6 swale	1.26	0.437	118.7	0.067	0.023	0.067	0.171	0.092	0.137	0.249				
E-B3-02	1:6 swale	0.53	0.861	112.9	0.132	0.051	0.132	0.291	0.265	0.561	0.749				
E-B4-01	K300, 0.4m deep	0.5	0.57	150.2	0.09	0.046	0.09	0.15	0.161	0.27	0.405			I	-
E-B4-02	1:4 swale	0.9	0.586	211.6	0.248	0.113	0.248	0.436	0.228	0.286	0.348			I	+
E-B5-01	1:4 swale	2.56	1.291	159.6	0.113	0.057	0.113	0.228	0.574	0.991	1.247		-	I	+
E-B5-02	1:4 swale	1.49	1.291	375.5	0.53	0.256	0.53	0.946	0.574	0.991	1.247	l	-	I	+
E-B6-01 E-B6-02	1:6 swale	3.87	0.699	142	0.094	0.007	0.094 0.051	0.32	0.19	0.399	0.614				+
=-B6-02 E-B6-03	1:4 swale 1:6 swale	5.3 0.8	0.699	158.6 310.6	0.051	0.005	0.051	0.18	0.19	0.399	0.614				+
E-B7-01	1:4 swale	0.8	0.508	74.5	0.138	0.023	0.098	0.055	0.092	0.399	0.304				-
E-B7-01	1:6 swale	0.67	0.408	160.6	0.098	0.023	0.098	0.285	0.092	0.208	0.304				-
E-B7-02	1:6 swale	1.16	0.408	129.3	0.025	0.021	0.025	0.128	0.091	0.108	0.195				+
E-B7-04	1:4 swale	0.97	0.685	61	0.101	0.021	0.101	0.127	0.285	0.385	0.524				+
E-B7-05	1:4 swale	1.92	0.685	30.7	0.042	0.032	0.042	0.063	0.203	0.385	0.524				-
E-B7-06	1:4 swale	2.67	0.854	149.8	0.042	0.022	0.13	0.289	0.226	0.365	0.854				+
E-B7-07	1:4 swale	1.57	0.832	143.0	0.033	0.000	0.033	0.192	0.220	0.395	0.832				+
E-B7-08	1:6 swale	2.66	0.446	153.8	0.115	0.054	0.115	0.222	0.113		0.179				-
E-B7-09	1:6 swale	1.45	0.463	144.6	0.113	0.053	0.113	0.222	0.128	0.163	0.203				1
E-B7-10A	1:6 swale	1.97	0.446	126.8	0.054	0.000	0.054	0.174	0.049	0.146	0.226				
E-B7-10B	1:4 swale	1.12	0.581	133.8	0.05	0.002	0.05	0.193	0.185	0.281	0.431				
E-B7-11	1:4 swale	0.01	0.773	73.1	0.227	0.077	0.227	0.579	0.412	0.473	0.691				
E-B8-01A	1:4 swale	0.56	0.569	126.1	0.037	0.013	0.037	0.113	0.108	0.269	0.53				
E-B8-01B	1:4 swale	2.08	0.569	120.2	0.032	0.011	0.032	0.087	0.083	0.269	0.53				
E-B9-01	1:6 swale	3.6	0.447	152.7	0.129	0.034	0.129	0.255	0.093	0.147	0.211				
E-B9-02	1:6 swale	1.57	0.441	95.6	0.059	0.015	0.059	0.115	0.077	0.141	0.211				
E-B9-03	1:6 swale	3.65	0.802	167	0.03	0	0.03	0.163	0	0.388	0.802				
E-B9-04	1:6 swale	1.85	0.802	113.2	0.019	0	0.019	0.105	0		0.802				
E-B9-05	1:4 swale	2.78	0.416	165.1	0.04	0.012	0.04	0.132	0.08	0.116	0.203			I	-
E-B9-06	1:4 swale	1.37	0.405	116.3	0.023	0.007	0.023	0.073	0.069		0.206			I	-
E-B9-07	1:4 swale	1.64	0.781	341.3	0.072	0	0.072	0.402	0	0.322	0.781		I	I	-
E-B9-08	1:4 swale	0.94	0.781	115.5	0.024	0	0.024	0.125	0 435		0.781	l		 	+
E-B10-01	1:6 swale	0.55	0.658	182.6	0.042	0.005	0.042	0.15	0.135		0.521			I	+
E-B10-02	1:6 swale	0.49	0.658	306.3	0.181	0.026	0.181	0.617	0.135	0.358	0.521		-		+
E-B10-03A E-B10-03B	1:6 swale 1:6 swale	3.09 1.69	0.41	<u>83.7</u> 54	0.041	0.012	0.041	0.095	0.062	0.11 0.358	0.176		-	<u> </u>	+
E-B10-03B	1:6 swale	2.44	0.658	54	0.064	0.01	0.064	0.21	0.135	0.358	0.521		1	1	+
E-B10-05	1:4 swale	3.18	0.475	94.3	0.017	0	0.027	0.061	0		0.319			1	+
W-B1-01	1:6 swale	0.67	0.438	178.5	0.051	0.009	0.051	0.145	0.074	0.138	0.201		1	1	1
W-B1-02	1:6 swale	0.85	0.417	100	0.029	0.006	0.029	0.073	0.069	0.117	0.178				
W-B1-03	1:6 swale	0.52	0.458	96.6	0.026	0.005	0.026	0.068	0.071	0.158	0.252				
W-B1-04	1:6 swale	0.91	1.003	109.3	0.464	0.001	0.464	0.473	0.248		0.707				
W-B1-05	1:6 swale	0.35	1.003	140.9	0.721	0.001	0.721	0.725	0.248	0.703	0.707				T
W-B3-01	1:6 swale	5.88	1.047	80		0.057	0.145	0.269	0.41	0.747					
N-B4-01	1:6 swale	1.8	0.909	166.8		0.038	0.088	0.183	0.533	0.609					
V-B4-02	1:6 swale	4.81	0.909	197.5	0.11	0.048	0.11	0.22	0.533	0.609	0.684			L	1
V-B5-01	1:6 swale	4.3	0.473	59.8	0.022	0.002	0.022	0.052	0.055		0.29		-	I	-
N-B5-02	1:6 swale	3.34	0.473	32	0.013	0.002	0.013	0.03	0.055		0.29		-	I	+
N-B5-03	1:6 swale	9	0.34	77.8	0.005	0	0.005	0.029	0		0.075			 	+
N-B5-04	1:6 swale	3	0.811	40		0.044	0.188	0.574	0.224		0.763			 	+
N-B5-05	1:6 swale	4.89	0.798	45	0.018	0.003	0.018	0.04	0.266	0.498	0.763		-	 	+
N-B5-06 07	1:6 swale	5.8 2.01	0.695	150		0.025	0.104	0.235	0.218		0.649		-		+
N-B5-08 N-B5-09	1:6 swale	2.01 4.63	0.695	<u>59.7</u> 80	0.038	0.009	0.038	0.082	0.218		0.649				+
W-B5-09 W-B5-11	1:6 swale 1:6 swale	4.63	0.479	27.1	0.044	0.01	0.044	0.093	0.153		0.291		-	<u> </u>	+
N-B5-11 N-B5-12	1:6 swale	5.19	0.345	27.1	0.004	0.001	0.004	0.018	0.027	0.045	0.077		1	<u> </u>	+
W-B5-12 W-B5-13A	1:6 swale	1.01	0.935	79.3	0.007	0.001	0.359	0.016	0.027		0.063			1	+
W-B5-13A W-B5-13B	1:6 swale	1.01	0.935	51.9	0.359	0.054	0.359	0.552	0.419		0.753			1	+
W-B5-13B W-B5-16	1:6 swale	3.8	0.935	51.9		0.007	0.021	0.18	0.419		0.753		1	<u> </u>	+
W-B5-CULV14 15	1:6 swale	4.38	0.665	164.5	0.021	0.015	0.021	0.054	0.124		0.753			1	+
W-B6-01	1:6 swale	0.69	0.005	175	0.087	0.015	0.087	0.190	0.124		0.569			1	+
W-B0-01 W-B7-01	1:6 swale	6.52	0.996	60		0	0.041		0				1	1	+
N-B7-01 W-B7-02	1:6 swale	7.82	1.101	140.7	0.12	0.031	0.12		0.354		0.996			1	+
W-EXT02	1:6 swale	0.38	0.542	132.4	0.12	0.031	0.12	0.524	0.095		0.363			1	+
W-EXT02	1:6 swale	4.92	0.342	71.1	0.067	0.014	0.067	0.149	0.033		0.293		1	1	+
W-EXT03	1:6 swale	1.56	1.423	89.7	0.186	0.013	0.186	0.463	0.13		1.423		1	1	+

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 | MR High Flow Catchpit, 3% sidestope, 0.5% grade | WA Main Roads High Flow Catchpit with Single Grate | 567429.2 | 6134213.54
 | No | | _ | 1941336
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 | WEST-84 | 50
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 | Mix High Flow Calcipit, 3% sideslope, 0.5% grade | res stain Roads High Flow Catchpit with Single Grate | 567565.0 | 6134266.11
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 | SUB-CATCHMENT DETALS | Pitor
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 | W45-CUVI-CAT
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W45-CULV2-HW
 | 0.246 | 9
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 | 40 | |
 | | | 1 3 | 5 96.5
5 25
 | 1 1 | 6.667 | 6.667 | 49
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 | 1286-004-05-05-04
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W-85-CULV2-HW
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 | W-01-02-CAT
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 | Pipe20555 | W-07-CULV1-IW
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N87149 | 12.2
 | 51 561
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Concrete, under soade, 0.5% minimum slope | 450
 | | 0 0.01 | 1 NewFood
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 | W47CULV205 | 10
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61.24 | | Concrete, under soade, 0.5% minimum slope
Concrete, under soade, 0.5% minimum slope |
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N87181 | 2
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Concrete, under roads. 0.5% minimum slope | 422
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Concrete, under roade, 0.5% minimum slope</td><td>450</td><td>45</td><td>0 0.01</td><td>1 NewFood</td><td>1</td><td>NE7101
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Concrete, under roade, 0.5% minimum slope | 450
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WEST-85</td><td>N87255
N87225</td><td>12</td><td>61.65
52.7</td><td>52.63</td><td>25</td><td>Concrete, under stade, 0.5% minimum slope
Concrete, under stade, 0.5% minimum slope</td><td>452</td><td>9 45
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 | 61.65
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Concrete, under stade, 0.5% minimum slope | 452
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Stage 1A (WEST) DRAINS F								
DRAINS results prepared from 1EY	m Version 20	20.036						
PIT / NODE DETAILS Name	Max HGL	Max Pond	Max Surface	Version 8 Max Pond	Min	Overflow	Constraint	
	Indux FFOE	HGL	Flow Arriving	Volume	Freeboard	(cu.m/s)	Constraint	
DUMMY-SCALE2	10		(cu.m/s) 0		(m)			
DUMMY-SCALE1 W1-B1-01-US	8 69		0					
W-B1-02-US W-B1-03-US	68.65		0					
W-B1-04-US	68.65 67		0					
W-B1-05-US W- B4-01-US	66.5 62		0					
W-B4-02-US W-B5-CULV1-HW	68.5 56.49		0.008		0.51	0	None	
W-B5-CULV1-DS	56.2		0					
W-B5-CULV2-HW W-B5-CULV2-DS	56.02 55.52		0.115		0.48	0	None	
W-B5-CULV3-HW W-B5-CULV3-DS	54.97 54.43		0.112 0.013		0.53	0	None	
W-B5-CULV4-HW	56.91		0		1.09	0	None	
W-B5-CULV4-DS W-B5-CULV5-HW	56.51 55.35		0.002		1.15	0	None	
W-B5-CULV5-DS W-B7-CULV2-HW	54.44 55.92		0		1.08		None	
W-B7-CULV2-DS	55.42		0					
W-B5-CULV6-HW N87219	52.12 51.86		0.028		0.88	0	None	
W-B1-CULV1-HW	68.22		0.011		0.78	0	None	
W1-01-DS N87159	67.87 65.15		0.032					
N87076 N87168	64.01 61.29		0					
W-EXT02-US	61.09		0.002					
W-EXT W-EXT-CULV1-HW	60.57 59.23		0.016		1.27	0	None	
W-EXT-CULV1-DS N87207	59.07 61.65		0					
N87255	61.01		0					
W-EXT-HW N87181	64.2 58.21		0		0.8	0	None	
W-B5-03-DS	57.1		0					
W-B5-03-US W-B5-06-US	62 63.5		0					
W-B5-01-US W-B5-02-US	59 57.5		0					
W-B5-05-US	58		0					
W-B5-08-US W-B5-09-US	56 58		0					
W-B5-11-US W-B5-12-US	58 57.5		0					
N87237	57.26		0					
N87238 W-B6-01-US	57.1 59.2		0					
N87225	52.7		0					
N87218 W-B5-16-US	52.42 56.5		0					
W-B5-CULV14-US W-B7-CULV1-HW	59.2 51.85		0.093		1.15	0	None	
N87244	49.24		0				nono	
N87245 W-B7-02-US	49.01 62.5		0					
HW12 N87149	53.04 51.91		0.016		0.96	0	None	
HW13	47.01		0.009		0.99	0	None	
N87150 W-B3-01-US	46.8		0					
S1_US	57.5		0					
SUB-CATCHMENT DETAILS								
Name	Max Flow Q	Paved Max Q	Grassed Max Q	Paved Tc	Grassed Tc	Supp. Tc	Due to Storm	
	(cu.m/s)	(cu.m/s)	(cu.m/s)	(min)	(min)	(min)		
W-B5-CULV1-CAT W-B5-CULV2-CAT	0.007		0.008		8.08	3.94	1EY AEP, 2 hour burst, Storm 2 1EY AEP, 2 hour burst, Storm 3	
W-B5-CULV3-CAT W-B5-CULV3-DS-CAT	0.038	0	0.038	0	5.22	2.54	1EY AEP, 1 hour burst, Storm 1 1EY AEP, 1 hour burst, Storm 1	
W-B5-CULV4-CAT	0	0	0	0	1.98	0	1EY AEP, 10 min burst, Storm 5	
W-B5-CULV5-CAT W-B5-CULV6-CAT	0.002	0	0.025	0	5.18	2.52	1EY AEP, 1 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 3	
W-B1-03-CAT W-B1-01-CAT	0.01 0.03	0	0.01	0	3.83	1.87	1EY AEP, 1 hour burst, Storm 1 1EY AEP, 1 hour burst, Storm 1	
WEST-B1-CAT	0.012	0	0.012	0	11.03	5.38	1EY AEP, 2 hour burst, Storm 3	
WEST-B2-CAT W-EXT-CAT	0.137	0.137	0		0 2.62		1EY AEP, 10 min burst, Storm 10 1EY AEP, 10 min burst, Storm 5	
W-EXT04-CAT WEST-B3-CAT	0.066	0	0	0	2.18	1.06	1EY AEP, 10 min burst, Storm 5 1EY AEP, 15 min burst, Storm 1	
CulvW_ext	0	0	0	5	75	2	1EY AEP, 10 min burst, Storm 5	
WEST-B4-CAT W-B5-03-CAT	0.161	0.161	0		10.08		1EY AEP, 10 min burst, Storm 4 1EY AEP, 10 min burst, Storm 5	
WEST-B6-CAT	0	0	0	0	3.56	1.74	1EY AEP, 10 min burst, Storm 5	
WEST-B5-CAT W-B7-01-CAT	0	0	0	0	3.33	0	1EY AEP, 10 min burst, Storm 5 1EY AEP, 10 min burst, Storm 5	
WEST-B7-CAT S1_catch	0.065						1EY AEP, 15 min burst, Storm 1 1EY AEP, 10 min burst, Storm 5	
					24.01			
PIPE DETAILS								
Name	Max Q	Max V	Max U/S		Due to Storm			
DUMMY-SCALE	(cu.m/s) 0				1EY AEP, 10 min burst, Storm 5			
W-B5-CULV1 W-B5-CULV2	0.002		56.485	56.199	1EY AEP, 2 hour burst, Storm 9 1EY AEP, 1 hour burst, Storm 1			
W-B5-CULV3	0.05	1.46	54.974	54.574	1EY AEP, 2 hour burst, Storm 3			
W-B5-CULV4 W-B5-CULV5	0.001	0.31	56.91 55.347		1EY AEP, 10 min burst, Storm 5 1EY AEP, 2 hour burst, Storm 2			
Pipe20528	0	0	55.913	55.416	1EY AEP, 10 min burst, Storm 5			
W-B5-CULV6 W-B1-CULV1	0.012	0.87	52.121 68.22	67.869	1EY AEP, 2 hour burst, Storm 4 1EY AEP, 2 hour burst, Storm 4			
Pipe20532	0	0	65.25	65.152	1EY AEP, 10 min burst, Storm 5			

Pipe20533	0	0	65.152	64.75	1EY AEP, 10 min burst, Storm 5			
Pipe20566	0	0	61.3	61.294	1EY AEP, 10 min burst, Storm 5			
Pipe20567	0.014				1EY AEP, 1 hour burst, Storm 1			
W-EXT-CULV1 Pipe20702	0.013		59.229 61.75		1EY AEP, 3 hour burst, Storm 7 1EY AEP, 10 min burst, Storm 5			
Pipe20716	0				1EY AEP, 10 min burst, Storm 5			
W-EXT-CULV	0			61.093	1EY AEP, 10 min burst, Storm 5			
Pipe20591	0.02		58.397		1EY AEP, 1 hour burst, Storm 1			
Pipe20597 Pipe20785	0.044	3.05			1EY AEP, 1 hour burst, Storm 1 1EY AEP, 10 min burst, Storm 5			
Pipe20790	0				1EY AEP, 10 min burst, Storm 5			
Pipe20745	0	0	52.7		1EY AEP, 10 min burst, Storm 5			
Pipe20746	0.029				1EY AEP, 3 hour burst, Storm 6			
Pipe20525 Pipe20821	0.032	0.15			1EY AEP, 3 hour burst, Storm 6 1EY AEP, 10 min burst, Storm 5			
Pipe20820 Pipe20830	0				1EY AEP, 10 min burst, Storm 5			
Pipe20526	0.013			51.956	1EY AEP, 3 hour burst, Storm 7			
Pipe20527	0	0	47.003	46.8	1EY AEP, 9 hour burst, Storm 3			
CHANNEL DETAILS								
Name	Max Q	Max V			Due to Storm			
-	(cu.m/s)	(m/s)						
OVERFLOW ROUTE DETAIL Name		Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm
0134039	0.009			3				1EY AEP, 3 hour burst, Storm 6
O134055	0.009	0	12.141	3	0	32	0	1EY AEP, 3 hour burst, Storm 6
0137112	0.005			3				1EY AEP, 1 hour burst, Storm 1
0137116	0.005			3				1EY AEP, 1 hour burst, Storm 1
O137914 O137918	0.006			3				1EY AEP, 1 hour burst, Storm 1 1EY AEP, 1 hour burst, Storm 1
O90392	0.012			0			0	
O90396	0			0			0	
OF76225	0.016	0.016	0.338	0.248	0.04	2.97	0.57	1EY AEP, 2 hour burst, Storm 3
OF76315	0.014		0.656	0.127	0.05	1.02		1EY AEP, 3 hour burst, Storm 6
OF76316	0			0		0	0	
OF76323 OF76327	0			0				
OF76345	0			0		0		
OF76352	0			0		0	0	
OF76354	0.002	0.002	0.332	0.266	0.01	3.19		1EY AEP, 2 hour burst, Storm 9
OF76357	0		0	0	0	0	0	
OF76359	0.042		0.35	0.174	0.08	2.09		1EY AEP, 1 hour burst, Storm 1
OF76363 OF76364	0			0				
OF76369	0			0				
OF76373	0	0	1.322	0	0			
OF76375	0	0	0	0	0	0	0	
OF76377	0			0			0	
OF76384 OF76391	0.013	0.013		0.003	0		0.13	1EY AEP, 3 hour burst, Storm 7
OF76405	0.029		0.393	0.294	0.06	3.53		1EY AEP, 3 hour burst, Storm 6
OF76407	0.012			0.294	0.03	3.53		1EY AEP, 2 hour burst, Storm 4
OF76410	0	0	19.24	0	0	0	0	
OF76413	0			0	0		0	
OF76415	0			0		0	0	
OF76418 OF76420	0			0				
OF76420 OF76424	0			0				
OF76426	0			0				
OF76429	0	0	0.225	0	0	0	0	
OF76432	0			0				
OF76434	0			0				
OF76436 OF76444	0			0			0	
OF76451	0			0				
W-B1-01	0		0.14	0.074	0.02	0.89		1EY AEP, 2 hour burst, Storm 3
W-B1-02	0			0.069	0.01	0.83		1EY AEP, 2 hour burst, Storm 3
W-B1-03 W-B1-04	0		0.123	0.071	0.01	0.86		1EY AEP, 2 hour burst, Storm 3 1EY AEP, 2 hour burst, Storm 9
W-B1-04 W-B1-05	0		0.103	0.248	0			1EY AEP, 2 hour burst, Storm 9
W-B1-03 W-B2-O1	0.005			3	0	32		1EY AEP, 1 hour burst, Storm 1
W-B3-01	0	0.057	0.414	0.41				
W-B4-01	0				0.06	4.92	0.63	1EY AEP, 15 min burst, Storm 1
W-B4-02			0.229	0.533	0.04	4.92 6.4	0.63	1EY AEP, 15 min burst, Storm 1
W R4 O1	0	0.048	0.229	0.533	0.04	4.92 6.4 6.4	0.63 0.43 0.68	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1
W-B4-O1 W-B5-01	0.006	0.048	0.229 0.375 12.141	0.533	0.04 0.06 0	4.92 6.4 6.4 32	0.63 0.43 0.68 0	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1
W-B4-O1 W-B5-01 W-B5-02	0	0.048	0.229 0.375 12.141 0.354	0.533	0.04	4.92 6.4 6.4	0.63 0.43 0.68 0.68 0.01	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1
W-B5-01 W-B5-02 W-B5-03	0 0.006 0 0 0	0.048 0 0.002 0.002 0	0.229 0.375 12.141 0.354 0.312 0.512	0.533 3 0.055 0.055 0.055	0.04 0.06 0 0.01 0.01 0.01	4.92 6.4 6.4 32 0.66 0.66	0.63 0.43 0.68 0 0 0 0 0 0 0 0 0 0 0 0	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04	0.006 0 0 0 0.044	0.048 0 0.002 0.002 0 0.044	0.229 0.375 12.141 0.354 0.312 0.512 0.296	0.533 3 0.055 0.055 0 0 0.224	0.04 0.06 0 0 0.01 0.01 0.01 0 0 0 0.07	4.92 6.4 6.4 32 0.66 0.66 0.66 0.2.69	0.63 0.43 0.68 0 0 0.13 0.09 0 0 0 0.09	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 1 hour burst, Storm 1
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-05	0.006 0 0 0 0 0.044 0	0.048 0 0.002 0.002 0 0 0.044 0.003	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378	0.533 3 0.055 0.055 0 0.224 0.266	0.04 0.06 0 0.01 0.01 0.01 0 0.07 0.07 0.07	4.92 6.4 6.4 32 0.66 0.66 0.66 0.2.69 3.19	0.63 0.43 0.66 0 0.13 0.09 0.09 0.076 0.26	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-06 W-B5-06 07	0.006 0 0 0 0.044 0 0 0 0	0.048 0 0.002 0.002 0 0 0.044 0.003 0.025	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411	0.533 3 0.055 0 0.224 0.266 0.218	0.04 0.06 0 0.01 0.01 0 0 0.07 0.01 0.07 0.01	4.92 6.4 32 0.66 0.66 0 2.69 3.19 2.62	0.63 0.43 0.68 0 0 0.13 0.09 0 0 0.76 0.26 0.65	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-05	0.006 0 0 0 0 0.044 0	0.048 0 0.002 0.002 0 0.044 0.003 0.025 0.009	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378	0.533 3 0.055 0.055 0 0.224 0.266	0.04 0.06 0 0.01 0.01 0.01 0 0.07 0.07 0.07	4.92 6.4 6.4 32 0.66 0.66 0.66 0.2.69 3.19	0.63 0.43 0.68 0 0.01 0.09 0 0 0.026 0.226 0.22 0.27	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-06 W-B5-06 07 W-B5-06 W-B5-09 W-B5-09 10 W-B5-11	0.006 00 0.044 0.044 00 00 00 00 00	0.048 0 0.002 0.002 0.044 0.003 0.025 0.009 0.01 0.01	0.229 0.375 12.141 0.352 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232	0.533 3 0.055 0.055 0 0.224 0.266 0.218 0.218 0.218 0.153 0	0.04 0.06 0 0 0.01 0.01 0.01 0.07 0.01 0.07 0.02 0.02 0.02 0.02 0.02	4.92 6.4 6.4 32 0.66 0.66 0.2.69 3.19 2.62 2.62 2.62 1.83 0	0.63 0.43 0.68 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-06 W-B5-06 07 W-B5-06 07 W-B5-08 W-B5-09 10 W-B5-11 W-B5-12	0.006 00 00 0.044 00 00 00 00 00 00 00 00 00 00	0.048 0 0.002 0.002 0 0 0.044 0.003 0.025 0.009 0.01 0 0 0.001	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389	0.533 3 0.055 0.055 0 0.224 0.266 0.218 0.218 0.218 0.153 0 0.027	0.04 0.06 0 0.01 0.01 0.07 0.07 0.07 0.02 0.02 0.02 0.02 0.02	4.92 6.4 32 0.66 0.66 0.2.69 3.19 2.62 2.62 1.83 0 0 0.32	0.63 0.43 0.68 0 0 0.013 0.09 0 0 0.05 0.65 0.27 0.27 0.38 0.05 0.027 0.38 0.027 0.38 0.027 0.38 0.027 0.038	1EY AEP, 15 min burst, Storn 1 1EY AEP, 16 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-05 W-85-06 07 W-85-08 W-85-09 10 W-85-09 W-85-11 W-85-12 W-85-13A	0.006 0.006 0.044 0.044 0.004 0.000 0.000 0.000 0.055	0.048 0 0.002 0.002 0.044 0.003 0.025 0.009 0.01 0 0.001	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172	0.533 3 0.055 0.055 0.024 0.224 0.266 0.218 0.218 0.153 0 0 0.027 0.419	0.04 0.06 0 0.01 0.01 0.07 0.07 0.01 0.05 0.02 0.02 0.02 0.02 0.02 0.02 0.01 0.01	4.92 6.4 32 0.66 0.66 0.2.69 3.19 2.62 2.62 1.83 0 0.32 5.03	0.63 0.43 0.68 0 0 0.13 0.09 0 0.76 0.26 0.65 0.27 0.36 0.22 0.65 0.27 0.36 0.22 0.65 0.27 0.36 0.22 0.53 0.22 0.53 0.53	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-06 W-B5-06 07 W-B5-08 W-B5-09 10 W-B5-11 W-B5-12 W-B5-13A W-B5-13B	0 0.006 0 0 0 0 0.044 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 00 0.002 0.044 0.044 0.025 0.009 0.01 0.001 0.001	0.229 0.375 12.141 0.354 0.312 0.296 0.378 0.411 0.242 0.367 0.232 0.367 0.232 0.367	0.533 3 0.055 0.055 0.024 0.224 0.218 0.218 0.218 0.153 0 0.027 0.419 0.419	0.04 0.06 0 0.01 0.01 0.07 0.07 0.07 0.02 0.02 0.02 0.02 0.02	4.92 6.4 6.4 32 0.66 0.66 0.0 2.69 2.62 2.62 2.62 1.83 0.0 2.62 5.03 5.03	0.63 0.43 0.68 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1EY AEP, 15 min burst, Storn 1 1EY AEP, 16 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-05 W-85-06 07 W-85-08 W-85-09 10 W-85-09 W-85-11 W-85-12 W-85-13A	0.006 0.006 0.044 0.044 0.004 0.000 0.000 0.000 0.055	0.048 0 0.002 0.002 0.044 0.003 0.025 0.009 0.01 0.054 0.001 0.054 0.007 0.001	0.229 0.375 12.141 0.512 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333	0.533 3 0.055 0.055 0.024 0.224 0.266 0.218 0.218 0.153 0 0 0.027 0.419	0.04 0.06 0 0 0.01 0.01 0.01 0.07 0.01 0.02 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 32 0.66 0.66 0.2.69 3.19 2.62 2.62 1.83 0 0.32 5.03	0.63 0.43 0.68 0.068 0.013 0.09 0.026 0.65 0.27 0.27 0.36 0.05 0.27 0.36 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-06 W-B5-06 07 W-B5-08 W-B5-09 10 W-B5-11 W-B5-12 W-B5-13A W-B5-13A W-B5-13B W-B5-16 W-B5-01	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0 0.002 0.002 0.044 0.003 0.025 0.009 0.011 0.054 0.007 0 0.005 0.007 0 0.015 0 0	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.322 0.389 0.172 0.232 0.389 0.172 0.232	0.533 3 0.055 0.055 0 0.224 0.224 0.228 0.218 0.153 0 0.027 0.419 0.419 0.419 0.124 3	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.06 0.06 0.02 0.69 2.62 2.62 2.62 2.62 1.83 0.32 0.32 5.03 5.03 5.03 3.19 9.2.62 1.49 3.23 0.02 0.02 0.02 0.03 0.03 0.03 0.03	0.63 0.43 0.68 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 2 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 9 hour burst, Storn 3
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 07 W-85-06 W-85-08 W-85-09 W-85-10 W-85-12 W-85-13A W-85-13A W-85-13A W-85-16 W-85-01 W-85-01	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0 002 0.002 0.042 0.044 0.003 0.044 0.003 0.009 0.001 0.001 0.054 0.007 0.054 0.007 0.054 0.007 0.015 0.001 0.015 0.00200000000	0.229 0.375 12.141 0.354 0.312 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.357 12.141 0.142	0.533 0.0555 0.0555 0.224 0.218 0.218 0.218 0.218 0.218 0.219 0.0027 0.419 0.0124 3 0 0 0 0 0 0 0 0 0 0 0 0 0	0.04 0.06 0 0.01 0.01 0.07 0.07 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.66 0.66 0.0 2.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 3.19 0.32 5.03 0.032 5.03 0.0320000000000	0.63 0.43 0.68 0.68 0.01 0.09 0.02 0.26 0.26 0.27 0.27 0.36 0.27 0.36 0.27 0.36 0.27 0.36 0.27 0.36 0.27 0.36 0.27 0.36 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.0	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 16 hour burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 6
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-06 W-85-08 W-85-09 W-85-10 W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-86-01 W-87-02	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.042 0.044 0.003 0.044 0.003 0.025 0.009 0.011 0.054 0.007 0.005 000000	0.229 0.375 12.141 0.354 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.367 0.232 0.367 0.232 0.367 1.241 0.478	0.533 3 0.055 0.055 0.224 0.266 0.218 0.218 0.153 0 0.027 0.419 0.0124 3 0 0.0124 3 0 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.026 0.027 0.0	0.04 0.06 0 0.01 0.01 0.07 0.07 0.07 0.02 0.02 0.02 0.02 0.02	4.92 6.4 6.4 32 0.66 0.66 0.06 2.69 2.62 2.62 2.62 1.83 0.0 0.32 5.03 0.032 5.03 0.032 0.032 0.032 0.032 0.032 0.04 0.05 0.032 0.04 0.04 0.04 0.04 0.04 0.05 0.05 0.05	0.63 0.43 0.68 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 3 1EY AEP, 9 hour burst, Storm 3 1EY AEP, 9 hour burst, Storm 6 1EY AEP, 2 hour burst, Storm 6
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-05 W-B5-06 W-B5-08 W-B5-10 W-B5-13A W-B5-13B W-B5-16 W-B5-16 W-B5-10 W-B5-10 W-B5-10 W-B5-10 W-B5-10 W-B5-10 W-B5-01 W-B5-01 W-B7-01	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.003 0.004 0.048 0.002 0.009 0.015 0.054 0.005 0.005 0.009 0.015 0.001 0.015 0.002 0.	0.229 0.375 12.141 0.354 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.172 0.236 0.333 0.357 12.141 0.142 0.478 12.141	0.533 3 0.0555 0.0555 0.2244 0.2666 0.218 0.153 0 0.027 0.419 0.419 0.1244 3 0 0.055 0.055 0.027 0.0218 0.055 0.027 0.0218 0.055 0.027 0.0218 0.027 0.0218 0.027 0.0218 0.027 0.0218 0.027 0.0218 0.0218 0.027 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0218 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0227 0.0237 0.0237 0.0227 0.0237 0.0227 0.0237 0.0377 0.0337 0.0357 0.03	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 32 0.666 0.666 0.666 0.666 0.666 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 2.62 2.6	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.26 0.65 0.027 0.33 0.027 0.33 0.027 0.33 0.027 0.33 0.027 0.33 0.027 0.33 0.027 0.03 0.04 0.04 0.04 0.04 0.04 0.04 0.04	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 6 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 1 hour burst, Storn 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-05 W-85-06 07 W-85-09 10 W-85-12 W-85-12 W-85-13A W-85-16 W-85-01 W-85-01 W-87-02 W-87-02	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.004 0.044 0.003 0.025 0.009 0.01 0.054 0.007 0.007 0.001 0.001 0.001 0.001 0.001 0.002 0.003 0.0	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.387 0.387 0.382 0.387 0.332 0.387 0.333 0.357 12.141 0.142 0.478 10.142	0.533 3 0.055 0.055 0.224 0.266 0.218 0.218 0.153 0 0.027 0.419 0.0124 3 0 0.0124 3 0 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.026 0.027 0.0	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.66 0.66 2.69 2.62 2.62 2.62 2.62 2.62 2.62 2	0.63 0.43 0.68 0.05 0.09 0.076 0.065 0.026 0.055 0.027 0.36 0.053 1.122 0.045 0.053 0.045 0.045 0.045 0.045 0.047 0.045	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 16 hour burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 6
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-05 W-B5-06 W-B5-08 W-B5-10 W-B5-13A W-B5-13B W-B5-16 W-B5-16 W-B5-10 W-B5-10 W-B5-10 W-B5-10 W-B5-10 W-B5-10 W-B5-01 W-B5-01 W-B7-01	0 0006 00 00 0007 0007 0007 0007 0007 0	0.048 0.002 0.002 0.004 0.044 0.003 0.025 0.009 0.015 0.054 0.0015 0.055 0.005 0.015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0010 0.0015 0.0010 0.00000000	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.387 0.387 0.382 0.387 0.332 0.387 0.333 0.357 12.141 0.142 0.478 10.142	0.533 3 0.055 0.055 0.224 0.266 0.218 0.153 0 0.419 0.419 0.124 3 0 0.554 0.055 0.224 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.055 0.024 0.026 0.025 0.02	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 6.4 32 0.866 0.866 0.866 0.866 0.866 0.82 0.319 0.32 0.32 0.33 5.03 0.32 0.32 0.32 0.0320000000000	0.63 0.43 0.43 0.68 0 0.09 0 0 0.09 0.076 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.0270000000000	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 6 1EY AEP, 3 hour burst, Storn 9 1EY AEP, 3 hour burst, Storn 6 1EY AEP, 1 hour burst, Storn 6
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-06 W-B5-06 W-B5-06 W-B5-08 W-B5-09 10 W-B5-11 W-B5-12 W-B5-13A W-B5-13A W-B5-13A W-B5-16 W-B5-01 W-B5-01 W-B5-01 W-B7-01 W-B7-01 W-EXT02 W-EXT02	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.003 0.04 0.004 0.002 0.003 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.002 0.003 0.005 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.004 0.003 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.004 0.003 0.004 0.004 0.004 0.004 0.004 0.004 0.003 0.004 0.0	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.357 12.141 0.142 0.478 12.141 0.142 0.379 0.379 0.379 0.379	0.533 3 0.055 0.055 0 0.224 0.266 0.218 0.218 0.218 0.218 0.218 0.218 0.218 0.214 0.218 0.214 0.218 0.214 0.218 0.214 0.218 0.214 0.218 0.217 0.214 0.218 0.217 0.214 0.218 0.217 0.214 0.218 0.218 0.217 0.219 0.214 0.218 0.055 0.005 0.005 0.005 0.015 0.015 0.027 0.015 0.027 0.015 0.027 0.015 0.027 0.019 0.005 0.019 0.019 0.005 0.019 0.005 0.019 0.005 0.019 0.005 0.005 0.019 0.005 0.0	0.04 0.06 0.01 0.01 0.01 0.07 0.02 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 32 0.66 0.66 0.66 0.66 0.66 0.66 0.66 0.6	0.63 0.43 0.43 0.68 0 0.09 0 0 0.09 0.076 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.0270000000000	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 9
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-05 W-B5-06 W-B5-09 W-B5-10 W-B5-12 W-B5-13A W-B5-16 W-B5-16 W-B5-01 W-B5-01 W-B7-01 W-B7-01 W-EXT03 W-EXT04	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.003 0.04 0.004 0.002 0.003 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.002 0.003 0.005 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.003 0.004 0.003 0.003 0.004 0.003 0.004 0.003 0.004 0.003 0.004 0.004 0.003 0.004 0.004 0.004 0.004 0.004 0.004 0.003 0.004 0.0	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.357 12.141 0.142 0.478 12.141 0.142 0.379 0.379 0.379 0.379	0.533 3 0.055 0.055 0.224 0.266 0.218 0.218 0.218 0.218 0.027 0.419 0.0419 0.0419 0.0419 0.0419 0.055 0.055 0.027 0.419 0.055 0.055 0.055 0.055 0.022 0.226 0.021 0.226 0.021 0.021 0.025 0.0226 0.021 0.021 0.021 0.025 0.025 0.025 0.0226 0.025 0.027 0.021 0.027 0.027 0.027 0.027 0.025 0.025 0.025 0.025 0.025 0.027	0.04 0.06 0.01 0.01 0.01 0.07 0.02 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-08 W-85-09 W-85-11 W-85-12 W-85-12 W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-85-01 W-87-02 W-87-01 W-87-01 W-82T02 W-EXT03 W-EXT04 W-S1	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.003 0.04 0.004 0.002 0.003 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.002 0.0	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.357 12.141 0.142 0.478 12.141 0.142 0.379 0.379 0.379 0.379	0.533 3 0.055 0.055 0.224 0.266 0.218 0.218 0.218 0.218 0.027 0.419 0.0419 0.0419 0.0419 0.0419 0.055 0.055 0.027 0.419 0.055 0.055 0.055 0.055 0.022 0.226 0.021 0.226 0.021 0.021 0.025 0.0226 0.021 0.021 0.021 0.025 0.025 0.025 0.0226 0.025 0.027 0.021 0.027 0.027 0.027 0.027 0.025 0.025 0.025 0.025 0.025 0.027	0.04 0.06 0.01 0.01 0.01 0.07 0.02 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-06 W-85-09 W-85-01 W-85-12 W-85-13A W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-85-01 W-87-01 W-87-01 W-87-01 W-8XT04 W-SXT04	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.003 0.004 0.003 0.005 0.009 0.001 0.001 0.005 0.007 0.001 0.001 0.0014 0.0014 0.003 0.0014 0.003 0.0014 0.003 0.0014 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.00	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.387 0.232 0.387 0.232 0.387 0.232 0.387 12.141 0.142 0.478 12.141 0.142 0.353 12.141 0.357	0.533 3 0.055 0.055 0 0.224 0.266 0.218 0.218 0.218 0.218 0.218 0.218 0.219 0.419 0.419 0.055 0.00 0.027 0.419 0.055 0.027 0.214 0.218 0.027 0.0419 0.0419 0.055 0.055 0.027 0.027 0.0419 0.055 0.027 0.0419 0.055 0.055 0.027 0.0419 0.055 0.027 0.0419 0.055 0.027 0.0419 0.055 0.027 0.0419 0.055 0.055 0.027 0.0419 0.055 0.055 0.027 0.0419 0.055 0.000 0.027 0.0419 0.055 0.000 0.027 0.019 0.000 0.027 0.019 0.000 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.019 0.027 0.055	0.04 0.06 0 0.01 0.01 0.07 0.07 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-08 W-85-09 W-85-11 W-85-12 W-85-12 W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-85-01 W-87-02 W-87-01 W-87-01 W-82T02 W-EXT03 W-EXT04 W-S1	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.003 0.04 0.004 0.002 0.003 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.005 0.002 0.0	0.229 0.375 12.141 0.354 0.312 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.357 12.141 0.142 0.478 12.141 0.142 0.379 0.379 0.379 0.379	0.533 3 0.055 0.055 0 0.224 0.266 0.218 0.218 0.218 0.218 0.218 0.027 0.419 0.0124 3 0 0.0124 0 0.055 0 0 0.055 0 0 0.214 0.218 0.218 0.055 0 0.214 0.218 0.218 0.055 0 0.214 0.218 0.218 0.055 0 0.214 0.218 0.218 0.055 0 0.214 0.218 0.218 0.055 0.055 0.055 0.055 0.024 0.218 0.027 0.027 0.0218 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.027 0.015 0.027 0.055 0.027 0.027 0.0153 0.005 0.027 0.0153 0.005 0.027 0.0153 0.005 0.018 0.018 0.005 0.018 0.018 0.007 0.019 0.019 0.019 0.019 0.019 0.019 0.005 0.018 0.000 0.018 0.000 0.018 0.000 0.018 0.000 0.018 0.000 0.019 0.000 0.000 0.019 0.0000 0.00000 0.00000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000 0.00000 0.00000000	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-06 W-85-09 W-85-01 W-85-12 W-85-13A W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-85-01 W-87-01 W-87-01 W-87-01 W-8XT04 W-SXT04	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.003 0.004 0.003 0.005 0.009 0.001 0.001 0.005 0.007 0.001 0.001 0.0014 0.0014 0.003 0.0014 0.003 0.0014 0.003 0.0014 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.00	0.229 0.375 12.141 0.354 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.357 12.141 0.142 0.478 12.141 0.045 0.379 0.213 0.385	0.533 3 0.055 0.055 0 0.224 0.266 0.218 0.218 0.218 0.218 0.218 0.218 0.219 0.419 0.0419 0.0419 0.0419 0.0419 0.0419 0.055 0.027 0.224 0.266 0.218 0.0419 0.0419 0.0419 0.0419 0.055 0.0419 0.0419 0.055 0.0419 0.0419 0.055 0.055 0.027 0.0419 0.055 0.055 0.027 0.0419 0.055 0.055 0.027 0.0419 0.055 0.055 0.0419 0.0419 0.055 0.055 0.0419 0.055 0.055 0.055 0.0419 0.055 0.055 0.0419 0.055 0.055 0.005 0.0419 0.005 0.005 0.005 0.005 0.010 0.010 0.010 0.010 0.010 0.010 0.005 0.010 0.010 0.005 0.010 0.027 0.010 0.027 0.010 0.027 0.027 0.027 0.010 0.027 0.010 0.027 0.005 0.	0.04 0.06 0.01 0.01 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.04 0.07 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.07 0.04 0.05 0.02 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.04 0.03 0.03 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.04 0.05 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.04 0.03 0.03 0.03 0.04 0.03 0.03 0.04 0.03 0.03 0.04 0.03 0.03 0.04 0.03 0.03 0.04 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.04 0.03 0.04	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 6 1EY AEP. 3 hour burst, Storm 6
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-06 W-85-09 W-85-10 W-85-12 W-85-13A W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-85-01 W-87-02 W-87-01 W-87-02 W-87-01 W-87-02	0 0.006 0.006 0.0044 0.044 0.009 0.005 0.009 0.009 0.009 0.009 0.009 0.0014 0.009 0.0013 0.0013 0.0013 0.0013 0.0013 0.0013 0.0013 0.0013 0.0014 0.0016 0.0010 0.0016 0.0010 0.0016 0.00100 0.00000000	0.048 0.002 0.002 0.002 0.044 0.003 0.025 0.009 0.011 0.055 0.007 0.001 0.055 0.007 0.001 0.001 0.001 0.001 0.001 0.001 0.002 0.003 0.002 0.003 0.002 0.003 0.003 0.002 0.003 0.002 0.003 0.002 0.002 0.003 0.002 0.002 0.003 0.002 0.003 0.002 0.003 0.002 0.002 0.003 0.002 0.003 0.002 0.	0.229 0.375 12.141 0.354 0.312 0.296 0.378 0.411 0.242 0.387 0.378 0.387 0.172 0.236 0.389 0.172 0.236 0.333 0.357 12.141 0.142 0.478 12.141 0.105 0.379 0.213 0.385 0.375 0.075 0.0	0.533 0.555 0.055 0.055 0.224 0.2266 0.218 0.218 0.533 0.0027 0.419 0.419 0.0419 0.0124 3.0 0.0354 0.0355 0.0095 0.000 0.0095 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000 0.00000000	0.04 0.06 0.01 0.01 0.01 0.07 0.02 0.03	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 6 1EY AEP. 3 hour burst, Storm 6
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-06 W-85-08 W-85-10 W-85-12 W-85-13A W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-87-01 W-87-02 W-87-02 W-87-01 W-87-02 W-87-01	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.002 0.044 0.003 0.025 0.009 0.01 0.054 0.007 0.001 0.055 0.007 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.001 0.002 0.003 0.003 0.003 0.003 0.002 0.003 0.002 0.003 0.002 0.003 0.0	0.229 0.375 12.141 0.354 0.312 0.296 0.378 0.411 0.242 0.367 0.232 0.367 0.232 0.387 0.232 0.387 0.232 0.387 0.232 0.385 12.141 0.422 0.478 12.141 0.422 0.387 0.232 0.385 12.141 0.422 0.387 0.232 0.385 12.141 0.422 0.387 0.232 0.385 12.141 0.367 0.232 0.385 12.141 0.367 0.232 0.385 0.378 0.357 12.141 0.242 0.378 0.378 0.378 0.385 0.378 0.385 0.377 0.232 0.385 0.357 12.141 0.367 0.232 0.385 0.377 12.141 0.367 0.232 0.385 0.377 12.141 0.367 0.385 0.385 0.385 0.385 0.378 0.385 0.385 0.385 0.385 0.385 0.378 0.385 0.378 0.385 0.385 0.378 0.385 0.378 0.385 0.378 0.385 0.378 0.357 12.141 0.367 0.322 0.385 0.357 12.141 0.367 0.325 0.385 0.357 12.141 0.367 0.325 0.357 12.141 0.367 0.325 0.379 0.379 0.378 0.379 0.385 0.379 0.385 0.379 0.212 0.385 0.379 0.212 0.385 0.379 0.212 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.214 0.385 0.3	0.533 3 0.555 0.055 0.224 0.266 0.218 0.218 0.218 0.218 0.218 0.218 0.027 0.419 0.419 0.419 0.0419 0.0354 0.0355 0.055 0.027 0.419 0.419 0.0355 0.027 0.419 0.0419 0.0355 0.027 0.0419 0.055 0.027 0.218 0.055 0.027 0.218 0.027 0.218 0.027 0.218 0.027 0.021 0.021 0.027 0.021 0.027 0.021 0.021 0.027 0.021 0.027 0.021 0.027 0.021 0.027 0.021 0.027 0.00 0.027 0.007	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.02 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.04 0.04 0.04 0.05 0.02 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.04 0.04 0.04 0.04 0.05 0.02 0.03 0.04 0.04 0.03 0.03 0.04 0.04 0.04 0.02 0.04 0.04 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.03 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05 0.04 0.05	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 6 1EY AEP. 3 hour burst, Storm 6
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-05 W-B5-06 W-B5-09 W-B5-09 W-B5-10 W-B5-12 W-B5-13 W-B5-13 W-B5-13 W-B5-14 W-B5-10 W-B5-01 W-B5-10 W-B	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.002 0.004 0.003 0.025 0.009 0.015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.002 0.0015 0.002 0.0015 0.002 0.0015 0.002 0.002 0.0015 0.002 0.001	0.229 0.375 12.141 0.354 0.512 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.333 0.357 12.141 0.142 0.474 0.474 12.141 0.142 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385	0.533 3 0.055 0.055 0 0.224 0.266 0.218 0.218 0.218 0.218 0.218 0.218 0.219 0.027 0.419 0 0.027 0.419 0 0.0354 0.055 0 0.214 0.266 0.214 0.218 0.214 0.214 0.218 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.214 0.218 0.055 0.055 0.027 0.214 0.218 0.055 0.027 0.019 0.027 0.019 0.00 0.027 0.019 0.00 0.010 0.010 0.010 0.00 0.027 0.019 0.00 0.027 0.019 0.00 0.00 0.027 0.019 0.000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000 0.00000 0.000000 0.00000000	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.02 0.01	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 6 1EY AEP. 3 hour burst, Storm 6
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W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-06 W-85-08 W-85-09 W-85-11 W-85-12 W-85-13A W-85-13A W-85-13A W-85-13A W-85-16 W-85-01 W-85-01 W-85-01 W-85-01 W-85-01 W-87-02 W-87-02 W-87-02 W-87-02 W-87-02 W-87-01 W-87-01 W-87-01 W-87-01 W-87-01 W-87-01 W-87-02 W-87-01 W-87-01 W-87-01 W-87-02 W-87-01 W-87-01 W-87-02 W-87-02 W-87-01 W-87-01 W-87-02 W-87-01 W-87-02 W-87-01 W-87-02 W-87-02 W-87-01 W-87-02 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-03 W-87-04	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.002 0.044 0.003 0.025 0.009 0.01 0.05 0.007 0.001 0.05 0.001 0.005	0.229 0.375 12.141 0.354 0.312 0.296 0.378 0.411 0.242 0.389 0.172 0.232 0.389 0.172 0.232 0.389 0.172 0.233 0.357 12.141 0.142 0.478 12.141 0.142 0.478 12.141 0.142 0.379 0.213 0.357 12.141 0.142 0.478 12.141 0.142 0.379 0.213 0.357 12.141 0.142 0.379 0.213 0.357 0.213 0.357 0.212 0.378 0.378 0.378 0.212 0.378 0.378 0.327 0.212 0.385 0.378 0.212 0.329 0.213 0.357 0.212 0.329 0.213 0.357 0.212 0.212 0.329 0.213 0.357 0.212 0.212 0.329 0.213 0.357 0.212 0.212 0.329 0.212 0.329 0.212 0.212 0.329 0.212 0.212 0.212 0.212 0.220 0.389 0.172 0.220 0.329 0.325 0.025	0.533 3 0.555 0.055 0.224 0.266 0.218 0.218 0.218 0.218 0.218 0.219 0.027 0.419 0.0419 0.0419 0.0354 0.0354 0.0355 0.055 0.027 0.419 0.0419 0.0355 0.055 0.027 0.419 0.0419 0.0355 0.055 0.027 0.419 0.0419 0.0355 0.027 0.0419 0.0355 0.027 0.0419 0.0419 0.0355 0.055 0.027 0.0419 0.0419 0.0355 0.027 0.0419 0.0419 0.0355 0.027 0.0419 0.0355 0.027 0.0419 0.0355 0.027 0.0419 0.0355 0.027 0.0419 0.0355 0.027 0.0419 0.0355 0.027 0.0419 0.0355 0.000 0.027 0.0419 0.027 0.0354 0.0355 0.000 0.027 0.0419 0.000 0.027 0.0419 0.000 0.0354 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.00000000	0.04 0.06 0 0.01 0.01 0.07 0.07 0.05 0.02 0.02 0.02 0.02 0.02 0.02 0.02	4.92 6.4 0.66 0.66 0.66 0.66 0.69 3.19 2.62 2.62 2.62 2.62 2.62 2.62 0.32 0.32 0.32 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.032 0.04 0.04 0.04 0.04 0.04 0.04 0.04 0.0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP. 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1 1EY AEP, 2 hour burst, Storm 9 1EY AEP. 2 hour burst, Storm 3 1EY AEP. 3 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 1 hour burst, Storm 9 1EY AEP. 3 hour burst, Storm 9
W-85-01 W-85-02 W-85-03 W-85-04 W-85-06 W-85-06 W-85-06 W-85-09 W-85-10 W-85-12 W-85-12 W-85-13A W-85-12 W-85-13A W-85-16 W-85-01 W-85-01 W-85-01 W-85-01 W-85-01 W-87-02 W-87-02 W-87-01 W-87-02 WEST-80 W	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.002 0.044 0.003 0.025 0.009 0.011 0.054 0.007 0.001 0.005 0.	0.229 0.375 12.141 0.354 0.312 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.367 12.141 0.142 0.478 12.141 0.142 0.478 12.141 0.142 0.478 12.141 0.142 0.339 0.357 12.141 0.142 0.478 12.141 0.142 0.478 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.375 0.212 0.212 0.325 0.025	0.533 0.553 0.055 0.055 0.024 0.224 0.224 0.228 0.218 0.218 0.218 0.218 0.218 0.218 0.027 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.0354 0.055 0.055 0.027 0.419 0.0354 0.055 0.0155 0.027 0.419 0.0354 0.0355 0.0155 0.027 0.419 0.0355 0.0155 0.0155 0.027 0.419 0.0155 0.0155 0.0155 0.027 0.419 0.0124 0.0155 0.0155 0.027 0.419 0.0124 0.0355 0.0155 0.0155 0.0155 0.0155 0.027 0.0155 0.0155 0.0155 0.027 0.019 0.0124 0.0354 0.0055 0.0124 0.0155 0.0155 0.0155 0.0155 0.0218 0.0155 0.0155 0.0155 0.0155 0.027 0.019 0.0124 0.0124 0.0124 0.0124 0.000 0.027 0.019 0.0124 0.000 0.027 0.019 0.0124 0.025 0.000 0.027 0.019 0.027 0.019 0.020 0.020 0.000 0.020 0.020 0.020 0.020 0.020 0.000 0.020 0.000 0.020 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.0000000 0.00000000	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.05 0.02 0.02 0.02 0.02 0.03 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.04 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.04 0.05 0.05 0.02 0.04 0.04 0.05 0.05 0.02 0.04 0.05 0.05 0.02 0.04 0.04 0.05 0.05 0.05 0.02 0.04 0.04 0.04 0.05 0.05 0.02 0.04 0.04 0.04 0.05 0.05 0.05 0.02 0.04 0.05 0.04 0.04 0.04 0.05 0.04 0.04 0.05 0.04 0.05 0.04 0.05	4.92 6.4 6.4 32 0.666 0.66 0.66 0.66 0.62 0 0 0.319 2.62 2.62 2.62 1.83 0 0.32 0 0.32 0 0.32 0 0.32 0 0.32 0 0 1.14 0 0 0 1.56 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.63 0.43 0.68 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 2 hour burst, Storn 3 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 6 1EY AEP, 3 hour burst, Storn 6 1EY AEP, 3 hour burst, Storn 6 1EY AEP, 3 hour burst, Storn 6
W-B5-01 W-B5-02 W-B5-03 W-B5-04 W-B5-06 W-B5-06 W-B5-09 W-B5-09 W-B5-10 W-B5-11 W-B5-12 W-B5-13A W-B5-13A W-B5-14 W-B5-16 W-B5-01 W-B5-01 W-B5-01 W-B5-01 W-B5-01 W-B7-02 W-B7-02 W-EXT02 W-EXT03 W-EXT03 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 W-EXT04 WEST-B1 WEST-B1 WEST-B1 WEST-B2 WEST-B4 WEST-B5 WEST-B7 Run Log for 12546218_Albar	0 0.006 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.048 0.002 0.002 0.002 0.044 0.003 0.025 0.009 0.011 0.054 0.007 0.001 0.005 0.	0.229 0.375 12.141 0.354 0.312 0.296 0.378 0.411 0.242 0.367 0.232 0.389 0.172 0.236 0.367 12.141 0.142 0.478 12.141 0.142 0.478 12.141 0.142 0.478 12.141 0.142 0.339 0.357 12.141 0.142 0.478 12.141 0.142 0.478 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.379 0.213 0.385 0.375 0.212 0.212 0.325 0.025	0.533 0.553 0.055 0.055 0.024 0.224 0.224 0.228 0.218 0.218 0.218 0.218 0.218 0.218 0.027 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.419 0.0354 0.055 0.055 0.027 0.419 0.0354 0.055 0.0155 0.027 0.419 0.0354 0.0355 0.0155 0.027 0.419 0.0355 0.0155 0.0155 0.027 0.419 0.0155 0.0155 0.0155 0.027 0.419 0.0124 0.0155 0.0155 0.027 0.419 0.0124 0.0355 0.0155 0.0155 0.0155 0.0155 0.027 0.0155 0.0155 0.0155 0.027 0.019 0.0124 0.0354 0.0055 0.0124 0.0155 0.0155 0.0155 0.0155 0.0218 0.0155 0.0155 0.0155 0.0155 0.027 0.019 0.0124 0.0124 0.0124 0.0124 0.000 0.027 0.019 0.0124 0.000 0.027 0.019 0.0124 0.025 0.000 0.027 0.019 0.027 0.019 0.020 0.020 0.000 0.020 0.020 0.020 0.020 0.020 0.000 0.020 0.000 0.020 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.00000 0.00000 0.0000000 0.00000000	0.04 0.06 0.01 0.01 0.01 0.07 0.07 0.05 0.02 0.02 0.02 0.02 0.03 0.04 0.03 0.04 0.03 0.04 0.03 0.04 0.04 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.05 0.02 0.04 0.04 0.05 0.05 0.02 0.04 0.04 0.05 0.05 0.02 0.04 0.05 0.05 0.02 0.04 0.04 0.05 0.05 0.05 0.02 0.04 0.04 0.04 0.05 0.05 0.02 0.04 0.04 0.04 0.05 0.05 0.05 0.02 0.04 0.05 0.04 0.04 0.04 0.05 0.04 0.04 0.05 0.04 0.05 0.04 0.05	4.92 6.4 6.4 32 0.666 0.66 0.66 0.66 0.62 0 0 0.319 2.62 2.62 2.62 1.83 0 0.32 0 0.32 0 0.32 0 0.32 0 0.32 0 0 1.14 0 0 0 1.56 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.63 0.43 0.68 0.68 0.09 0.09 0.09 0.026 0.65 0.27 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.36 0.027 0.03 0.04 0.04 0.04 0.044	1EY AEP, 15 min burst, Storn 1 1EY AEP, 15 min burst, Storn 1 1EY AEP, 1 hour burst, Storn 1 1EY AEP, 2 hour burst, Storn 9 1EY AEP, 2 hour burst, Storn 7 1EY AEP, 2 hour burst, Storn 6 1EY AEP, 3 hour burst, Storn 6

Stage 1A (WEST) DRAI								
DRAINS results prepared 10% AEP	from Versio	n 2020.036						
PIT / NODE DETAILS		Mary Daniel	M	Version 8	N 41	0	Ormateriat	
 Name		HGL	Max Surface Flow Arriving		Freeboard	Overflow (cu.m/s)	Constraint	
 DUMMY-SCALE2	10		(cu.m/s) 0	(cu.m)	(m)			
DUMMY-SCALE1	8		0					
W1-B1-01-US W-B1-02-US	69 68.65		0					
W-B1-03-US	68.65		0					
W-B1-04-US W-B1-05-US	67 66.64		0					
W- B4-01-US W-B4-02-US	62 68.5		0					
W-B5-CULV1-HW	56.6		0.028		0.4	0	None	
W-B5-CULV1-DS W-B5-CULV2-HW	56.31 56.3		0.314		0.2	0	None	
W-B5-CULV2-DS W-B5-CULV3-HW	55.59 55.19		0.29		0.31			
W-B5-CULV3-DS	54.53		0.032				None	
W-B5-CULV4-HW W-B5-CULV4-DS	56.98 56.55		0.006		1.02	0	None	
W-B5-CULV5-HW	55.39		0.012		1.11	0	None	
W-B5-CULV5-DS W-B7-CULV2-HW	54.47 55.92		0		1.08	0	None	
W-B7-CULV2-DS W-B5-CULV6-HW	55.42 52.37		0.074		0.63	0	None	
N87219	52.36		0					
W-B1-CULV1-HW W1-01-DS	68.31 67.92		0.026		0.69	0	None	
N87159	65.27		0					
N87076 N87168	64.13 61.33		0					
W-EXT02-US W-EXT	61.24 60.69		0.093					
W-EXT-CULV1-HW	59.64		0.372		0.86	0	None	
W-EXT-CULV1-DS N87207	59.19 61.73		0					
N87255 W-EXT-HW	61.07 64.63		0.26		0.37		None	
N87181	58.28		0		0.37	0	none	
W-B5-03-DS W-B5-03-US	57.16 62		0.038					
W-B5-06-US	63.5		0					
W-B5-01-US W-B5-02-US	59 57.5		0					
W-B5-05-US W-B5-08-US	58 56		0					
W-B5-09-US	58		0					
W-B5-11-US W-B5-12-US	58 57.5		0					
N87237	57.26		0					
N87238 W-B6-01-US	57.1 59.2		0					
N87225 N87218	52.82 52.52		0					
W-B5-16-US	56.5		0					
W-B5-CULV14-US W-B7-CULV1-HW	59.2 52.36		0.379		0.64	0	None	
N87244 N87245	49.39 49.17		0					
W-B7-02-US	62.5		0			_		
HW12 N87149	53.44 51.93		0.317		0.56	0	None	
HW13 N87150	47.42 46.81		0.239		0.58	0	None	
W-B3-01-US	67.2		0					
 S1_US	57.5		0					
 SUB-CATCHMENT DET		David	0	D	0	0	Due to Otamo	
Name		Paved Max Q	Grassed Max Q	Paved Tc	Grassed Tc	Supp. Tc	Due to Storm	
 W-B5-CULV1-CAT	(cu.m/s) 0.04	(cu.m/s) 0	(cu.m/s) 0.04	(min) 0	(min) 2.63	(min) 1.28	10% AEP, 10 min burst, Storm 5	
W-B5-CULV2-CAT	0.035	0	0.035	0	3.48	1.69	10% AEP, 10 min burst, Storm 7	
W-B5-CULV3-CAT W-B5-CULV3-DS-CAT	0.169	0	0.053	0	2.14	1.04	10% AEP, 10 min burst, Storm 5 10% AEP, 10 min burst, Storm 4	
W-B5-CULV4-CAT W-B5-CULV5-CAT	0.007	0					10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 5	
W-B5-CULV6-CAT	0.118	0	0.118	0	2.23	1.09	10% AEP, 10 min burst, Storm 5	
W-B1-03-CAT W-B1-01-CAT	0.044 0.132	0					10% AEP, 10 min burst, Storm 4 10% AEP, 10 min burst, Storm 5	
WEST-B1-CAT WEST-B2-CAT	0.103	0.269	0.103	0	4.75	2.31	10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 1	
W-EXT-CAT	0.043	0	0.043	0	2.06	0	10% AEP, 10 min burst, Storm 3	
W-EXT04-CAT WEST-B3-CAT	0.029	0					10% AEP, 10 min burst, Storm 9 10% AEP, 10 min burst, Storm 9	
CulvW_ext WEST-B4-CAT	0.142	0.322		5		2	10% AEP, 3 hour burst, Storm 6 10% AEP, 10 min burst, Storm 4	
W-B5-03-CAT	0.013	0	0.013	0	2.12	0	10% AEP, 10 min burst, Storm 3	
WEST-B6-CAT WEST-B5-CAT	0.124 0.073	0					10% AEP, 10 min burst, Storm 9 10% AEP, 10 min burst, Storm 9	
W-B7-01-CAT	0.007	0	0.007	0	2.63	0	10% AEP, 10 min burst, Storm 6	
WEST-B7-CAT S1_catch	0.225	0					10% AEP, 10 min burst, Storm 5 10% AEP, 3 hour burst, Storm 2	
PIPE DETAILS	-							
 Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm			
DUMMY-SCALE	0	0	10	8	10% AEP, 10 min burst, Storm 5			
W-B5-CULV1 W-B5-CULV2	0.025	0.57 2.98	56.12	55.63	10% AEP, 15 min burst, Storm 6 10% AEP, 30 min burst, Storm 5			
W-B5-CULV3 W-B5-CULV4	0.249	2.03 0.64	55.046	54.684	10% AEP, 30 min burst, Storm 5 10% AEP, 2 hour burst, Storm 3			
W-B5-CULV5	0.007	0.61	55.393	54.465	10% AEP, 10 min burst, Storm 3			
Pipe20528 W-B5-CULV6	0.064	0.46	52.365	52.363	10% AEP, 10 min burst, Storm 5 10% AEP, 30 min burst, Storm 7			
W-B1-CULV1 Pipe20532	0.02	0.58	68.308	67.923	10% AEP, 30 min burst, Storm 5 10% AEP, 9 hour burst, Storm 5			
1 1620002	0.091	2.00	05.459	05.27	10 /0 AEF, 9 HOULDUISL, SION 5			I

Dec 0.047 1.98 61.333 61.242 10% AFP.3 2 0.037 2.08 61.132 10% AFP.3 3 0.037 2.08 61.132 10% AFP.3 1 0.148 3.44 68.68 58.22 10% AFP.3 1 0.148 3.44 58.68 58.22 10% AFP.1 5 0.20 0 57.28 57.16 10% AFP.1 5 0.242 3.28 52.31 10% AFP.1 10% AFP.1 5 0.242 3.28 52.31 10% AFP.1 10% AFP.1 5 0.242 3.28 42.31 10% AFP.1 10% AFP.1 6 0.13 2.38 42.31 10% AFP.1 10% AFP.1 6 0.13 10.23 48.32 49.32 10% AFP.1 7 0.138 0.28 49.31 10% AFP.1 3 0.12141 0.3 10.12 10.12 10.12 10.12 0.141 0.12	5 min burst, Storm 8 5 min burst, Storm 8 hour burst, Storm 2 hour burst, Storm 2 hour burst, Storm 2 hour burst, Storm 6		
JLV1 0.21 0.037 2.08 61.28 61.72 10% AEP.3 JLV 0.141 1.26 64.49 61.242 10% AEP.3 JLV 0.143 3.44 58.568 55.222 10% AEP.3 J 0 0 57.233 10% AEP.3 10% AEP.3 J 0 0 57.233 10% AEP.3 10% AEP.3 J 0.151 2.26 52.41 10% AEP.3 J 0.151 2.26 49.322 49.17 10% AEP.3 J 0.151 2.264 49.322 49.17 10% AEP.3 J 0.131 2.224 47.259 46.992 10% AEP.3 J 0.131 2.26 10% AEP.3 10% AEP.3 10% AEP.3 J 0.012 0 12.141 3 10% AEP.3 J 0.012 0 12.141 3 10% AEP.3 J 0.012 0 12.141 3 10% AEP.3	hour burst, Storm 2 hour burst, Storm 2 hour burst, Storm 2 hour burst, Storm 6) min burst, Storm 7		
2 0.037 2.08 61.726 61.77 1078 AEP.3 3 0.148 3.44 56.56 55.22 1078 AEP.3 7 0.173 4.09 58.222 57.64 1078 AEP.3 5 0 0 57.303 57.263 1078 AEP.3 5 0.266 2.22 52.93 52.81 1078 AEP.3 5 0.260 2.72 52.93 52.81 1078 AEP.3 5 0.269 4.18 53.23 62.93 1078 AEP.3 5 0.269 4.16 53.23 62.93 1078 AEP.3 6 0.208 4.16 53.23 62.92 1078 AEP.3 6 0.208 4.16 53.23 62.92 1078 AEP.3 0 0.13 10.24 4.928 1078 AEP.3 0 0.18 172.6 46.92 1078 AEP.3 0 0.18 10.22 10.23 1078 AEP.3 0 0.18 10.20	hour burst, Storm 2 hour burst, Storm 2 hour burst, Storm 6 0 min burst, Storm 7		
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0 0.051 0.14 0.138 0 0.029 0.157 0.117 0 0.026 0.123 0.158 0 0.464 0.163 0.703 0.011 0.721 0.101 0.703 0.006 0 1.2141 3 0 0.0488 0.229 0.609 0 0.145 0.414 0.747 0 0.088 0.229 0.609 0 0.11 0.375 0.609 0 0.12141 3 3 0 0.0022 0.354 0.173 0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 0 0.018 0.378 0.498 0 0.044 0.367 0.365 0 0.007 0.389 0.472 0 0.021 0.333 0.635	0 0	0 0	10% AEP, 3 hour burst, Sto
0 0.026 0.123 0.168 0 0.464 0.163 0.703 0.011 0.721 0.101 0.703 0 0.145 0.414 0.703 0 0.145 0.414 0.747 0 0.088 0.229 0.609 0 0.016 0.113 0.609 0 0.006 0 12.141 3 0 0.0022 0.354 0.173 0 0.013 0.312 0.173 0 0.018 0.378 0.498 0.77 0 0.114 0.375 0 0.038 0.242 0.395 10 0.0104 0.411 0.395 0 0.038 0.242 0.395 10 0.0044 0.367 0.179 0 0.0041 0.226 0.635 0 0.021 0.333 0.665 V14 15 0 0.021 0.333<	0.07 1.66	.66 0.56	10% AEP, 30 min burst, St
0 0.464 0.163 0.703 0.011 0.721 0.011 0.703 0 0.006 0 12.141 3 0 0.045 0.414 0.747 0 0.045 0.414 0.747 0 0.088 0.229 0.609 0 0.11 0.375 0.609 0 0.013 0.312 0.173 0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 0 0.018 0.378 0.498 0 0.018 0.378 0.498 0 0.018 0.322 0.045 0 0.004 0.323 0.045 0 0.007 0.389 0.047 0 0.021 0.333 0.635 0 0.021 0.333 0.635 0 0.021 0.375 0.365	0.04 1.41	.41 0.35	10% AEP, 15 min burst, St
0.011 0.721 0.101 0.703 0.006 0 12.141 3 0 0.0145 0.414 0.747 0 0.0188 0.229 0.609 0 0.11 0.375 0.609 0 0.11 0.375 0.609 0 0.011 0.375 0.609 0 0.013 0.312 0.173 0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 0 0.038 0.242 0.395 10 0 0.038 0.242 0.395 10 0 0.044 0.286 0.047 0 0.007 0.389 0.047 0.333 0 0.004 0.143 0.226 0.635 0 0.021 0.333 0.635 0 0.021 0.333 0.635 0	0.03 1.89		10% AEP, 15 min burst, St 10% AEP, 9 hour burst, Sto
0.006 0 12.141 3 0 0.145 0.414 0.747 0 0.088 0.229 0.609 0 0.11 0.375 0.609 0 0.011 0.375 0.609 0 0.022 0.354 0.173 0 0.005 0.512 0.04 0 0.013 0.312 0.173 0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.014 0.411 0.395 0 0.044 0.367 0.179 0 0.044 0.367 0.179 0 0.044 0.367 0.179 0 0.004 0.338 0.047 0 0.004 0.338 0.635 0 0.021 0.333 0.635 0 0.021 0.333 0.635 V14 15 0 0.0241 0.341	0.31 8.44	.44 0.84	10% AEP, 9 hour burst, Sto
0 0.088 0.229 0.609 0 0.11 0.375 0.609 0 0.006 0 12.141 3 0 0.022 0.354 0.173 0 0.013 0.312 0.173 0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 07 0 0.104 0.411 0.395 10 0 0.038 0.242 0.395 10 0 0.044 0.367 0.179 0 0.004 0.433 0.266 0.635 0 0.004 0.433 0.685 141 3 0 0.021 0.333 0.685 141 3 0 0.021 0.333 0.685 141 3 0 0.021 0.333 0.685 141 3 0 0.021 0.337 <td>0 32</td> <td>32 0</td> <td>10% AEP, 45 min burst, St</td>	0 32	32 0	10% AEP, 45 min burst, St
0 0.11 0.375 0.609 0.006 0 12.141 3 0 0.013 0.312 0.173 0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 0 0.014 0.411 0.395 0 0.0038 0.242 0.395 0 0.004 0.378 0.498 0 0.038 0.242 0.395 10 0 0.044 0.367 0.395 10 0 0.044 0.367 0.365 0 0.004 0.322 0.045 0.045 0 0.007 0.389 0.047 0.33 0.635 0 0.021 0.333 0.635 0.047 0.065 0 0.021 0.333 0.635 0.172 0.139 0.142 0.417 0 0.021 0.478	0.12 8.97 0.08 7.31		10% AEP, 10 min burst, St 10% AEP, 10 min burst, St
0.006 0 12.141 3 0 0.022 0.354 0.173 0 0.013 0.312 0.173 0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 0 0.018 0.378 0.498 0 0.038 0.242 0.395 0 0.038 0.242 0.395 0 0.004 0.232 0.045 0 0.007 0.389 0.047 0 0.007 0.389 0.047 0 0.007 0.389 0.047 0 0.012 0 1.2141 0 0.021 0.333 0.635 .V14 15 0 0.026 0.387 0.012 0 1.2141 3 0 0.12 0.478 0.801 0 0.12 0.478 0.801	0.08 7.31		10% AEP, 10 min burst, St 10% AEP, 10 min burst, St
0 0.013 0.312 0.173 0 0.005 0.512 0.04 0.79 0.188 0.296 0.511 0 0.018 0.378 0.498 0 0.018 0.378 0.498 0 0.014 0.411 0.395 0 0.040 0.378 0.498 0 0.038 0.242 0.395 0 0.044 0.367 0.179 0 0.004 0.322 0.045 0 0.007 0.389 0.047 0 0.007 0.389 0.045 0 0.021 0.333 0.635 0 0.021 0.333 0.635 0 0.012 0 12.141 3 0 0.012 0.474 0.801 0 0.172 0.165 0.242 0.099 0.067 0.379 0.188 0 0.265 0.385 0.178	0 32	32 0	10% AEP, 30 min burst, St
0 0.005 0.512 0.04 0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 07 0 0.104 0.378 0.498 07 0 0.014 0.378 0.498 01 0 0.038 0.242 0.395 10 0 0.044 0.367 0.179 0 0.004 0.232 0.045 0 0.007 0.389 0.047 0 0.004 0.133 0.635 0 0.021 0.333 0.635 0 0.021 0.333 0.635 0 0.021 0.333 0.635 V14 15 0 0.047 3 0 0.041 0.142 0.417 0 0.041 0.422 0.411 0 0.172 0.172 0.050 0 0.166 0.213 0.538 0 <t< td=""><td>0.03 2.07</td><td></td><td>10% AEP, 10 min burst, St</td></t<>	0.03 2.07		10% AEP, 10 min burst, St
0.179 0.188 0.296 0.511 0 0.018 0.378 0.498 07 0 0.104 0.411 0.395 0 0.038 0.242 0.395 10 0 0.044 0.367 0.179 0 0.004 0.332 0.045 0 0.004 0.332 0.045 0 0.007 0.389 0.172 0 0.004 0.332 0.045 0 0.007 0.389 0.635 0 0.021 0.333 0.635 V14 15 0 0.087 0.357 0 0.021 0.378 0.635 V14 15 0 0.041 0.142 0 0.12 0.478 0.801 0 0.12 0.478 0.801 0 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0.172 0.175 0.2	0.02 2.07		10% AEP, 10 min burst, St 10% AEP, 2 hour burst, Sto
0 0.018 0.378 0.498 07 0 0.104 0.411 0.395 0 0.038 0.242 0.395 10 0 0.044 0.367 0.179 0 0.0044 0.367 0.179 0 0.004 0.322 0.045 0 0.007 0.389 0.047 0 0.007 0.389 0.047 0 0.004 0.132 0.045 0 0.021 0.333 0.635 0 0.021 0.337 0.365 .V14 15 0 0.087 0.357 0.365 .V14 15 0 0.012 0 12.141 3 0 0.12 0.478 0.801 3 0 0.172 0.165 0.242 3 0.006 1 12.141 3 3 0.172 0.172 0.165 0.242 3 0.178 <t< td=""><td>0.18 6.13</td><td>.13 1.1</td><td>10% AEP, 30 min burst, St</td></t<>	0.18 6.13	.13 1.1	10% AEP, 30 min burst, St
0 0.038 0.242 0.395 10 0 0.044 0.367 0.179 0 0.004 0.232 0.045 0 0.007 0.389 0.047 0 0.004 0.232 0.045 0 0.007 0.389 0.172 0 0.133 0.262 0.635 0 0.021 0.333 0.635 V14 15 0 0.027 0.357 0.365 0.012 0 12.141 3 0 0 0.012 0.478 0.801 0.417 0 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178	0.03 5.98	.98 0.47	10% AEP, 10 min burst, St
IO O 0.044 0.367 0.179 0 0.004 0.232 0.045 0 0.007 0.389 0.047 0 0.359 0.172 0.635 0 0.004 0.143 0.226 0.635 0 0.004 0.143 0.226 0.635 0 0.004 0.143 0.226 0.635 0 0.021 0.333 0.635 V14 15 0 0.087 0.367 0.365 V14 15 0 0.041 0.142 0.417 0 0.012 0 12.141 3 0 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0.188 0.172 0.172 0.105 0.242 0.178 0.0165 0.186 0.213 0.538 0.178 0 0.265 0.385 0.178 0.178 DN BASIN DETAILS	0.11 4.74		10% AEP, 10 min burst, St 10% AEP, 10 min burst, St
0 0.004 0.232 0.045 0 0.007 0.389 0.047 0 0.359 0.172 0.635 0 0.004 0.143 0.226 0.635 0 0.004 0.143 0.226 0.635 0 0.021 0.333 0.635 0.047 10 0.021 0.333 0.635 0.047 0 0.021 0.333 0.635 0.047 0 0.012 0 12.141 3 0 0.041 0.142 0.417 0.066 0 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0.172 0.172 0.105 0.242 0.099 0.066 0.213 0.538 0 0.265 0.385 0.178 0.178 0.178 0 0.265 0.385 0.178 0.091 0.091 0.091 0 0.265 0.385 0.	0.04 4.74		10% AEP, 10 min burst, St 10% AEP, 10 min burst, St
N 0.139 0.359 0.172 0.635 0 0.004 0.143 0.226 0.635 0 0.021 0.333 0.635 V14 15 0 0.087 0.357 0.365 0 0.012 0 12.141 3 0 0.012 0 12.141 3 0 0.012 0.478 0.801 0 0.12 0.478 0.801 0 0.12 0.478 0.801 0.006 0 12.141 3 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.091 0.091 0 0.265 0.091 0.091 0 0.265 0.091 0.091	0.02 0.54	.54 0.43	10% AEP, 2 hour burst, Sto
Image: style	0.03 0.56		10% AEP, 10 min burst, St
0 0.021 0.333 0.635 _V14 15 0 0.087 0.357 0.365 _0.012 0 12.141 3 0 0.041 0.142 0.417 0 0.12 0.478 0.801 0 0.12 0.474 0.337 0.006 0 12.141 3 0.006 0 12.141 3 0.0172 0.478 0.801 3 0.0172 0.172 0.173 0.242 0.099 0.667 0.379 0.188 0.185 0.186 0.213 0.538 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.091 Low Level High Level 0 66.7 100.5 0.091 0.091 63.25 167.8 0.037 0.037 63.25 167.	0.31 7.62		10% AEP, 9 hour burst, Sto 10% AEP, 9 hour burst, Sto
VI4 15 0 0.087 0.357 0.365 0.012 0 12.141 3 0 0.041 0.142 0.417 0 0.041 0.142 0.417 0 0.12 0.478 0.801 0.006 0 12.141 3 0.006 0 12.141 3 0.006 0 12.141 3 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0 0.266 0.385 0.178 0 0.266 0.385 0.178 0 0.266 0.385 0.178 0 0.266 0.385 0.178 0 0.266 0.395 0.077 0 0.266 0.395 0.078 0 0.266 0.091 0.091 0 0.267 100.5 0.091 66.7 100.5 0.091 0.091	0.03 7.62	.62 0.38	10% AEP, 10 min burst, St
0 0.041 0.142 0.417 0 0.12 0.478 0.801 0.006 0 12.141 3 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0.185 0.186 0.213 0.538 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.0365 0.0178 0 0.265 0.0365 0.178 0 0.265 0.037 0.091 0 0.265 0.037 0.091 0 0.265 0.037 0.037 0.62.39 121.3 0.066 0.029 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 <td>0.09 4.39</td> <td>.39 0.76</td> <td>10% AEP, 10 min burst, St</td>	0.09 4.39	.39 0.76	10% AEP, 10 min burst, St
0 0.12 0.478 0.801 0.006 0 12.141 3 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0.185 0.186 0.213 0.538 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.391 0.091 0 0.265 0.091 0.091 0 0.265 0.091 0.091 0 0.265 0.091 0.091 66.7 100.5 0.091 0.091 62.39 121.3 0.106 0.029 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206	0 32		10% AEP, 1 hour burst, Sto 10% AEP, 1 hour burst, Sto
0.006 0 12.141 3 0.172 0.172 0.105 0.242 0.099 0.067 0.379 0.188 0.185 0.186 0.213 0.538 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 Max VL Max Q Max Q Max VL Max Q Ione Level High Level 66.7 100.5 0.091 0.091 0.091 63.25 167.8 0.037 0.037 0.37 59.61 92.9 0.179 0.148 54.13 93.8	0.02 5.01		10% AEP, 10 min burst, St
0.099 0.067 0.379 0.188 0.185 0.186 0.213 0.538 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 0.265 0.385 0.178 0 Max Q Max Q Max Q 100.5 0.091 Low Level High Level 66.7 100.5 0.091 0.091 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206	0 32	32 0	10% AEP, 3 hour burst, Sto
0.185 0.186 0.213 0.538 0 0.265 0.385 0.178 DN BASIN DETAILS Max VU Max Q Max Q Max Q 66.7 100.5 0.091 Low Level High Level 66.7 101.5 0.003 0.037 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206			10% AEP, 3 hour burst, Ste
0 0.265 0.385 0.178 DN BASIN DETAILS Max WL Max Q Max Q Max Q Max WL Max VO Total Low Level High Level 66.7 100.5 0.091 0.091 62.39 121.3 0.106 0.029 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206	0.12 2.25		10% AEP, 9 hour burst, Sto 10% AEP, 9 hour burst, Sto
Max WL MaxVol Max Q <	0.25 2.13		10% AEP, 3 hour burst, Ste
Max WL MaxVol Max Q Max Q Max Q Max Q 66.7 Total Low Level High Level 66.7 100.5 0.091 0.091 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206			
Max WL MaxVol Max Q Max Q Max Q Max Q 66.7 Total Low Level High Level 66.7 100.5 0.091 0.091 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206			
Total Low Level High Level 66.7 100.5 0.091 0.091 62.39 121.3 0.106 0.029 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206			
66.7 100.5 0.091 0.091 62.39 121.3 0.106 0.029 63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206			
63.25 167.8 0.037 0.037 59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206	0		
59.61 92.9 0.179 0.148 58.42 67 0 0 54.13 93.8 0.242 0.206	0.077		
58.42 67 0 0 54.13 93.8 0.242 0.206	0.031		
54.13 93.8 0.242 0.206	0		
j 52.31 504.51 0.151 0.1311	0.037		
	0.019		
or 12546218 AlbanyMotorPark_west run at 13:48:04 on 14/7/2021 using versi	n 2020.036		
or 12546218_AI	54.13 93.8 0.242 0.206 52.3 504.5 0.15 0.131	54.13 93.8 0.242 0.206 0.037 52.3 504.5 0.15 0.131 0.019	54.13 93.8 0.242 0.206 0.037 52.3 504.5 0.15 0.131 0.019

	Stage 1A (WEST) DRA DRAINS results prepar			6					
	1% AEP								
	PIT / NODE DETAILS Name	Max HGL	Max Pond	Max Surface	Version 8 Max Pond	Min	Overflow	Constraint	
			HGL	Flow Arriving	Volume	Freeboard	(cu.m/s)		
	DUMMY-SCALE2	10		(cu.m/s) 0	(cu.m)	<u>(m)</u>			
	DUMMY-SCALE1	8		0					
	W1-B1-01-US W-B1-02-US	69 68.65		0					
	W-B1-03-US	68.65		0					
	W-B1-04-US W-B1-05-US	67 66.71		0					
	W- B4-01-US	62		0					
	W-B4-02-US W-B5-CULV1-HW	68.5 56.72		0.05		0.28	0	None	
	W-B5-CULV1-DS	56.57		0					
	W-B5-CULV2-HW W-B5-CULV2-DS	56.56 55.66		0.789		-0.06	0.243	Headwall height/system capacity	
	W-B5-CULV3-HW	55.45		0.864		0.05	0	None	
	W-B5-CULV3-DS W-B5-CULV4-HW	54.61 57.06		0.317		0.94	0	None	
	W-B5-CULV4-DS	56.57		0.032			0	Nana	
	W-B5-CULV5-HW W-B5-CULV5-DS	55.5 54.51		0.032		I	0	None	
	W-B7-CULV2-HW	56.2 55.51		0.148		0.8	0	None	
	W-B7-CULV2-DS W-B5-CULV6-HW	52.64		0.129		0.36	0	None	
	N87219	52.62 68.4		0.045		0.6		None	
	W-B1-CULV1-HW W1-01-DS	67.98		0.151		0.6	0		
	N87159 N87076	65.29 64.14		0.032					
	N87168	61.39		0					
	W-EXT02-US W-EXT	61.36 60.79		0.252					
	W-EXT-CULV1-HW	60.52		1.092		-0.02	0.051	Headwall height/system capacity	
	W-EXT-CULV1-DS N87207	59.26 61.8		0.321					_]
	N87255	61.12		0					
	W-EXT-HW N87181	65.04 58.35		0.694		-0.04	0.176	Headwall height/system capacity	
	W-B5-03-DS	57.25		0.239					
	W-B5-03-US W-B5-06-US	62 63.5		0					
	W-B5-01-US	59		0					
	W-B5-02-US W-B5-05-US	57.5 58		0					
	W-B5-08-US	56		0					
	W-B5-09-US W-B5-11-US	58 58		0					
	W-B5-12-US	57.5		0					
	N87237 N87238	57.39 57.19		0					
	W-B6-01-US	59.2		0					
	N87225 N87218	52.93 52.63		0.134					
	W-B5-16-US	56.5		0					
	W-B5-CULV14-US W-B7-CULV1-HW	59.2 52.62		0 1.016		0.38	0	None	
	N87244	49.54		0					
	N87245 W-B7-02-US	49.27 62.5		0.121					
	HW12	54.03		0.745		-0.03	0.107	Headwall height/system capacity	
	N87149 HW13	51.94 48.04		0.373		-0.04	0.153	Headwall height/system capacity	
	N87150 W-B3-01-US	46.83		0.448					
-	S1 US	67.2 57.5		0					
	SUB-CATCHMENT DE								
	Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm	
		Flow Q (cu.m/s)	Max Q (cu.m/s)	Max Q (cu.m/s)	Tc (min)	Tc (min)	Tc (min)]
	W-B5-CULV1-CAT	0.082	0	0.082	0	2.33	1.13	1% AEP, 15 min burst, Storm 8	
	W-B5-CULV2-CAT W-B5-CULV3-CAT	0.074 0.319						1% AEP, 10 min burst, Storm 4 1% AEP, 15 min burst, Storm 4	
	W-B5-CULV3-DS-CAT	0.091	0	0.091	0	1.9	0.92	1% AEP, 15 min burst, Storm 4	
	W-B5-CULV4-CAT W-B5-CULV5-CAT	0.018						1% AEP, 15 min burst, Storm 8 1% AEP, 15 min burst, Storm 4	
	W-B5-CULV6-CAT	0.215	0	0.215	0	1.98	0.96	1% AEP, 15 min burst, Storm 8	
	W-B1-03-CAT W-B1-01-CAT	0.075					1.22	1% AEP, 15 min burst, Storm 4 1% AEP, 15 min burst, Storm 4	
	WEST-B1-CAT	0.211	0	0.211	0	3.84	1.87	1% AEP, 10 min burst, Storm 4	
	WEST-B2-CAT W-EXT-CAT	0.435				0		1% AEP, 10 min burst, Storm 4 1% AEP, 15 min burst, Storm 8	
	W-EXT04-CAT	0.068	0	0.068	0	1.53	0.74	1% AEP, 15 min burst, Storm 8	
	WEST-B3-CAT CulvW_ext	0.324 0.479						1% AEP, 10 min burst, Storm 4 1% AEP, 3 hour burst, Storm 8	
	WEST-B4-CAT	0.589	0.516	0.082	3.03	7.05	0	1% AEP, 15 min burst, Storm 8	
	W-B5-03-CAT WEST-B6-CAT	0.032	0	0.281	0	2.49	1.22	1% AEP, 15 min burst, Storm 8 1% AEP, 15 min burst, Storm 8	
	WEST-B5-CAT W-B7-01-CAT	0.162	0	0.162		2.55	1.24	1% AEP, 15 min burst, Storm 8	
	WEST-B7-CAT	0.427	0	0.427	0	2.79	1.36	1% AEP, 10 min burst, Storm 4 1% AEP, 10 min burst, Storm 4	
	S1_catch	1.641	0	1.641	0	19.68	0	1% AEP, 25 min burst, Storm 8	
	PIPE DETAILS Name	Max Q	Max V	Max U/S	May D/S	Due to Storm			
		(cu.m/s)	(m/s)	HGL (m)	HGL (m)				
	DUMMY-SCALE W-B5-CULV1	0.069	0	10	8	1% AEP, 10 min burst, Storm 5 1% AEP, 15 min burst, Storm 8			
	W-B5-CULV2	0.286	3.27	56.204	55.668	1% AEP, 15 min burst, Storm 1			
	W-B5-CULV3 W-B5-CULV4	0.517 0.017		55.197	54.783	1% AEP, 30 min burst, Storm 3 1% AEP, 15 min burst, Storm 8			
	W-B5-CULV5	0.033	1.31	55.496	54.507	1% AEP, 15 min burst, Storm 8			
	Pipe20528 W-B5-CULV6	0.069	2.46			1% AEP, 2 hour burst, Storm 10 1% AEP, 15 min burst, Storm 8			
	W-B1-CULV1	0.053	0.9	68.389	67.978	1% AEP, 15 min burst, Storm 1			
	Pipe20532	0.143	3.23	65.513	65.295	1% AEP, 2 hour burst, Storm 10			

Pipe20533	0.143	3.27	65.295		1% AEP, 2 hour burst, Storm 10			
Pipe20566	0.097	2.12 2.53	61.516 61.388		1% AEP, 15 min burst, Storm 1 1% AEP, 15 min burst, Storm 1			
Pipe20567 W-EXT-CULV1	0.115	2.53	60.157		1% AEP, 2 hour burst, Storm 7			
Pipe20702	0.146	3.12	62.016	61.801	1% AEP, 30 min burst, Storm 5			
Pipe20716	0.146	3.28	61.801		1% AEP, 30 min burst, Storm 5			
W-EXT-CULV Pipe20591	0.303	4.55	64.851 58.69		1% AEP, 3 hour burst, Storm 8 1% AEP, 15 min burst, Storm 8			
Pipe20597	0.362	4.94	58.351	57.711	1% AEP, 15 min burst, Storm 8			
Pipe20785	0.069	1.89			1% AEP, 2 hour burst, Storm 10			
Pipe20790 Pipe20745	0.069	1.98 3.79			1% AEP, 2 hour burst, Storm 10 1% AEP, 30 min burst, Storm 8			
Pipe20746	0.583	4.08	52.933		1% AEP, 30 min burst, Storm 8			
Pipe20525	0.49	1.54	52.55		1% AEP, 30 min burst, Storm 8			
Pipe20821 Pipe20830	0.506	3.6 3.75			1% AEP, 2 hour burst, Storm 2 1% AEP, 2 hour burst, Storm 2			
Pipe20526	0.362	4.84	53.309		1% AEP, 2 hour burst, Storm 7			
Pipe20527	0.346	2.82	47.498	47.124	1% AEP, 1 hour burst, Storm 6			
CHANNEL DETAILS								
Name	Max Q	Max V			Due to Storm			
	(cu.m/s)	(m/s)						
OVERFLOW ROUTE								
Name		Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm
O134039	0.014	0	12.141	3	0	32		1% AEP, 30 min burst, Storm 8
O134055 O137112	0.014	0		3	0	32 32		1% AEP, 30 min burst, Storm 8 1% AEP, 15 min burst, Storm 1
0137112	0.006	0		3	0	32		1% AEP, 15 min burst, Storm 1
O137914	0.007	0	12.141	3	0	32	0	1% AEP, 15 min burst, Storm 8
O137918	0.014	0		3	0	32		1% AEP, 15 min burst, Storm 8
O90392 O90396	0.007	0		3	0	32		1% AEP, 2 hour burst, Storm 2 1% AEP, 2 hour burst, Storm 2
OF76225	0.255	0.255	0.996	0.707	0.24	8.48	1.34	1% AEP, 15 min burst, Storm 8
OF76315	0.469	0.469	1.729	1.124	0.45	8.99		1% AEP, 2 hour burst, Storm 7
OF76316 OF76323	0.069	0.069	1.286	0.996	0.11	<u>11.96</u> 0	1.14	1% AEP, 2 hour burst, Storm 10
OF76325	0.173	0.173	19.113	0.348	0.01	32	0.51	1% AEP, 15 min burst, Storm 1
OF76345	0.164	0.164	1.305	0.025	0.1	4		1% AEP, 15 min burst, Storm 8
OF76352 OF76354	0.095	0.095		0.778	0.04	9.34		1% AEP, 15 min burst, Storm 9
OF76357	0.095	0.095	0.364	0.042	0.04	9.34		1% AEP, 15 min burst, Storm 9 1% AEP, 15 min burst, Storm 1
OF76359	0.527	0.527	1.031	0.649	0.38	7.79	1.62	1% AEP, 15 min burst, Storm 1
OF76363 OF76364	0.017	0.017	0.757	0.065	0.04	0.78	07	1% AEP, 15 min burst, Storm 8
OF76369	0.017	0.017		0.065	0.04	0.78	0.7	
OF76373	0	0	1.322	0	0	0	0	
OF76375	0.051	0.051	0.644	0.017	0.01	6.66		1% AEP, 2 hour burst, Storm 7
OF76377 OF76384	0.107	0.107	0.79	0.021	0.02	7.52		1% AEP, 2 hour burst, Storm 7 1% AEP, 2 hour burst, Storm 7
OF76391	0.001	0.001	1.379	0.001	0	0.13	0	1% AEP, 30 min burst, Storm 8
OF76405	0.583	0.583	1.159	1.064	0.36	12.77		1% AEP, 30 min burst, Storm 8
OF76407 OF76410	0.243	0.243	0.769	1.064	0.05	12.77	0.06	1% AEP, 9 hour burst, Storm 10
OF76413	0	0	0.455	0	0	0	0	
OF76415	0	0	0.464	0	0	0		
OF76418 OF76420	0.069	0.069		0.288	0.13	0 3.45		1% AEP, 2 hour burst, Storm 10
OF76420 OF76424	0.069	0.069		0.288	0.13	3.45	1.43	
OF76426	0	0	19.114	0	0	0	0	
OF76429	0.528	0.517	0.664	1.046	0.32	12.56		1% AEP, 2 hour burst, Storm 2 1% AEP, 1 hour burst, Storm 6
OF76432 OF76434	0.499	0.499	19.225 0.526	0.032	0.02	32 9.12		1% AEP, 1 hour burst, Storm 6 1% AEP, 1 hour burst, Storm 6
OF76436	0	0	0.526	0	0	0	0	
OF76444	0.176	0.176		0.684	0.01	32		1% AEP, 3 hour burst, Storm 8
OF76451 W-B1-01	0.146	0.146	1.792 0.412	1.423 0.201	0.21	17.07		1% AEP, 30 min burst, Storm 5 1% AEP, 15 min burst, Storm 8
W-B1-02	0	0.073	0.464	0.178	0.07	2.13	0.39	1% AEP, 15 min burst, Storm 8
W-B1-03	0				0.05	3.03		1% AEP, 15 min burst, Storm 8
W-B1-04 W-B1-05	0.012	0.473	0.48	0.707	1.17	8.48 8.48		1% AEP, 9 hour burst, Storm 2 1% AEP, 9 hour burst, Storm 2
W-B2-O1	0.006	0	12.141	3	0	32	0	1% AEP, 15 min burst, Storm 1
W-B3-01	0	0.269	1.221	0.808	0.18	9.7	1.04	1% AEP, 10 min burst, Storm 4
W-B4-01 W-B4-02	0	0.183	0.676	0.684	0.13	8.21 8.21		1% AEP, 10 min burst, Storm 6 1% AEP, 10 min burst, Storm 10
W-B4-02 W-B4-01	0.007	0.22	12.141	3	0	32	0	1% AEP, 15 min burst, Storm 8
W-B5-01	0	0.052	1.044	0.29	0.06	3.47	0.61	1% AEP, 15 min burst, Storm 8
W-B5-02 W-B5-03	0	0.03	0.92	0.29	0.04	3.47		1% AEP, 15 min burst, Storm 8 1% AEP, 15 min burst, Storm 1
W-B5-03 W-B5-04	0.551	0.574	0.872	0.763	0.07	9.15	1.45	1% AEP, 15 min burst, Storm 8
W-B5-05	0	0.04	1.113	0.763	0.05	9.15	0.59	1% AEP, 15 min burst, Storm 8
W-B5-06 07 W-B5-08	0	0.235	1.213 0.714	0.649	0.19	7.79		1% AEP, 15 min burst, Storm 8 1% AEP, 15 min burst, Storm 8
W-B5-09 10	0	0.082	1.083	0.649	0.04	3.49		1% AEP, 10 min burst, Storm 4
W-B5-11	0	0.018	0.685	0.077	0.04	0.92	0.59	1% AEP, 15 min burst, Storm 8
W-B5-12 W-B5-13A	0.548	0.016	1.147	0.063	0.04	0.75		1% AEP, 15 min burst, Storm 8
W-B5-13A W-B5-13B	0.548	0.552		0.753	0.3	9.03		1% AEP, 30 min burst, Storm 8 1% AEP, 9 hour burst, Storm 5
W-B5-16	0	0.054	0.982	0.753	0.06	9.03	0.55	1% AEP, 10 min burst, Storm 4
W-B5-CULV14 15 W-B5-O1	0.014	0.196	1.054 12.141	0.643	0.16	7.72		1% AEP, 10 min burst, Storm 9
W-B5-01 W-B6-01	0.014	0.159		0.569	0.07	6.82		1% AEP, 30 min burst, Storm 8 1% AEP, 15 min burst, Storm 8
W-B7-02	0	0.24	1.408	0.94	0.16	11.28	0.97	1% AEP, 10 min burst, Storm 4
W-B7-O1	0.007	0 524		3	0	32		1% AEP, 2 hour burst, Storm 2
W-EXT02 W-EXT03	0.521	0.524 0.149	0.31	0.363	0.31	4.36 3.52		1% AEP, 30 min burst, Storm 8 1% AEP, 2 hour burst, Storm 10
W-EXT03	0.143	0.149	0.629	1.423	0.34	17.07		1% AEP, 1 hour burst, Storm 7
W-S1	0	1.604	1.134	0.341	0.78	4.1		1% AEP, 20 min burst, Storm 4
DETENTION BASIN D	ETAILS							
Name		MaxVol	Max Q		Max Q			
WEET D4	00 7	401-	Total		High Level			
WEST-B1 WEST-B2	66.71 62.43	101.3 143.9	0.143	0.143	0.192			
WEST-B2 WEST-B3	63.31	143.9	0.289	0.097	0.192			
WEST-B4	59.68	109.3	0.526	0.334	0.192			
WEST-B6 WEST-B5	58.57 54.25	106.2 118.1	0.069	0.069	0.041			
WEST-B5	54.25	628.9			0.041			
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	5-CULV14	15, W-B5-11	3B, W-B5-1	3A, W-B5-	 			5, W-B5-04			W-B4-02, /		

Stage 1B (EAST) DRAINS Inpu	t Data																					
PIT / NODE DETAILS Name	Туре	Family	Version 15 Size		Pressure Change	Surface Elev (m)	Max Pond Depth (m)	Base Inflow	Blocking Factor	x	v	Bolt-down lid	id	Part Full Shock Los	Inflow Hydrograp	Pit is	Internal Width	Inflow is Misaligned	Minor Safe	Major Safe Pond Dept	h	
	Node			(cu.m)	Coeff. Ku	60.5		(cu.m/s) 0		568175	6133948		97325		No		(mm)		(m)	(m)		
N57	Node Node					9 58 56		0		567155 568106 568093	6133961		97367 97505 97516		No No No							
E-B2-01-US E-B5-CULV1-HW	Node Headwall				0.5	63.5 68		0		568158 568616	6134105 6133924		97469 97687		No							
N302	Node Node					67.5 64.5 10.5		0		568663 568673 568871	6133907		1336024 99131 97701		No No No				<u> </u>			
DUMMY-SCALE1 E-B5-01-US	Node Node					8		0		568934 568522	6134070 6133990		97702 97795		No No							
E-B7-CULV2-HW	Node Headwall				0.5	72.5		0		568460	6134258 6134257		97815 97829		No							
E-B7-04-US E-B7-05-US	Node Node					72 73 73		0		568452 568445 568490	6134203 6134258		97831 97846 97849		No No No							
E-B9-CULV1-HW E-B9-CULV1-DS	Headwall Node				0.5	68.5 67.5		0		568636 568622	6134618 6134619		97880 97882		No							
E-B9-08-US	Node Node					73 68.5 71		0		568632 568636 568577	6134734		97904 97910 97923		No No No							
E-B9-06-US E-B9-CULV2-HW	Node Headwall				0.5	68 66		0		568622 568578 568547	6134629		97926 97939		No							
E-B9-03-US	Node Node Node					64 71 67		0		568547 568560 568596	6134465		97960 97945 97951		No No No							
E-B9-01-US E-B9-02-US	Node Node					69.5 65.5		0		568513 568566	6134498 6134737		97977 97985		No No							
N297	Node Node					61.5 57 70		0		568167 568128 568465	6134265		99152 99115 98259		No No No							
N296 N305	Node Node					62.225 59.5		0		568511 567984	6134661 6133886		99112 99135		No No							
N61649	Node Node Node					53.5 66 63		0		567968 568245 568227	6134283		99134 1337247 99116		No No No							
	Node Node					62.5		0		568520 568485	6134829		100059 99109		No No							
E-B9-CULV3-HW	Headwall Node				0.5	62 60 63		0		568491 568450	6134668 6134694		98030 98032 98042		No							
E-B10-02-US	Node Node Node					63.5 65.5		0		568467 568382 568569	6134548		98042 98052 98066		No No No							
E-B10-CULV1-HW E-B10-CULV1-DS	Headwall Node				0.5	65.5 64		0		568607 568579	6134840 6134834		98068 98071		No							
E-B10-04-US E-B10-05-US	Node Node Node					67 68 66.5		0		568598 568622 568208	6134759 6134757		98119 98121 98149		No No No							
E-B6-02-US E-B6-03-US	Node Node					69.5 63.5		0		568325 568373	6134226 6134534		98154 98192		No No							
E-B7-01-US E-B7-02-DS	Node Node					69.5 69.5		0		568313 568333	6134256		98206 98218		No No							
E-B7-02-US	Node Node					70.5 70.5 72		0		568362 568365 568416	6134100		98221 98223 98225		No No No				 			
E-B7-B E-B7-CULV1-HW	Node Headwall	10.12			0.5	68 69 67.91		0		568366 568363	6134360 6134359		98245 98248 183745		No							
E-B7-CULV1-DS	Sag Node Node	MR High F	WA Main	0.5	1.5	67.91 65.5 72	0.5	0	0	568360 568305 568418	6134359 6134365	No	183745 98277 98287		No No No	New	1050	Yes	0.3	0.5		
E-B7-09-US E-B7-10-US	Node Node					70 69.5		0		568466 568503	6134433 6134488		98294 98311		No No							
E-B3-02-US	Node Node Node					65.1 70.6 72		0		568287 568368 568422	6134298 6134088 6134111		98326 98339 98341		No No No							
E-B4-01-DS E-B4-01-US	Node Node					71.25		0		568469 568406	6134074 6134211		98364 98367		No No							
E-B4-02-US	Node Node					71.1		0			6134198		98381 98384		No No							
E-B1-CULV1-DS	Node Node					58.5 58 60.5		0		568117 568017 568147	6133910		98398 98405 98415		No No No							
E-B1-03-SPLIT E-B1-03-US	Node Node					65.5 68.5 68.5		0		568286 568265	6133938 6134075		98443 98448		No No							
E-B1-04-US	Node Node Sag	MR High F	WA Main	20	1.5	68.5 69.5 69	0.5	0		568373 568317	6133909	No	98452 98455 98537		No No No	New	1050	No	0.15	0.3		
E-B7-CULV3-DS N266	Node Node			20	1.3	67 66.75	0.5	0		568293 568298	6134250 6134276		98138 98633		No No		.000		3.15	0.3		
E-B2-02-DS DUMMY E-B8-01A-US	Node Node					58 71.2		0		568127 568622	6133951 6134476		98869 98976		No No No							
N388 N511	Node Node Node					73 56 67		0		568508 568035 568387	6133940 6134457		98979 100415 101985		No No				L			
N539 Pit1296	Node Sag	MR High F	WA Main	0.25	1.5	51.5 71.8	0.4	0	0	567984 568465	6133984 6134072	No	102852 171193	1 x Ku	No No	New	1050	No	0.3	0.3		
N299	Node Node					71 68 64		0		568423 568372 568694	6133891		1334698 99125 807388		No No No				 			
N38868 HW1478	Node Headwall				0.5	47 49.5		0		567911 567937	6134045 6134017		807705 807769		No							
N59 N38875 HW1479	Node Node Headwall				0.5	48.5 50 53		0		567924 568077 568107	6134294		97518 807976 807978		No No				-			
N38873 HW1480	Node Headwall				0.5	52 57.5		0		568094 568328	6134287 6134678		807973 808445		No							
N38880	Node Node					56.5 55		0		568308 568292	6134661		808406 808616		No No							
DETENTION BASIN DETAILS Name	Elev	Surf. Area	Not Used	Outlet Typ	к	Dia(mm)	Centre RL	Pit Familv	Pit Type	x	v	HED	Crest RL	Crest Lenc					L			
EAST-B2	57	500 1150		Pit/Sump				MR High I	WA Main		6133959	No			97460							
EAST-B5 EAST-B6	66 67.5 61	300 1300 600		Pit/Sump Pit/Sump			 		WA Main WA Main	568660	6133924				97684							
EAST-B8	61.5 70.5	1000 250		Pit/Sump					WA Main		6134412				97998						-	-
EAST-B9	71.5 63 64	750 950 1800		Pit/Sump				MR High I	WA Main	568527	6134653	No	 		98000				<u> </u>			
EAST-B1	58 59.5	145 950		Pit/Sump					WA Main		6133871				98006							
EAST-B7 EAST-B10	65 66 62	300 850 430		Pit/Sump Pit/Sump					WA Main WA Main		6134286 6134830				98017 98023							
EAST-B10 Bio-retention	62.5	800		None							6134333				98023							
EAST-B4	73.1 73.5 71 71.5	490 1750 250 550		Pit/Sump				MR High I	WA Main		6133989				98013							
EAST-B3	71.5 70 71	550 350 950		Pit/Sump				MR High I	WA Main	568430	6133991	No			98011							
SUB-CATCHMENT DETAILS			Douted	Orres	Sure	Barrad	Grace	Que-	Boy	Gran	Sur-	Boy	Orr	Sur-	Bound	Orre	Sur-	Loc T	Cutter	Cutter.	Gutter	Pointe"
	Node	Total Area (ha)	Area %	Grass Area %	Area %	Paved Time (min)	Grass Time (min)	Supp Time (min)	Paved Length (m)	Length (m)	Supp Length (m)	Slope(%) %	%	%	Paved Rough	Rough	Rough	Lag Time or Factor	Gutter Length (m)	Gutter Slope %	Gutter FlowFacto	Rainfall Multiplier
EAST-B2-CAT E-B5	EAST-B2 E-B5-CULV1-HW	2.568 3.378	20	0	30	0	0	0	117.12	117.12	117.12	5.746	-1	5.746	0.013	0.053	0.016	0				1
EAST-B5-CAT E-B7-A E-B9-A	EAST-B5 E-B7-CULV2-HW E-B9-CULV1-HW	2.338 0.664 3.022	0		0	0	0	0	-1 64.619 -1	295.09 -1 75.763	-1 -1	-1 0.889 -1	2.37 -1 1.105	-1 -1 -1	-1 0.013 -1	0.053	-1 -1 -1	0				1
	E-B9-CULV1-DS E-B9-CULV2-HW	0.63	30 0	70 100	0	0	0	0	17.65	17.65 33.011	-1	4.27	4.27 3.799	-1	0.013	0.053	-1					1
E-B9-D EAST-B6-CAT EAST-B8-CAT	E-B9-CULV2-DS EAST-B6 EAST-B8	1.097 5.475 0.838	35 10 40	30	35 10 0	0	0	0	39.502 64.734 13.81	39.502 64.734 13.81	39.502 64.734	5.326 7.72 3.32	5.326 7.72 3.32	5.326 7.72	0.013 0.013 0.013	0.053 0.053 0.053	0.016	0				1
EAST-B9-CAT	EAST-B8 EAST-B9 EAST-B1	0.838 0.116 1.9121	40 0 50	100 40	0	0	0	0	-1	16.962 46.71	-1 -1 46.71	3.32 -1 3.178	5.9	-1 -1 3.178	0.013 -1 0.013	0.053	-1 -1 0.016	0				1 1 1 1 1
EAST-B7-CAT EAST-B10-CAT	EAST-B7 EAST-B10	0.33 3.7674	0 20	100	0	0	0	0	-1 31.74	103.06 31.74	-1 31.74	-1 4.69	4.85	-1 4.69	-1 0.013	0.053	-1 0.016	0				1
E-B7-02-CAT	E-B10-CULV1-HW E-B10-CULV1-DS E-B7-02-DS	0.381 0.2796 0.594	0 40 0	100	20 10 0	0	0	000000000000000000000000000000000000000	24.61	24.61 46.395	-1	4.238 6.095 -1	6.095	4.238 6.095 -1	0.013 0.013 -1	0.053 0.053 0.053	0.016 0.016 -1	0				1 1 1
E-B7-03-CAT E-B7-B-CAT	E-B7-03-DS E-B7-CULV1-HW	0.384	60 0	20	20	0	0	0	33.111	33.111 129.98	33.111	1.51	1.51	1.51	0.013	0.053	0.016	0				1
	Pit1448 E-B7-CULV1-DS E-B7-11-DS	1.255 0.1624 0.236	82.5 0	100	7.5 0	0	0	0		35.342 50.268 23.373	35.342 50.268 -1	1.448 1.989 -1	1.448 1.989 2.139	1.448 1.989 -1	0.013 0.013 -1	0.053 0.053 0.053	0.016 0.016 -1	0				1
E-B4-02-CAT	E-B1-11-DS E-B4-02-DS E-B1-CULV1-DS E-B1-03-SPLIT	1.245	100	0 80	0	0	0	0	40.879	-1 40.879	-1 40.879	0.736	-1 4.892	-1 4.892	0.013	-1	-1 0.016					1
E-B1-04-CAT	E-B1-03-SPLIT E-B1-04-DS Pit8	1.056 0.474 1.026	50 0 20	10	40 0 20	0	0	0	58.809 -1 50.013	58.809 19.545 50.013	58.809 -1 50.013	3.401 -1 1.999	3.401 5.116 1.999	3.401 -1 1.999	0.013 -1 0.013	0.053 0.053 0.053	0.016	0				1
Cat314	Pit8 N266 Bio-retention	1.026 0.33 1.772	20	100	20 0	0	0	0	-1	50.013 103.06 173.62	50.013 -1 -1	-1	4.85	1.999 -1 -1	0.013 -1 -1	0.053 0.053	-1 -1	0				1
E-B1-01-CAT E-B7-10-CATA	N388 N511	0.274 0.6496	40 10	50	10	0	0	0	34.788 50.268	34.788	34.788 50.268	5.749 1.989	5.749	5.749 1.989	0.013	0.053	0.016	0			-	1
EAST-B4-CAT	Pit1296 EAST-B4 EAST-B3	0.384 0.182 2.133	100 50 50	50	0 0 10	0	0	0	57.265	-1 57.265 39.23	-1 57.265 39.23	2.277 0.87 2.2	-1 0.87 2.2	-1 0.87 2.2	0.013 0.013 0.013	-1 0.053 0.053	-1 0.016 0.016	0				1 1 1
PIPE DETAILS																						
Name DUMMY-SCALE		To DUMMY-S	Length (m) 161.044	U/S IL (m) 10	D/S IL (m) 8	(%)	Type uPVC, under roads, 1% minimum	Dia (mm) 150	I.D. (mm) 154	Rough 0.012			Chg From DUMMY-S	At Chg 0	Chg (m)				etc (m)			
E-B5-CULV1	E-B5-CULV1-HW Pit1448	EAST-B5 E-B7-CUL	15 55.2	66.91 66.91	66 65.5	6.07 2.55	Concrete, under roads, 1% minimu Concrete, under roads, 1% minimu	450 450	450 450	0.013	NewFixed NewFixed	1	E-B5-CUL Pit1448	0								
E-B7-CULV2 E-B7-CULV3 E-B9-CULV1	E-B7-CULV2-HW Pit8	E-B7-CUL E-B7-CUL E-B9-CUL	13.4 97.1 13.7	72.41 67.485	72 67 66.41	0.5	Concrete, under roads, 1% minimu Concrete, under roads, 1% minimu Concrete, under roads, 1% minimu	450 450 450	450 450 450	0.013	NewFixed New	1	E-B7-CUL Pit8 E-B9-CUL	0								
E-B9-CULV2	E-B9-CULV2-HW	E-B9-CUL E-B9-CUL E-B9-CUL	13.7 28.3 49	64.91	66.41 64 60	3.22	Concrete, under roads, 1% minimu Concrete, under roads, 1% minimu Concrete, under roads, 1% minimu	450 450 450	450	0.013	NewFixed NewFixed NewFixed	1	E-B9-CUL E-B9-CUL E-B9-CUL	0					-			
												· · · · ·				-				-		

	P13783	EAST-B3	N61629	2	69.3	69.233	3.35 Concrete. under roads. 0.5% mini	r 600	600	0.013	NewFixed	1	EAST-B3	0				r			,	
Norme Norme <t< td=""><td>P13826</td><td>EAST-B5</td><td>N61643</td><td>1.5</td><td>65.3</td><td>65.24</td><td>4 Concrete. under roads. 0.5% mini</td><td>r 450</td><td>450</td><td>0.013</td><td>NewFixed</td><td>1</td><td>EAST-B5</td><td></td><td></td><td>_</td><td></td><td></td><td></td><td>_</td><td></td><td></td></t<>	P13826	EAST-B5	N61643	1.5	65.3	65.24	4 Concrete. under roads. 0.5% mini	r 450	450	0.013	NewFixed	1	EAST-B5			_				_		
	P21	N57	N58	8.5	56.255	56	3 Concrete, under roads, 1% minim	450	450	0.013	New	1	N57	0								
Name Name Name Name N	Pipe10	EAST-B2	N57		56.3	56.255	3 Concrete, under roads, 1% minim	u 450	450	0.013	NewFixed	1	EAST-B2	0								
	Pipe177	N61629	N299	58	69.233	68	2.13 Concrete, under roads, 0.5% mini	r 600	600	0.013	NewFixed	1	N61629	0								
No. No. No. No. No.	Pipe179	N61643	EAST-B3 N302		65.24	64.5	4 Concrete. under roads. 0.5% mini	r 450	450	0.013	NewFixed	1	N61643									
Name Name Name Name N		N306	N297	18	60.155	55.5	12.25 Concrete, under roads, 0.5% mini	r 600	600	0.013	New	1	N306									
	Pipe184 Pipe185		N296	15	62.3		0.5 Concrete, under roads, 0.5% mini	r 450	450			1	EAST-B9	0								
	Pipe186 Pipe213	N367 EAST-B1	N294 N305	48	61.268 57		1.6 Concrete, under roads, 0.5% mini 5.67 Concrete, under roads, 0.5% mini	600 450	600	0.013	New NewFixed	1	N367 EAST-B1									
	Pipe220	N305	N304	60	56.915	53.5	5.69 Concrete, under roads, 0.5% mini	r 450	450	0.013	New	1	N305	0				<u> </u>				
	Pipe2927	Pit1296	EAST-B4		71.4	71	0.42 Concrete. under roads. 0.5% mini	r 375	375	0.013	NewFixed	1	Pit1296	0								
	Pipe8633	HW1478	N59		48.41	47.41	5 Concrete, under roads, 0.5% mini	450	450	0.013	NewFixed	1	HW1478	0		=						
					51.91	50.91	4 Concrete, under roads, 0.5% mini 4 Concrete, under roads, 0.5% mini			0.013	NewFixed NewFixed											
	DETAILS of SERVICES CROSS	SING PIPES																				
Sate No No No No No No No No No No No			Bottom Elev (m)	Height of S (m)	Chg (m)	Bottom Elev (m)	Height of 9 Chg (m) (m)															
	CHANNEL DETAILS																					
	Name	From	То	Туре	Length (m)		D/S IL Slope (m) (%)	Base Widt (m)		R.B. Slope (1:?)	Manning n		Roofed					—				
	OVERELOW POLITE DETAILS								<u></u>	,				=								
Superior Point Point Point Point <		From	То		Spill			Safe Dept	SafeDepth					id '	U/S IL	D/S IL	Length (m)					
	E 040.04	E D40.04 UP	EACT D40	(min)				(m)	(m)		(%)	%		00050			400.0					
	E-B10-02	E-B10-02-US	EAST-B10	7.8			Swale with 1:6 sideslopes	0.3	0.2	1	0.49	69.04		98055	63.5	62	306.3					
	E-B10-03B	E-B10-CULV1-DS	EAST-B10	0.7			Swale with 1:6 sideslopes	0.3	0.2	1	1.69	4.95		99069	62.91	62	54					
	E-B10-04 E-B10-05	E-B10-04-US	E-B10-CU	0.9				0.3		1	2.44			98124				—				
		E-B1-01-US							0.2	1	0.51											
	E-B1-02B	E-B1-CULV1-DS	EAST-B1				Swale with 1:6 sideslopes	0.3	0.2	1	2.78			98819	59.8		28.8					
	E-B1-03B	E-B1-03-SPLIT	EAST-B1	3.9		L	Swale with 1:6 sideslopes	0.3	0.2	1	2.08	66.3		98467	65.5	59	312.1			$ \rightarrow $	_	
	E-B1-04-CONNECT	E-B1-04-DS	E-B1-03-S				Dummy OF	0.3	0.3	1	3.25	0		98876	68.5	65.5	92.4					
	E-B2-01 E-B2-02	E-B2-02-US	EAST-B2				Swale with 1:6 sideslopes	0.3	0.2	1	5.28	45.25		98482		57.5	56.8					
	E-B3-01	E-B3-01-US	EAST-B3 EAST-B3	2.8			Swale with 1:6 sideslopes Swale with 1:6 sideslopes	0.3	0.2	1	1.26	25.69 47.07		98348 98344	72 70.6	70	112.9					
	E-B4-01 E-B4-02	E-B4-01-US	Pit1296	2.2			K300, 0.4m deep, wall on one side	e 0.3	0.2	0.6	0.5	100		98369		71.8	150.2					
	E-B5-01 E-B5-02	E-B5-01-US	E-B5-CUL	1.4			Swale with 1:4 sideslopes	0.45	0.3	1	2.56	15.7		97787		66.91	159.6			_		
	E-B6-01	E-B6-01-US	EAST-B6				Swale with 1:6 sideslopes	0.3	0.2	1	3.87	19.7		98156	66.5	61	142			=		
	E-B6-03	E-B6-03-US	EAST-B6			L	Swale with 1:6 sideslopes	0.3	0.2	1	0.8	49.41		98198	63.5	61	310.6			$ \rightarrow $		
	E-B7-01 E-B7-02	E-B7-02-US	E-B7-02-D	3.6			Swale with 1:6 sideslopes	0.3	0.2	1	0.62	100		98229		69.5	160.6					
	E-B7-03 E-B7-04	E-B7-03-US E-B7-04-US	E-B7-03-D E-B7-CUL	2.1			Swale with 1:6 sideslopes Swale with 1:4 sideslopes	0.3	0.2	1	1.16	70.93		98233 97862	72	70.5	129.3					
	E-B7-05 E-B7-06	E-B7-05-US E-B7-CULV2-DS	E-B7-CUL E-B7-CUL	0.3			Swale with 1:4 sideslopes Swale with 1:4 sideslopes	0.45	0.3	1	1.92	29.07				72.41	30.7 149.8					
	E-B7-07	E-B7-07-US	E-B7-CUL	1.4			Swale with 1:4 sideslopes	0.45	0.3	1	1.57	67.5		98258	70	68	127.4					
	E-B7-09	E-B7-09-US	Pit1448	2.1			Swale with 1:6 sideslopes	0.3	0.2	1	1.45	50.2		98296	70	67.91	144.6			$ \rightarrow $		
	E-B7-10A E-B7-10B	N511	E-B7-CUL	1.7			Swale with 1:4 sideslopes	0.45		1	1.12	100		102058	67	65.5	133.8					
	E-B8-01A	E-B8-01A-US	EAST-B8	2.3			Swale with 1:4 sideslopes	0.45	0.3	1	0.56	41.89		98986	71.2	70.5	126.1					
	E-B9-01	E-B9-01-US	E-B9-CUL	1.4			Swale with 1:6 sideslopes	0.3	0.2	1	3.6	68.8		97981		64	152.7					
	E-B9-02 E-B9-03	E-B9-02-US E-B9-03-US	E-B9-CUL E-B9-CUL	1.4				0.3		1	1.57	31.2 60.9										
	E-B9-04 E-B9-05	E-B9-04-US	E-B9-CUL				Swale with 1:6 sideslopes Swale with 1:4 sideslopes		0.2	1	1.85	39.1		97956								
	E-B9-06	E-B9-06-US	E-B9-CUL				Swale with 1:4 sideslopes	0.45	0.3	1	1.37			97933	68	66.41	116.3					
	E-B9-08	E-B9-08-US	E-B9-CUL	1.6			Swale with 1:4 sideslopes	0.45		1	0.94	24.2		97909		67.41	115.5			$ \rightarrow $		
	OF144	E-B7-03-DS	E-B7-02-D	0.4			Swale with 1:6 sideslopes	0.3		1	2.83	100		98593	70.5	69.5	35.3					
Phy Phy <td>OF159</td> <td>E-B7-CULV3-DS</td> <td>N266</td> <td>0.5</td> <td></td> <td></td> <td>Swale with 1:6 sideslopes</td> <td>0.3</td> <td>0.2</td> <td>1</td> <td></td> <td>50</td> <td></td> <td>98625</td> <td>67</td> <td></td> <td>26.7</td> <td></td> <td></td> <td></td> <td></td> <td></td>	OF159	E-B7-CULV3-DS	N266	0.5			Swale with 1:6 sideslopes	0.3	0.2	1		50		98625	67		26.7					
	OF165 OF18		EAST-B7 N539						0.2	1	5 4.05				66.75 56							
Dial Dial <th< td=""><td>OF22 OF226</td><td>EAST-B2</td><td>N58</td><td>0.1</td><td>57.75</td><td>5</td><td>1.45 4 m wide pathway</td><td>0.3</td><td>0.15</td><td>0.4</td><td>17.5</td><td>0</td><td></td><td>97566</td><td></td><td>56</td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	OF22 OF226	EAST-B2	N58	0.1	57.75	5	1.45 4 m wide pathway	0.3	0.15	0.4	17.5	0		97566		56						
PRA Listend 10 Proceeding Proceeding <td>OF244</td> <td>E-B7-11-DS</td> <td>EAST-B7</td> <td>0.1</td> <td></td> <td></td> <td>Dummy OF</td> <td>0.3</td> <td>0.3</td> <td>0.6</td> <td>10</td> <td>0</td> <td></td> <td>98967</td> <td>65.1</td> <td>65</td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td>	OF244	E-B7-11-DS	EAST-B7	0.1			Dummy OF	0.3	0.3	0.6	10	0		98967	65.1	65	1					
Dial Name Name <th< td=""><td>OF266</td><td>E-B9-CULV1-DS</td><td>E-B9-CUL</td><td>0.4</td><td>70.6</td><td>45</td><td>Swale with 1:6 sideslopes</td><td>0.3</td><td>0.2</td><td>1</td><td>3.3</td><td>0</td><td></td><td>99033</td><td>66.41</td><td>64.91</td><td>45.4</td><td></td><td></td><td>_</td><td></td><td></td></th<>	OF266	E-B9-CULV1-DS	E-B9-CUL	0.4	70.6	45	Swale with 1:6 sideslopes	0.3	0.2	1	3.3	0		99033	66.41	64.91	45.4			_		
	OF309	N388	N539	0.5			Dummy OF	0.3		0.6	5.67	0		99431	55.5	51.5	70.6					
Dipo Non Non <td>OF315</td> <td>EAST-B4</td> <td>N299</td> <td>0.4</td> <td>71.5</td> <td></td> <td>1.45 4 m wide pathway</td> <td>0.3</td> <td>0.15</td> <td>0.4</td> <td></td> <td></td> <td></td> <td>99544</td> <td></td> <td>68</td> <td>80</td> <td></td> <td></td> <td></td> <td></td> <td></td>	OF315	EAST-B4	N299	0.4	71.5		1.45 4 m wide pathway	0.3	0.15	0.4				99544		68	80					
CBU. EASI 00 NO2 0 0 0.43 0.4	OF32192	N302	N38859	1.7	/1	15	Swale with 1:4 sideslopes	0.12		0.6	5			807389		64	50					
Display Display <t< td=""><td>OF32197 OF322</td><td>EAST-B5</td><td>N302</td><td>0.1</td><td>67.2</td><td>5</td><td>Swale with 1:4 sideslopes 1.45 4 m wide pathway</td><td>0.3</td><td>0.15</td><td>0.4</td><td>13.5</td><td></td><td></td><td>99574</td><td>67.2</td><td>64.5</td><td>20</td><td></td><td>-</td><td></td><td></td><td></td></t<>	OF32197 OF322	EAST-B5	N302	0.1	67.2	5	Swale with 1:4 sideslopes 1.45 4 m wide pathway	0.3	0.15	0.4	13.5			99574	67.2	64.5	20		-			
Distant Distant of the second se		N539 HW1478	HW1478 N59	0.8	49.5	15	Swale with 1:4 sideslopes		0.05	1	5.7			807624 807871		48.41	<u>54.2</u> 20					
D211 DV170 N0873 61 61 61 62 61 63 61 63 61 63 61 63 61 63								0.3														
CH2020 EB0.04.946 W1140 CH2 See with 14 desteques 0.0 0.0 0 0 0 0 <td></td> <td>HW1479</td> <td>N38873</td> <td>0.1</td> <td>53</td> <td>15</td> <td>1.45 Overflow across road low point - p</td> <td></td> <td>0</td> <td>0.6</td> <td>6.67</td> <td>0</td> <td></td> <td>808355</td> <td>53</td> <td>52</td> <td>15</td> <td></td> <td></td> <td></td> <td></td> <td></td>		HW1479	N38873	0.1	53	15	1.45 Overflow across road low point - p		0	0.6	6.67	0		808355	53	52	15					
PS222 H1140 NS880 0.1 1.55 Define accoss rande log of 1, 2 0.65 0.0 0.1 0.2 0.0 0.000 0.0	OF32220 OF32222	E-B9-CULV3-DS	HW1480				Swale with 1:4 sideslopes		0.05	1	2.87			808409		56.41	125			=		
P34 P34 <td>OF32227</td> <td>HW1480</td> <td>N38880</td> <td></td> <td>57.5</td> <td>15</td> <td>1.45 Overflow across road low point - p</td> <td></td> <td>0</td> <td>0.6</td> <td>4</td> <td></td> <td></td> <td>808567</td> <td></td> <td></td> <td>25</td> <td></td> <td></td> <td>=</td> <td></td> <td></td>	OF32227	HW1480	N38880		57.5	15	1.45 Overflow across road low point - p		0	0.6	4			808567			25			=		
Chain Control Control <thcontrol< th=""> <thcontrol< th=""> <thcon< td=""><td>OF324</td><td>EAST-B10</td><td>N294</td><td>0.6</td><td>62.5</td><td>15</td><td>1.45 Overflow across road low point - p</td><td>a 0.05</td><td>0</td><td></td><td>4</td><td>0</td><td></td><td>99602</td><td>62.5</td><td>60.5</td><td>50</td><td></td><td></td><td></td><td></td><td></td></thcon<></thcontrol<></thcontrol<>	OF324	EAST-B10	N294	0.6	62.5	15	1.45 Overflow across road low point - p	a 0.05	0		4	0		99602	62.5	60.5	50					
PSB Eds CAU-14W PASE O II S II O III PSIII PSIIII PSIIII PSIIIII PSIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	OF326 OF330	EAST-B7	EAST-86 N298	0.1	65.75	5	1.45 4 m wide pathway	0.45		0.4				99715								
P399 Edit CAUX-HW	OF336	E-B5-CULV1-HW	EAST-B5	0.1	68		1.45 4 m wide pathway	0.3		0.4				99781	68	67						
PASE UV28 E59/C4L 0.1 Image with 14 selences 0.3 0.2 1 6.22 0.91 20.8 0.92 0.98 0.22 0.98 0.92 0.98 </td <td></td> <td>Pit1448</td> <td>E-B7-CUL</td> <td>0.9</td> <td></td> <td>5</td> <td>Dummy OF</td> <td>0.05</td> <td>0</td> <td></td> <td>6.34</td> <td>0</td> <td></td> <td>99806</td> <td>69</td> <td>65.5</td> <td>55.2</td> <td></td> <td></td> <td></td> <td></td> <td></td>		Pit1448	E-B7-CUL	0.9		5	Dummy OF	0.05	0		6.34	0		99806	69	65.5	55.2					
EAS1 EAS1-28 EAS1-28 EAS1-28 EAS1-28 Control of the control of	OF343 OF345	N296	E-B9-CUL	0.1			Swale with 1:6 sideslopes	0.3	0.2	1	6.32	0		99846	62.225	60.91	20.8					
Figs EdsCLU-2HW EssCLU 0.2 0.6 0.6 0.6 7.07 0 100011 68 64 28 State Controls	OF360	EAST-B9	E-B7-07-U N296	0.1	64	5	1.45 4 m wide pathway 1.45 4 m wide pathway	0.3	0.15	0.4	12.5 11.83	0		99974	64	62.225	10 15					
F367 E38-CULV3-HW E38-CUL	OF363 OF365	E-B9-CULV2-HW E-B9-CULV1-HW	E-B9-CUL E-B9-CUL	0.2	66	15	1.45 Overflow across road low point - p	a 0.05	0	0.6	7.07	0		100011 100021	66	64	28.3					
by Set 1004 NS94 0.3 I Same with 14 defedgee 0.3 1 4.88 0 102855 3.55 51.5 4.77 Image: state	OF367	E-B9-CULV3-HW	E-B9-CUL	0.5	62	5	1.45 Overflow across road low point - p	a 0.05	0	0.6	4.08	0		100034	62	60	49			$ \rightarrow $		
Income Income<	OF526	N304	N539	0.3			Swale with 1:4 sideslopes	0.45		1	4.58			102855	53.5	51.5	43.7			=		
anne Type Da (mm) Sile Cover Cover (m) Image: C	0.00400	C-D/-GULVI-HW	r.n.(448	0.1	69	5	1.45 4 m wide pasiwaly	0.3	<u>U.15</u>	U.4	∠1.8	0		1228108	69	01.91	5			$ \rightarrow $		
anne Type Da (mm) Sile Cover Cover (m) Image: C	PIPE COVER DETAILS	T	Dia	0-4. 2	0																	
21 Concrete, under and 450 0.6 0.40 Unsde Image: Concrete, under and 1.6 Image: Concrete, under and Image: Concrete, under and 1.6 Image: Concrete, under and Image: Concrete, under and 1.6 Image: Concrete, under and 1.6 Image: Concrete, under and Image: Concrete, under and 1.6 Image: Concrete, under and 1.6 <td>Name Pipe10</td> <td>Concrete, under roads</td> <td>450</td> <td>0.6</td> <td>0.21</td> <td>Unsafe</td> <td></td>	Name Pipe10	Concrete, under roads	450	0.6	0.21	Unsafe																
13383 Concrete, under and 450 0.6 0.2 Under 304 0.6 0.4 0.6 0.4 0.6 0.4 0.6	P21 E-B5-CULV1	Concrete, under roads Concrete, under roads	450	0.6	-0.49	Unsafe																F
UMM-Solate UP/C. under mask. 1 54 0.5 0.4 0.1 0		Concrete, under roads	450		-0.49	Unsafe		\square														
88-CULV1 Concrete, under roadt 450 0.6 <	DUMMY-SCALE	uPVC, under roads, 1	154	0.5	-0.16	Unsafe											_					
begess Concrete, under rande 660 0.6 0.65 0.45 0.14 0	E-B9-CULV1	Concrete. under roads	450	0.6	0.6											\rightarrow				$ \rightarrow $		
Uncerted desite Openate desite desi	Pipe283	Concrete, under roads	600	0.6	-0.05	Unsafe		\square						=		=				=		
leg13 Concrete, under and 450 0.6 0.51 Unade Image: State of the sta	Pipe184	Concrete, under roads	450	0.6	-0.49	Unsafe								=		=						
13854 Concrete, under rande 600 0.6 0.66 Under rande 600 0.6 0.66 Under rande 0.6 0		Concrete, under roads	450	0.6	0.51	Unsafe										=						
Dentifie Ommeter, under rande 660 0.6 -0.65 Under name Image: Concrete, under rande Image: Concrete, under ran	P13854	Concrete. under roads	600	0.6	0.06	Unsafe																
Uncertain 600 0.6 0.15 Unsale 0	Pipe182 Pipe349	Concrete, under roads	600 600	0.6	-0.65	Unsafe Unsafe																\square
Uper 12 Concrete, under rander 450 0.6 </td <td>Pipe186</td> <td>Concrete, under roads</td> <td>600</td> <td>0.6</td> <td>-0.15</td> <td>Unsafe</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>\square</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>	Pipe186	Concrete, under roads	600	0.6	-0.15	Unsafe							\square									
Br-CULV1 Concrete, underroad 450 0.6 0.48 Image: Concrete, underroad 0.6 0.48 Image: Concrete, underroad 0.6 0.48 Image: Concrete, underroad 0.6 0.44 Image: Concrete, underroad 0.6 0.6 0.6 0.44 Image: Concrete, underroad 0.6 <t< td=""><td>Pipe122</td><td>Concrete, under roads</td><td>450</td><td>0.6</td><td>0.6</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>=</td><td></td><td>=</td><td></td><td></td><td></td><td>=</td><td></td><td></td></t<>	Pipe122	Concrete, under roads	450	0.6	0.6									=		=				=		
Dec2927 Concrete, underroadt 375 0.6 -0.41 Unsate Image: Concrete, underroadt -0.5 -0.6 -0.41 Image: Concrete, underroadt -0.5 -0.6 <t< td=""><td>E-B7-CULV1</td><td>Concrete, under roads</td><td>450</td><td>0.6</td><td>-0.49</td><td>Unsafe</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>\rightarrow</td><td></td><td></td></t<>	E-B7-CULV1	Concrete, under roads	450	0.6	-0.49	Unsafe														$ \rightarrow $		
Depender Concrete, underroads 450 0.68 Unsafe Image: Concrete, underroads Concrete, underroads <td>Pipe2927</td> <td>Concrete. under roads</td> <td>375</td> <td>0.6</td> <td>-0.41</td> <td>Unsafe</td> <td></td>	Pipe2927	Concrete. under roads	375	0.6	-0.41	Unsafe																
Depet77 Concrete, underroads 600 0.6 -0.64 Unste -0.64 -0.64 -0.66 <td>Pipe178</td> <td>Concrete, under roads</td> <td>600</td> <td>0.6</td> <td>0.06</td> <td>Unsafe</td> <td></td>	Pipe178	Concrete, under roads	600	0.6	0.06	Unsafe																
Upee846 Concrete, under road 900 0.6 0.12 Unsale Image: Concrete, under road Image: Concrete, under Image: Concrete, under road		Concrete, under roads																				
	Pipe177 Pipe8633																					
hese alces have non-return values, Piae10, P13826, Piae233, Piae213, P13854, Piae349, P13783	Pipe177 Pipe8633 Pipe8646	Concrete, under roads	900	0.6	0.12	Unsafe												I 1				
	Pipe177 Pipe8633	Concrete, under roads	900	0.6	0.12	Unsafe										\equiv						

Stage 1B (EAST) DRAINS Results	1	1		1				
DRAINS results prepared from Version 2020.036								
1EY PIT / NODE DETAILS				Version 8				
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving			Overflow (cu.m/s)	Constraint	
E-B2-02-US	60.5		(cu.m/s) 0	(cu.m)	<u>(m)</u>			
N57	56.3		0					
N58 E-B2-01-US	56 63.5		0					
E-B5-CULV1-HW N61643	67.48 65.3		0.22		0.52	0	Headwall height/system capacity	
N302 DUMMY-SCALE2	64.61 10		0					
DUMMY-SCALE1	8		0					
E-B5-01-US E-B5-02-US	71		0					
E-B7-CULV2-HW E-B7-CULV2-DS	72.69 72.14		0.041		0.81	0	Headwall height/system capacity	
E-B7-04-US	73		0					
E-B7-05-US E-B9-CULV1-HW	73 67.41		0		1.09	0	Headwall height/system capacity	
E-B9-CULV1-DS E-B9-07-US	66.47 73		0.014					
E-B9-08-US	68.5 71		0					
E-B9-05-US E-B9-06-US	68		0					
E-B9-CULV2-HW E-B9-CULV2-DS	65.01 64.1		0.016		0.99	0	Headwall height/system capacity	
E-B9-03-US E-B9-04-US	71		0					
E-B9-01-US	69.5		0					
E-B9-02-US N306	65.5 60.2		0					
N297 E-B7-07-US	55.5 70.01		0					
N296	62.23		0					
N305 N304	56.98 53.59		0					
N61649 N298	64.24 63.09		0					
N367 N294	61.33 60.59		0					
E-B9-CULV3-HW	60.92		0		1.08	0	Headwall height/system capacity	
E-B9-CULV3-DS E-B10-01-US	60.01 63		0					
E-B10-02-US E-B10-03-US	63.5 65.5		0					
E-B10-CULV1-HW	64.41		0.003		1.09	0	None	
E-B10-CULV1-DS E-B10-04-US	62.97 67		0.008					
E-B10-05-US E-B6-01-US	68 66.5		0					
E-B6-02-US	69.5		0					
E-B6-03-US E-B7-01-US	63.5 69.5		0					
E-B7-02-DS E-B7-03-DS	69.56 70.57		0.027					
E-B7-02-US	70.5		0					
E-B7-03-US E-B7-CULV1-HW	72 68.23		0.068		0.77	0	None	
Pit1448 E-B7-CULV1-DS	67.18 65.68	68	0.077		0.73	0	Inlet Capacity	
E-B7-08-US E-B7-09-US	72 70		0					
E-B7-10-US	69.5		0					
E-B7-11-DS E-B3-02-US	65.52 70.6		0.109					
E-B3-01-US E-B4-01-US	72		0					
E-B4-02-DS	71.18		0.075					
E-B4-02-US E-B1-01-US	73 58.5		0					
E-B1-CULV1-DS E-B1-02-US	59.83 60.5		0.006					
E-B1-03-SPLIT E-B1-03-US	65.59 68.5		0.05					
E-B1-04-DS	68.5		0					
E-B1-04-US Pit8	69.5 67.6		0.015		1.4	0	Inlet Capacity	
E-B7-CULV3-DS N266	67.09 66.83		0.049					
E-B8-01A-US	71.2		0					
E-B8-01B-US N388	73 55.5		0.008					
N511 N539	67.05 51.59		0.005					
Pit1296	71.6	71.86	0.029	0	0.2	0	Inlet Capacity	
N61629 N299	69.24 68		0					
HW1478 N59	48.6 47.42		0.044		0.9		None	
N38873	52.04 50.98		0.138		0.96	0	None	
HW1480	56.56		0.026		0.94	0	None	
N38880	55.5		0					
SUB-CATCHMENT DETAILS Name	Max	Paved	Grassed	Paved	Grassed	Supp.	Due to Storm	
	Flow Q	Max Q	Max Q	Tc	Tc	Тс		
EAST-B2-CAT	(cu.m/s) 0.062	(cu.m/s) 0	(cu.m/s) 0		(min) 11.28		1EY AEP, 10 min burst, Storm 10	
E-B5 EAST-B5-CAT	0.409		0		0 25.62	0	1EY AEP, 10 min burst, Storm 10 1EY AEP, 10 min burst, Storm 5	
E-B7-A E-B9-A	0.078	0	0	5.95	0	0	1EY AEP, 10 min burst, Storm 10 1EY AEP, 10 min burst, Storm 5	
E-B9-B	0.023	0	0	1.7	3.96	0	1EY AEP, 10 min burst, Storm 9	
E-B9-C E-B9-D	0.06	0		2.59	6.01		1EY AEP, 10 min burst, Storm 5 1EY AEP, 10 min burst, Storm 7	
EAST-B6-CAT EAST-B8-CAT	0.066	163.253	0.255	3.11	7.23	3.53	1EY AEP, 10 min burst, Storm 9 1EY AEP, 10 min burst, Storm 9	
EAST-B9-CAT	0	-9999	0	0	3.51	0	1EY AEP. 10 min burst. Storm 5	
EAST-B1-CAT EAST-B7-CAT	0.116	0.178	0	0	7.76	0	1EY AEP, 10 min burst, Storm 9 1EY AEP, 10 min burst, Storm 5	
EAST-B10-CAT E-B10-A	0.091	0	0	2.36	5.48	2.67	1EY AEP, 10 min burst, Storm 9 1EY AEP, 10 min burst, Storm 5	
E-B10-03-CATA	0.014	0	0	1.87	4.35	2.12	1EY AEP, 10 min burst, Storm 9	
E-B7-02-CAT E-B7-03-CAT	0.029	0	0	3.4	8.69 7.89	3.85	1EY AEP, 10 min burst, Storm 5 1EY AEP, 10 min burst, Storm 9	
E-B7-B-CAT E-B7-C	0.125	0	0	0	17.2	0	1EY AEP, 10 min burst, Storm 5 1EY AEP, 10 min burst, Storm 9	
E-B7-10-CATB	0	0	0	4.02	9.34	4.55	1EY AEP, 10 min burst, Storm 5	
E-B7-11-CAT E-B4-02-CAT	0.144	0	0	6.48	5.77	0	1EY AEP, 10 min burst, Storm 5 1EY AEP, 10 min burst, Storm 10	
E-B1-02-CATA E-B1-03-US-CAT	0.01	0	0	2.71		3.07	1EY AEP, 10 min burst, Storm 9 1EY AEP, 10 min burst, Storm 7	
E-B1-04-CAT	0	0	0	0	3.99	0	1EY AEP, 10 min burst, Storm 5	
E-B7-01-CAT	0.025	0	0	4	9.29	4.53	1EY AEP, 10 min burst, Storm 9	

Cat314	0	0	0	0	10.99	0	1EY AEP, 10 min burst, Storm 5	
E-B8-02 E-B1-01-CAT	0.013		0	0 2.34	23.14 5.44	0	1EY AEP, 10 min burst, Storm 5 1EY AEP, 10 min burst, Storm 9	
E-B7-10-CATA E-B4-01-CAT	0.008	0	0	4.02	9.34	4.55	1EY AEP, 10 min burst, Storm 9 1EY AEP, 10 min burst, Storm 9	
EAST-B4-CAT EAST-B3-CAT	0.011	0	0	5.57	12.94 7.81	6.31	1EY AEP, 10 min burst, Storm 10 1EY AEP, 10 min burst, Storm 9	
	0.125			0.00	1.01	0.0		
PIPE DETAILS Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm			
	(cu.m/s)		HGL (m)	HGL (m)				
Pipe10 P21	0.006	1.09	56.303 56.295	56.033	1EY AEP, 10 min burst, Storm 5 1EY AEP, 9 hour burst, Storm 6			
E-B5-CULV1 P13826	0.24		67.395 65.3	65.3	1EY AEP, 15 min burst, Storm 1 1EY AEP, 10 min burst, Storm 5			
Pipe179 DUMMY-SCALE	0.021		65.3 10	8	1EY AEP, 3 hour burst, Storm 9 1EY AEP, 10 min burst, Storm 5			
E-B7-CULV2 E-B9-CULV1	0.067	1.66 0	72.617 67.41	72.136 66.471	1EY AEP, 10 min burst, Storm 7 1EY AEP, 10 min burst, Storm 5			
E-B9-CULV2 Pipe283	0.007	0.29	65.006 60.4		1EY AEP, 1 hour burst, Storm 1 1EY AEP, 10 min burst, Storm 5			
Pipe183 Pipe184	0.018	3.15	60.202 70.053	55.531 70.009	1EY AEP, 6 hour burst, Storm 7 1EY AEP, 10 min burst, Storm 5			
Pipe185 Pipe213	0.021	0	62.303 57.098	62.225	1EY AEP, 10 min burst, Storm 5 1EY AEP, 6 hour burst, Storm 1			
Pipe220 P13854	0.032	2.18	56.981 64.376	53.593	1EY AEP, 6 hour burst, Storm 1 1EY AEP, 6 hour burst, Storm 7			
Pipe182 Pipe349	0.04	2.3	64.237 61.741	63.094	1EY AEP, 6 hour burst, Storm 7			
Pipe186	0.02	1.15	61.335	60.591	1EY AEP, 10 min burst, Storm 5 1EY AEP, 2 hour burst, Storm 8 1EY AEP, 10 min burst, Storm 5			
E-B9-CULV3 Pipe122 Poter	0	0	64.41	62.973	1EY AEP, 10 min burst, Storm 5			
P3176 E-B7-CULV1	0.046		68.223 67.148	65.693	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1			
E-B7-CULV3 Pipe2927	0.024	0.93	67.598 71.596	71.279	1EY AEP, 10 min burst, Storm 4 1EY AEP, 10 min burst, Storm 4			
Pipe178 P13783	0		70.4 69.3	69.236	1EY AEP, 10 min burst, Storm 5 1EY AEP, 10 min burst, Storm 5			
Pipe177 Pipe8633	0.031	0 2.32	69.236 48.601	68 47.473	1EY AEP, 2 hour burst, Storm 10 1EY AEP, 6 hour burst, Storm 1			
Pipe8646 Pipe8668	0.016	0.66	52.036 56.562	50.983	1EY AEP, 6 hour burst, Storm 9 1EY AEP, 2 hour burst, Storm 8			
CHANNEL DETAILS				,				
Name	Max Q (cu.m/s)	Max V (m/s)			Due to Storm			
	(ou.111/S)	111/5)						
		Max Q D/S			Max DxV	Max Width		Due to Storm
Basin 1 EAST-B10-O	0.006	0	12.141 12.141	3	0	32	0	1EY AEP, 9 hour burst, Storm 6 1EY AEP, 2 hour burst, Storm 8
EAST-B1-O EAST-B6-0	0.011	0	12.141 12.141	3	0		0	1EY AEP, 6 hour burst, Storm 1 1EY AEP, 6 hour burst, Storm 7
E-B10-01 E-B10-02	0	0.005	0.127	0.135	0.01		0.24	1EY AEP, 1 hour burst, Storm 1 1EY AEP, 30 min burst, Storm 8
E-B10-03A E-B10-03B	0.01		0.3	0.062	0.03	0.74	0.55	1EY AEP, 10 min burst, Storm 7 1EY AEP, 30 min burst, Storm 6
E-B10-04 E-B10-05	0	0	0.267	0	0	0	0	
E-B1-01 E-B1-02A	0	0.01	0.122	0.065	0.03		0.56	1EY AEP, 15 min burst, Storm 1 1EY AEP, 1 hour burst, Storm 1
E-B1-02B	0.002	0.005	0.285	0.045	0.02	0.54	1.28	1EY AEP, 10 min burst, Storm 7 1EY AEP, 15 min burst, Storm 1
E-B1-03A E-B1-03B	0.03	0.047	0.247	0.149	0.1	1.3	0.71	1EY AEP, 2 hour burst, Storm 4
E-B1-04 E-B1-04-CONNECT	0	0	0.244	0	0	0	0	
E-B2-01 E-B2-02	0	0.027	0.683	0.089	0.08		0.84	1EY AEP, 10 min burst, Storm 7 1EY AEP, 10 min burst, Storm 4
E-B3-01 E-B3-02	0		0.192	0.092	0.05	1.1 3.18	0.62	1EY AEP, 15 min burst, Storm 1 1EY AEP, 10 min burst, Storm 7
E-B4-01 E-B4-02	0		0.059	0.161	0.13	0.29	0.8	1EY AEP, 10 min burst, Storm 10 1EY AEP, 10 min burst, Storm 7
E-B5-01 E-B5-02	0	0.057	0.531	0.574	0.08	4.59 4.59	0.66	1EY AEP, 10 min burst, Storm 7 1EY AEP, 10 min burst, Storm 7
E-B6-01 E-B6-02	0	0.007	0.336	0.19	0.01	2.28	0.17	1EY AEP, 30 min burst, Storm 5 1EY AEP, 15 min burst, Storm 1
E-B6-03 E-B7-01	0	0.011	0.153	0.19	0.02	2.28	0.17	1EY AEP, 1 hour burst, Storm 1 1EY AEP, 10 min burst, Storm 1
E-B7-02	0	0	0.134	0.092	0	0	0	
E-B7-03 E-B7-04	0	0.052	0.184	0.285	0.05	2.28	0.38	1EY AEP, 15 min burst, Storm 1 1EY AEP, 10 min burst, Storm 4
E-B7-05 E-B7-06	0.066	0.065	0.46	0.287	0.04		0.9	1EY AEP, 10 min burst, Storm 10 1EY AEP, 10 min burst, Storm 7
E-B7-07 E-B7-08	0	0.054	0.416	0.113	0.06	1.35		1EY AEP, 10 min burst, Storm 7
E-B7-09 E-B7-10A	0	0.004	0.206	0.128	0.04	0.59	0.24	1EY AEP, 10 min burst, Storm 7 1EY AEP, 30 min burst, Storm 8
E-B7-10B E-B7-11	0.003	0.002	0.351	0.185	0.01		0.67	1EY AEP, 1 hour burst, Storm 1 1EY AEP, 3 hour burst, Storm 9
E-B7-O1 E-B8-01A	0.009	0	12.141 0.248	3 0.108	0.04	32	0	1EY AEP, 6 hour burst, Storm 7 1EY AEP, 10 min burst, Storm 7
E-B8-01B E-B9-01	0	0.011	0.479	0.083	0.04	0.67	0.47	1EY AEP, 10 min burst, Storm 7 1EY AEP, 15 min burst, Storm 1
E-B9-02 E-B9-03	0	0.015	0.324 0.214 0.326	0.033	0.03	0.93		1EY AEP, 15 min burst, Storm 1
E-B9-04 E-B9-05	0	0	0.232	0.08	0.04	0	0	1EY AEP, 10 min burst, Storm 7
E-B9-06 E-B9-07	0	0.007	0.389	0.069	0.04	0.55	0.49	1EY AEP, 15 min burst, Storm 1
E-B9-08	0	0	0.322	0	0	0	0	
low25 low0.5	0.009	0	12.141	3	0	32	0	1EY AEP, 3 hour burst, Storm 9 1EY AEP, 3 hour burst, Storm 9
022992 023058	0.007	0	12.141 12.141	3	0	32	0	1EY AEP, 2 hour burst, Storm 8 1EY AEP, 2 hour burst, Storm 8
O29065 O29069	0.008	0	12.141 12.141	3	0	32	0	1EY AEP, 6 hour burst, Storm 7 1EY AEP, 6 hour burst, Storm 7
031534 031545	0			0	0		0	
031559 072267	0.006			0		0	0	
072283 09296	0.006	0		3	0	32	0	1EY AEP, 6 hour burst, Storm 7 1EY AEP, 6 hour burst, Storm 7 1EY AEP, 3 hour burst, Storm 9
OF139	0	0.021	0	0	0	0	0	
OF144 OF153	0.02	0.018	0.287	0.081	0.05	0.96	0.82	1EY AEP, 15 min burst, Storm 1 1EY AEP, 15 min burst, Storm 1
OF159 OF165	0.021	0.022	0.166	0.094	0.05	6.35	0.82	1EY AEP, 10 min burst, Storm 7 1EY AEP, 25 min burst, Storm 5
OF18 OF22	0.006	0	19.227 1.333	0.081 0	0	0	0	1EY AEP, 9 hour burst, Storm 6
OF226 OF244	0.227	0.227 0.315	19.201 19.201	0.18	0.01	32		1EY AEP, 30 min burst, Storm 6 1EY AEP, 3 hour burst, Storm 6
	0.010	0	10.302	0	0	0	0	1EY AEP, 30 min burst, Storm 8
OF262		0.013	0.31	0.096	0.03	1 1.15		
OF262 OF266 OF293	0.013	0	0.31 19.196 19.13	0	0.03	0	0	
OF262 OF266	0.013	0 0.007 0			0	0 32 0	0 0.11 0	1EY AEP, 30 min burst, Storm 6

	0.001	0.001	0.000	0.4.17	0.05	0.94	0.17	4FX AFD 0 hours hourst Otom 0
OF32192	0.021	0.021	0.003	0.117	0.05			1EY AEP, 3 hour burst, Storm 9
OF32197 OF322	0			0				
OF322 OF32200	0.031	0.031	0.007	0,191	0.09			1EY AEP, 6 hour burst, Storm 1
OF32200 OF32206	0.031	0.031						
OF32206 OF32209	0.031	0.031	17.383	0.007	0			1EY AEP. 6 hour burst. Storm 1
OF32209 OF32213		0.031			0			1EY AEP, 6 hour burst, Storm 1 1EY AEP, 6 hour burst, Storm 7
OF32213 OF32216	0.018	0.018		0.128				
		0.016						1EY AEP, 6 hour burst, Storm 9
OF32218 OF32220	0.016			0.073	0.06			
OF32220 OF32222	0.02							1EY AEP, 2 hour burst, Storm 8
DF32222 DF32227								
DF32227 DF32229	0.02	0.02			0.05			1EY AEP, 2 hour burst, Storm 8
DF32229 DF324	0.02							
DF324 DF326	0.037					1.52		1EY AEP, 6 hour burst, Storm 7
DF326 DF330								
DF330 DF334	0							
	0			0				
DF336	0			0				
DF339 DF341	0							
	0.045	0.045			0.18			1EY AEP. 1 hour burst. Storm 5
OF343								
DF345	0			0				
DF351	0							
OF360	0			0				
DF363								
DF365	0							
DF367	0							
OF369	0							
OF526	0.031	0.031	0.711		0.08			1EY AEP, 6 hour burst, Storm 1
OF53403	0	0	1.291	0	0	0	0	
DETENTION DAOIN DETAILO								
DETENTION BASIN DETAILS								
		Marsh (al						
name	Max WL	MaxVol	Max Q	Max Q	Max Q			
			Total	Low Level	High Level			
EAST-B2	57.22	0	Total 0.006	Low Level 0	High Level 0.006			
EAST-B2 EAST-B5	57.22 66.82	0	Total 0.006 0.021	Low Level 0 0	High Level 0.006 0.021			
EAST-B2 EAST-B6 EAST-B6	57.22 66.82 61.19	0 0 0	Total 0.006 0.021 0.018	Low Level 0 0 0	High Level 0.006 0.021 0.018			
EAST-B2 EAST-B5 EAST-B6 EAST-B8	57.22 66.82 61.19 70.58	0 0 0 0	Total 0.006 0.021 0.018 0	Low Level 0 0 0 0	High Level 0.006 0.021 0.018 0.018			
EAST-B2 EAST-B5 EAST-B6 EAST-B8 EAST-B8 EAST-B9 EAST-B9	57.22 66.82 61.19 70.58 63.02	0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0	Low Level 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0			
AST-B2 AST-B5 AST-B6 AST-B6 AST-B8 AST-B9 AST-B9 AST-B1	57.22 66.82 61.19 70.58 63.02 58.78	0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0 0.031	Low Level 0 0 0 0 0 0 0 0 0.021	High Level 0.006 0.021 0.018 0 0 0 0 0 0.011			
EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B9 EAST-B9 EAST-B1 EAST-B1 EAST-B7 EAS	57.22 66.82 61.19 70.58 63.02 58.78 65.53	0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0 0.031 0.039	Low Level 0 0 0 0 0 0 0 0 0.021 0.014	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0.011 0.025			
EAST-B2 EAST-B6 EAST-B6 EAST-B8 EAST-B8 EAST-B9 EAST-B9 EAST-B1 EAST-B7 EAST-B7 EAST-B7	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0 0.031 0.039 0.02	Low Level 0 0 0 0 0 0 0 0 0.021 0.014 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0.011 0.025 0.011 0.025 0.02			
EAST-B2 EAST-B5 EAST-B6 EAST-B8 EAST-B8 EAST-B9 EAST-B1 EAST-B1 EAST-B7 EAST-B10 Bio-retention	57.22 66.82 61.19 70.58 63.02 58.78 65.53 65.53 62.14 73.1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0.02 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 1 0 0 1 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0.011 0.025 0.025 0.02 0.02 0.02 0.02 0.02			
EAST-B2 EAST-B5 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B1 EAST-B1 EAST-B1 Bio-retention EAST-B4 EAST-B5 EAST-B	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0 0.031 0.039 0.02 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0.011 0.025 0.025 0.025 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
EAST-B2 EAST-B5 EAST-B6 EAST-B8 EAST-B8 EAST-B9 EAST-B1 EAST-B1 EAST-B1 EAST-B10 Bio-retention EAST-B4	57.22 66.82 61.19 70.58 63.02 58.78 65.53 65.53 62.14 73.1	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0 0.031 0.039 0.02 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0.011 0.025 0.025 0.025 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
EAST-B2 EAST-B5 EAST-B6 EAST-B8 EAST-B8 EAST-B9 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B1 Bio-retention EAST-B4 EAST-B3	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.039 0.029 0.021 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0.011 0.025 0.025 0.025 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B1 Bio-retention EAST-B10 Bio-retention EAST-B4 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark east run at 02	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.039 0.029 0.021 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0.011 0.025 0.025 0.025 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B1 EAST-B1 EAST-B1 EAST-B7 EAST-B1 EAST-B4 EAST-B4 EAST-B3 Sun Log for 12546218 AlbanyMotorPark east run at 02 vo water upwelling from any pit. Freeboard was adeque	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B1 EAST-B1 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B3 EAST-B3 Run Log for 12546218 AlbanyMotorPark east run at 02 to water upwelling from any pit. Freeboard was adequa	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B1 EAST-B1 EAST-B1 EAST-B7 EAST-B1 EAST-B4 EAST-B4 EAST-B3 Sun Log for 12546218 AlbanyMotorPark east run at 02 vo water upwelling from any pit. Freeboard was adeque	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
EAST-B2 EAST-B5 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B4 EAST-B3 Run Log for 12546218. AlbanyMotorPark east run at 02 No water upwelling from any pit. Freeboard was adequa	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
EAST-B2 EAST-B5 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B4 EAST-B3 Run Log for 12546218. AlbanyMotorPark east run at 02 No water upwelling from any pit. Freeboard was adequa	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
EAST-B2 EAST-B5 EAST-B5 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark east run at 02 No water upwelling from any pit. Freeboard was adequa	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
EAST-B2 EAST-B5 EAST-B5 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark east run at 02 No water upwelling from any pit. Freeboard was adequa	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
EAST-B2 EAST-B5 EAST-B5 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark east run at 02 No water upwelling from any pit. Freeboard was adequa	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
EAST-B2 EAST-B5 EAST-B5 EAST-B6 EAST-B8 EAST-B9 EAST-B1 EAST-B7 EAST-B7 EAST-B7 EAST-B7 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark east run at 02 No water upwelling from any pit. Freeboard was adequa	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B
Name EAST-82 EAST-85 EAST-86 EAST-88 EAST-88 EAST-88 EAST-81 EAST-81 EAST-81 EAST-81 EAST-81 Run Log for 12546218 AlbanyMotorPark east run at 02 The maximum flow in these overflow routes is unsafe. O	57.22 66.82 61.19 70.58 63.02 58.78 65.53 62.14 73.1 71.18 70.27 2:44:15 on 13	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.006 0.021 0.018 0 0 0.031 0.039 0.02 0 0 0 0 0 0 0 0 0 0 0 0 0	Low Level 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	High Level 0.006 0.021 0.018 0 0 0 0 0 0 0.011 0.025 0.025 0.025 0.02 0 0 0 0 0 0		341, OF334, OF324, OF320, OF311,	OF244, OF165, OF139, E-B3-02, E-B

Stage 1B (EAST) DRAINS Results								
DRAINS results prepared from Version 2020.036 10% AEP								
PIT / NODE DETAILS	Max HGL	Max Pond	Max Surface	Version 8 Max Pond	Min	Overflow	Constraint	
		HGL	Flow Arriving (cu.m/s)	Volume		(cu.m/s)		
E-B2-02-US N57	60.5 56.37		0					
N58 E-B2-01-US	56.01 63.5		0					
E-B5-CULV1-HW N61643	67.9		0.48		0.1	0	None	
N302	64.74		0					
DUMMY-SCALE2 DUMMY-SCALE1	10		0					
E-B5-01-US E-B5-02-US	71 72.5		0					
E-B7-CULV2-HW E-B7-CULV2-DS	72.8		0.091		0.7	0	None	
E-B7-04-US E-B7-05-US	73 73		0					
E-B9-CULV1-HW E-B9-CULV1-DS	67.73 66.54		0.099		0.77	0	None	
E-B9-07-US E-B9-08-US	73 68.5		0					
E-B9-05-US	71		0					
E-B9-06-US E-B9-CULV2-HW	68 65.27		0.204		0.73	0	None	
E-B9-CULV2-DS E-B9-03-US	64.15 71		0.122					
E-B9-04-US E-B9-01-US	67 69.5		0					
E-B9-02-US N306	65.5 60.37		0					
N297 E-B7-07-US	55.52 70.01		0.039					
N296 N305	62.23		0					
N303 N304 N61649	53.7 64.34		0					
N298	63.2 61.47		0					
N367 N294	60.71		0					
E-B9-CULV3-HW E-B9-CULV3-DS	60.92 60.01		0		1.08	0	None	
E-B10-01-US E-B10-02-US	63 63.5		0					
E-B10-03-US E-B10-CULV1-HW	65.5 64.59		0.038		0.91	0	None	
E-B10-CULV1-DS E-B10-04-US	63.02 67		0.03					
E-B10-05-US E-B6-01-US	68 66.5		0					
E-B6-02-US E-B6-03-US	69.5 63.5		0					
E-B7-01-US	69.5		0					
E-B7-02-DS E-B7-03-DS	69.6 70.61		0.071					
E-B7-02-US E-B7-03-US	70.5 72		0					
E-B7-CULV1-HW Pit1448	68.36 67.36	68.06	0.149	0.1	0.64	0	None Inlet Capacity	
E-B7-CULV1-DS E-B7-08-US	65.79 72		0.073					
E-B7-09-US E-B7-10-US	70 69.5		0					
E-B7-11-DS E-B3-02-US	65.66 70.6		0.319					
 E-B3-01-US E-B4-01-US	72		0					
E-B4-02-DS	71.34		0.168					
E-B4-02-US E-B1-01-US	73 58.5		0					
E-B1-CULV1-DS E-B1-02-US	59.91 60.5		0.054					
E-B1-03-SPLIT E-B1-03-US	65.64 68.5		0.115					
E-B1-04-DS E-B1-04-US	68.51 69.5		0.038					
Pit8 E-B7-CULV3-DS	67.73 67.16	69.08	0.063		1.27	0	Inlet Capacity	
N266 E-B8-01A-US	66.9 71.2		0.22					
E-B8-01B-US N388	73		0.026					
N500 N511 N539	67.15		0.026					
Pit1296	71.69	71.88	0.055		0.11	0	Inlet Capacity	
N61629 N299	69.31 68.1		0				•	
HW1478 N59	48.93 47.43		0.286		0.57		None	
HW1479 N38873	52.4 51.12		0.637		0.6		None	
HW1480 N38880	56.87 55.61		0.343		0.63	0	None	
SUB-CATCHMENT DETAILS								
Name	Max Flow Q		Grassed Max Q	Paved Tc	Grassed Tc	Supp. Tc	Due to Storm	
EAST-B2-CAT	(cu.m/s) 0.264	(cu.m/s) 0.031	(cu.m/s) 0.021	(min) 3.83		(min)	10% AEP, 10 min burst, Storm 3	
E-B5	0.204 0.807 0.045	216.25	52.036		0 0 41.19	0	10% AEP, 10 min burst, Storm 1 10% AEP, 10 min burst, Storm 1 10% AEP, 3 hour burst, Storm 2	
EAST-B5-CAT E-B7-A	0.157	50.983	0	4.69	0	0	10% AEP, 10 min burst, Storm 4	
E-B9-A E-B9-B	0.099	0 56.562	0	1.34	3.12	0	10% AEP, 2 hour burst, Storm 2 10% AEP, 10 min burst, Storm 3	
E-B9-C E-B9-D	0.067	0	0	2.04	5.16	2.31	10% AEP, 15 min burst, Storm 7 10% AEP, 10 min burst, Storm 8	
EAST-B6-CAT EAST-B8-CAT	0.493	0	61.741 0	2.46 1.25	5.71	2.78	10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 9	
EAST-B9-CAT EAST-B1-CAT	0.013	0.037	0	0	2.77 6.12	0	10% AEP, 10 min burst, Storm 6 10% AEP, 10 min burst, Storm 7	
 EAST-BT-CAT EAST-B10-CAT	0.273	0	0	0		0	10% AEP, 2 hour burst, Storm 2 10% AEP, 10 min burst, Storm 3	
E-B10-A	0.052	0	0	1.33	3.08	1.5	10% AEP, 10 min burst, Storm 8	
E-B10-03-CATA E-B7-02-CAT	0.045	0 57.217	0 118.72	0	3.43 7.5	0	10% AEP, 10 min burst, Storm 9 10% AEP, 15 min burst, Storm 4	
E-B7-03-CAT E-B7-B-CAT	0.068	0		0		0	10% AEP, 10 min burst, Storm 7 10% AEP, 2 hour burst, Storm 2	
E-B7-C E-B7-10-CATB	0.27	8 0	0	3.47	6.56 8.06	3.2	10% AEP, 10 min burst, Storm 4 10% AEP, 15 min burst, Storm 1	
E-B7-11-CAT E-B4-02-CAT	0.016	0	67.598 0	0 5.11	4.98	0	10% AEP, 15 min burst, Storm 1 10% AEP, 10 min burst, Storm 4	
E-B1-02-CATA E-B1-03-US-CAT	0.082	0	0	2.14	4.97 6.89	2.42	10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 9	
E-B1-04-CAT E-B7-01-CAT	0.046	0	0	0	3.15	0	10% AEP, 10 min burst, Storm 7 10% AEP, 10 min burst, Storm 3	
	0.100	0.000	0	3.13	1.33	3.37		

	Cat314 E-B8-02	0.014	64.335 0	0.139	0	15.98 37.2	0	10% AEP, 2 hour burst, Storm 2 10% AEP, 3 hour burst, Storm 8	
	E-B1-01-CAT E-B7-10-CATA	0.038	65.004 0	0.099	1.85 3.47	4.29	2.09	10% AEP, 10 min burst, Storm 9 10% AEP, 15 min burst, Storm 7	
	E-B4-01-CAT EAST-B4-CAT	0.092	56 0.076	0	1.85 4.39	0 10.2	0 4.97	10% AEP, 10 min burst, Storm 1 10% AEP, 10 min burst, Storm 5	
	EAST-B3-CAT	0.307	0.409	73	2.65	6.16	3	10% AEP, 10 min burst, Storm 7	
	PIPE DETAILS Name	Max Q	Max V	Max U/S	Max D/S	Due to Storm			
	Pipe10	(cu.m/s) 0.043		HGL (m) 56.928	HGL (m)	10% AEP, 3 hour burst, Storm 4			
	P21 E-B5-CULV1	0.055	2.24	56.369 67.696	56.095	10% AEP, 3 hour burst, Storm 4 10% AEP, 15 min burst, Storm 7			
	P13826 Pipe179	0.138 0.174	2.5 3.1	66.175 65.412	65.411	10% AEP, 2 hour burst, Storm 5 10% AEP, 2 hour burst, Storm 5			
	DUMMY-SCALE E-B7-CULV2	0.121	0 2.19	10 72.652	8 72.17	10% AEP, 10 min burst, Storm 5 10% AEP, 10 min burst, Storm 7			
	E-B9-CULV1 E-B9-CULV2	0.089	2.39 2.13	67.617 65.135	64.156	10% AEP, 2 hour burst, Storm 2 10% AEP, 2 hour burst, Storm 2			
	Pipe283 Pipe183	0.377	4.15 5.99	60.884 60.369	55.673	10% AEP, 2 hour burst, Storm 8 10% AEP, 2 hour burst, Storm 8			
	Pipe184 Pipe185 Pipe185	0		62.303	62.225	10% AEP, 10 min burst, Storm 5 10% AEP, 10 min burst, Storm 5			
	Pipe213 Pipe220 P13854	0.184 0.196 0.258	3.48 3.66 3.8	57.978 57.082 64.999	53.705	10% AEP, 2 hour burst, Storm 2 10% AEP, 2 hour burst, Storm 2 10% AEP, 2 hour burst, Storm 3			
	Pipe182 Pipe349	0.287	4.22	64.344 61.914	63.204	10% AEP, 2 hour burst, Storm 3 10% AEP, 2 hour burst, Storm 3			
	Pipe186 E-B9-CULV3	0.189	2.27	61.47 60.916	60.712	10% AEP, 2 hour burst, Storm 8 10% AEP, 10 min burst, Storm 5			
	Pipe122 P3176	0.026	0.81	64.585 68.363	63.025	10% AEP, 30 min burst, Storm 5 10% AEP, 15 min burst, Storm 2			
	E-B7-CULV1 E-B7-CULV3	0.282	2.4 1.29	67.282 67.718	65.812 67.217	10% AEP, 15 min burst, Storm 6 10% AEP, 15 min burst, Storm 8			
	Pipe2927 Pipe178 Pipe178	0.087	1.08	71.657	70.616	10% AEP, 10 min burst, Storm 5 10% AEP, 25 min burst, Storm 10			
	P13783 Pipe177 Dise8623	0.031	0	69.923 69.309	68.1	10% AEP, 10 min burst, Storm 5 10% AEP, 1 hour burst, Storm 4			
	Pipe8633 Pipe8646 Pipe8668	0.194 0.29 0.158	3.47 2.5 2.33	48.718 52.266 56.687	51.124	10% AEP, 2 hour burst, Storm 8 10% AEP, 2 hour burst, Storm 8 10% AEP, 2 hour burst, Storm 3			
	CHANNEL DETAILS	0.158	2.33	00.087	55.609	TO A ALF, 2 HOUL DUIST, STORM 3			
	Name	Max Q (cu.m/s)	Max V (m/s)			Due to Storm			
	OVERFLOW ROUTE DETAILS								
	Name Basin 1	0.011		12.141	3	0	Max Width 32	0	Due to Storm 10% AEP, 3 hour burst, Storm 4
	EAST-B10-O EAST-B1-O	0.015	0	12.141	3	0	32	0	10% AEP, 2 hour burst, Storm 8 10% AEP, 2 hour burst, Storm 2
	EAST-B6-0 E-B10-01	0.009	0.042	12.141	3 0.358	0.03	32 4.3	0.18	10% AEP, 2 hour burst, Storm 8 10% AEP, 15 min burst, Storm 5
	E-B10-02 E-B10-03A	0	0.041	0.12	0.358	0.1	4.3	0.57	10% AEP, 15 min burst, Storm 6 10% AEP, 10 min burst, Storm 3
	E-B10-03B E-B10-04 E-B10-05	0.05	0.017	0.222 0.267 0.592	0.358 0.175 0.175	0.07 0.02 0.05	4.3 2.1 1.4	0.31	10% AEP, 15 min burst, Storm 6 10% AEP, 15 min burst, Storm 6 10% AEP, 10 min burst, Storm 3
	E-B10-03 E-B1-01 E-B1-02A	0	0.037	0.122	0.106	0.03	1.4	0.79	10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 3 10% AEP, 15 min burst, Storm 10
	E-B1-02B E-B1-03A	0.052	0.057	0.285	0.11 0.201	0.09	1.32	0.79	10% AEP, 15 min burst, Storm 5 10% AEP, 10 min burst, Storm 3
	E-B1-03B E-B1-04	0.096	0.17	0.246	0.174 0.14	0.16	2.09 1.12		10% AEP, 1 hour burst, Storm 1 10% AEP, 2 hour burst, Storm 3
	E-B1-04-CONNECT E-B2-01	0.022		19.197 0.683	0.128	0	32 1.27	1.25	10% AEP, 2 hour burst, Storm 3 10% AEP, 15 min burst, Storm 7
	E-B2-02 E-B3-01	0	0.067	0.392	0.128	0.15	1.53 1.64	0.77	10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 3
	E-B3-02 E-B4-01	0	0.09	0.124	0.561	0.04	6.74 0.29	0.92	10% AEP, 10 min burst, Storm 9 10% AEP, 10 min burst, Storm 4
	E-B4-02 E-B5-01	0	0.113	0.315	0.286	0.26	2.29	0.74	10% AEP, 10 min burst, Storm 7 10% AEP, 10 min burst, Storm 5
	E-B5-02 E-B6-01 E-B6-02	0	0.094	0.405 0.336 0.764	0.991 0.399 0.399	0.31 0.08 0.09	7.92 4.78 3.19	0.66	10% AEP, 10 min burst, Storm 9 10% AEP, 15 min burst, Storm 7 10% AEP, 15 min burst, Storm 8
	E-B6-03 E-B7-01	0	0.158	0.153 0.272	0.399 0.208	0.05	4.78	0.5	10% AEP, 20 min burst, Storm 5 10% AEP, 15 min burst, Storm 7
	E-B7-02 E-B7-03	0	0.025	0.134	0.108	0.05	1.29	0.5	10% AEP, 2 hour burst, Storm 3 10% AEP, 10 min burst, Storm 3
	E-B7-04 E-B7-05	0	0.101	0.327	0.385	0.08	3.08 3.08	0.41	10% AEP, 10 min burst, Storm 1 10% AEP, 10 min burst, Storm 1
	E-B7-06 E-B7-07	0.121	0.13	0.542	0.365	0.18	2.92 3.16	0.41	10% AEP, 10 min burst, Storm 5 10% AEP, 2 hour burst, Storm 2
	E-B7-08 E-B7-09	0		0.279	0.146	0.1	1.75 1.96	0.43	10% AEP, 10 min burst, Storm 5 10% AEP, 10 min burst, Storm 7
	E-B7-10A E-B7-10B	0.051	0.05	0.24	0.146	0.06	1.75	0.61	10% AEP, 15 min burst, Storm 5 10% AEP, 15 min burst, Storm 4
	E-B7-01 E-B9-01	0.233		0.033	0.473	0.2	3.78	0	10% AEP, 25 min burst, Storm 8 10% AEP, 2 hour burst, Storm 3 10% AEP, 10 min burst, Storm 3
	E-B8-01A E-B8-01B E-B9-01	0	0.032	0.248 0.479 0.324	0.269 0.269 0.147	0.03 0.04 0.15	2.15 2.15 1.76	0.4	10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 3
	E-B9-02 E-B9-03	0	0.059	0.324 0.214 0.326	0.147 0.141 0.388	0.15 0.07 0.04	1.69	0.5	10% AEP, 10 min burst, Storm 3 10% AEP, 10 min burst, Storm 3 10% AEP, 2 hour burst, Storm 3
	E-B9-04 E-B9-05	0	0.019	0.232	0.388	0.04	4.66	0.28	10% AEP, 2 hour burst, Storm 3 10% AEP, 10 min burst, Storm 3
	E-B9-06 E-B9-07	0	0.023	0.389	0.105	0.06	0.84	0.58	10% AEP, 10 min burst, Storm 3 10% AEP, 2 hour burst, Storm 2
	E-B9-08 low25	0.011	0.024	0.322	0.322	0.03	2.58 32	0.31	10% AEP, 2 hour burst, Storm 2 10% AEP, 2 hour burst, Storm 5
	low0.5 022992	0.011	0		3	0		0	10% AEP, 2 hour burst, Storm 5 10% AEP, 2 hour burst, Storm 8
	023058 029065	0.015	0	12.141	3	0	32	0	10% AEP, 2 hour burst, Storm 8 10% AEP, 2 hour burst, Storm 3
	029069 031534 031545	0.01 0.01 0.01	0	12.141	3	0	32	0	10% AEP, 2 hour burst, Storm 3 10% AEP, 1 hour burst, Storm 4 10% AEP, 1 hour burst, Storm 4
	031545 031559 072267	0.01	0	12.141	3	0		0	10% AEP, 1 hour burst, Storm 4 10% AEP, 1 hour burst, Storm 4 10% AEP, 2 hour burst, Storm 8
	072287 072283 09296	0.009 0.013	0	12.141	3	0		0	10% AEP, 2 hour burst, Storm 8 10% AEP, 2 hour burst, Storm 8 10% AEP, 2 hour burst, Storm 5
	O5256 OF139 OF144	0.013	0.082	0.287	0.129	0.11	0	0	10% AEP, 15 min burst, Storm 6
	OF153 OF159	0.061	0.064	0.419	0.123	0.11	1.78	1.12	10% AEP, 10 min burst, Storm 3 10% AEP, 15 min burst, Storm 5
	OF165 OF18	0.161	0.173	0.382	0.656	0.18	7.88	1.23	10% AEP, 15 min burst, Storm 6 10% AEP, 3 hour burst, Storm 4
	OF22 OF226	0.729	0.729	1.333 19.201	0.342	0.02	0	0.09	10% AEP, 10 min burst, Storm 7
	OF262	0.794	0.794	19.201 10.302	0.656	0.02	32	0	10% AEP, 2 hour burst, Storm 3
	OF266 OF293	0.094	0	0.31	0.357	0.12	4.28	0	10% AEP, 2 hour burst, Storm 2
1	OF309	0.031	0.029	19.13	0.067	0	32		10% AEP, 15 min burst, Storm 6
	OF311 OF315	0	0	0	0	0	0		

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OF32192	0.174	0.174	0.003	0.241	0.18	1.93	
OF32197	0.03	0.03	0.005	0.517	0.07	4.14	
OF322	0		1.333	0	0	0	
OF32200	0.174	0.174	0.007	0.518	0.26	4.14	
OF32206	0	0	0	0	0	0	
OF32209	0.193	0.193	17.383	0.02	0.01	32	
OF32213	0.404	0.404	19.179	0.488	0.01	32	0.69 10% AEP, 2 hour burst, Store
OF32216	0	0	0	0	0	0	0
OF32218	0.29	0.29	0.006	0.217	0.34	1.73	1.58 10% AEP, 2 hour burst, Storn
OF32220	0	0	0.005	0	0	0	0
OF32222	0.182	0.181	0.004	0.458	0.21	3.67	1.01 10% AEP, 2 hour burst, Store
OF32227	0	0	0	0	0	0	0
OF32229	0.158	0.158	0.004	0.199	0.2	1.59	1 10% AEP, 2 hour burst, Store
OF324	0	0	0	0	0	0	
OF326	0.282	0.282	0.793	0.402	0.35	3.22	1.7 10% AEP, 2 hour burst, Storr
OF330	0		1.345	0	0	0	
OF334	0	0	0		0	0	
OF336	0		1.393	0		0	
OF339	0	0	1.337	0	0	0	
OF341	0		0		0	0	
OF343	0.163	0.163	0.506	0.296	0.19	3.55	
OF 343	0.103		0.300	0.250	0.13	0.00	
OF343	0	0	1.347	0	0	0	
OF360	0	0	1.347	0	0	0	
OF360 OF363	0	0	1.343	0	0	0	
	0	0			0	0	
OF365			0				
OF367	0	0	0		0	0	
OF369	0	0	0		0	0	
OF526	0.19	0.19	0.711	0.189	0.26	1.51	
OF53403	0	0	1.291	0	0	0	0
DETENTION DAGIN DETAIL O							
DETENTION BASIN DETAILS							
	NA	March (al	11 0	14 0	Marco.		
Name	Max WL	MaxVol	Max Q	Max Q	Max Q		
Name			Total	Low Level	High Level		
Name EAST-B2	57.55	0	Total 0.055	Low Level 0.043	High Level 0.011		
Name EAST-B2 EAST-B5	57.55 67.1	0	Total 0.055 0.174	Low Level 0.043 0.138	High Level 0.011 0.036		
Name EAST-B2 EAST-B5 EAST-B6	57.55 67.1 61.4	0	Total 0.055 0.174 0.405	Low Level 0.043 0.138 0.377	High Level 0.011 0.036 0.028		Image: Constraint of the second sec
Name EAST-B2 EAST-B5 EAST-86 EAST-88	57.55 67.1 61.4 70.77	0 0 0 0	Total 0.055 0.174 0.405 0	Low Level 0.043 0.138 0.377 0	High Level 0.011 0.036 0.028 0		
Name EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B6 EAST-B9	57.55 67.1 61.4 70.77 63.3	0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0	Low Level 0.043 0.138 0.377 0 0	High Level 0.011 0.036 0.028 0 0 0		Image: Constraint of the second sec
Name EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B8 EAST-B1	57.55 67.1 61.4 70.77 63.3 58.88	0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196	Low Level 0.043 0.138 0.377 0 0 0	High Level 0.011 0.036 0.028 0 0 0 0 0 0.012		
Name EAST-B2 EAST-B5 EAST-B6 EAST-86 EAST-88 EAST-89 EAST-89 EAST-87	57.55 67.1 61.4 70.77 63.3 58.88 65.66	0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288	Low Level 0.043 0.138 0.377 0 0 0 0.184 0.258	High Level 0.011 0.036 0.028 0 0 0 0 0 0.012 0.03		
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B1 EAST-B7 EAST-B7	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36	0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146	High Level 0.011 0.036 0.028 0 0 0 0.012 0.031 0.012 0.03 0.044		Image: Second
Name EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-80 EAST-81 EAST-87 EAST-87 Bo-retention	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 73.1	0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0.196 0.288 0.189 0	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0	High Level 0.011 0.036 0.028 0 0 0 0 0 0.012 0.03 0.044 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		Image: Second
Name EAST-82 EAST-86 EAST-86 EAST-86 EAST-80 EAST-80 EAST-80 EAST-81 EAST-87 EAST-87 EAST-810 Bio-retention EAST-84	57.55 67.11 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0.196 0.288 0.189 0 0.111	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111	High Level 0.011 0.036 0.028 0 0 0.012 0.032 0.012 0.03 0.044 0 0 0.044		Image: Section of the sectio
Name EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-80 EAST-81 EAST-87 EAST-87 Bo-retention	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 73.1	0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0.196 0.288 0.189 0	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0	High Level 0.011 0.036 0.028 0 0 0 0 0 0.012 0.03 0.044 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		Image:
Name EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B4 EAST-B3	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 73.1 71.34 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0.0405 0 0.196 0.288 0.189 0 0.111 0.031	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0.111	High Level 0.011 0.036 0.028 0 0 0.012 0.032 0.012 0.03 0.044 0 0 0.044		Image: Section of the sectio
Name EAST-B2 EAST-B5 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B10 Bio-retention EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east /r	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 73.1 71.34 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0.0405 0 0.196 0.288 0.189 0 0.111 0.031	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0.111	High Level 0.011 0.036 0.028 0 0 0.012 0.032 0.012 0.03 0.044 0 0 0.044		Image: Section of the sectio
Name EAST-B2 EAST-B2 EAST-B4 EAST-B6 EAST-B6 EAST-B7 EAST-B8 Bio-releation EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east n No water upwelling from any pit.	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 73.1 71.34 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0.0405 0 0.196 0.288 0.189 0 0.111 0.031	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0.111	High Level 0.011 0.036 0.028 0 0 0.012 0.032 0.012 0.03 0.044 0 0 0.044		Image: Section of the sectio
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041		Image: Section of the sectio
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041	=367, OF36	5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF32
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041	=367, OF36	5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF32
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041	F367, OF36	5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF320
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041		5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF320
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041		5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF320
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041	F367, OF36	5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF320
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041	=367, OF36	5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF320
Name EAST-B2 EAST-B6 EAST-B6 EAST-B6 EAST-B6 EAST-B7 EAST-B7 EAST-B1 EAST-B1 EAST-B1 EAST-B1 EAST-B4 EAST-B4 EAST-B4 EAST-B3 Run Log for 12546218 AlbanyMotorPark_east r No water upweiling from any pit. E95 Freeboard was less than 0.15m at Pit296	57.55 67.1 61.4 70.77 63.3 58.88 65.66 62.36 62.36 73.1 71.34 70.56 70.56	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Total 0.055 0.174 0.405 0 0 0 0.196 0.288 0.189 0 0.191 0.288 0.189 0.031 sing version 2	Low Level 0.043 0.138 0.377 0 0 0.184 0.258 0.146 0 0.111 0 0 0.1111 0 0 020.036	High Level 0.011 0.036 0.028 0 0 0 0.012 0.03 0.044 0.044 0.041	F367, OF36	5, OF363, OF343, OF341, OF339, OF334, OF326, OF324, OF320

Stage 1B (EAST) DRAINS Results								
DRAINS results prepared from Version 2020.036 1% AEP PIT / NODE DETAILS				Versien 9				
PTL/ NODE DETAILS Name	Max HGL		Max Surface		Min Freeboard		Constraint	
 E-B2-02-US	60.5	HGL	Flow Arriving (cu.m/s) 0	(cu.m)	(m)	(cu.m/s)		
N57 N58	56.49		0					
E-B2-01-US E-B5-CULV1-HW	63.5		0.761		-0.16	0.406	Headwall height/system capacity	
N61643 N302	65.55		0.176		-0.10	0.400	neadwair neight/system capacity	
DUMMY-SCALE2 DUMMY-SCALE1	10		0.170					
E-B5-01-US E-B5-02-US	71		0					
E-B3-02-03 E-B7-CULV2-HW E-B7-CULV2-DS	72.93		0.15		0.57	0	None	
E-B7-06-V2-50 E-B7-04-US E-B7-05-US	73		0					
E-B9-CULV1-HW E-B9-CULV1-DS	68.19 66.62		0.317		0.31	0	None	
E-B9-07-US E-B9-08-US	73 68.5		0.123					
 E-B9-05-US E-B9-06-US	71		0					
E-B9-CULV2-HW E-B9-CULV2-DS	65.71 64.21		0.49		0.29	0	None	
E-B9-03-US E-B9-04-US	71		0					
E-B9-01-US E-B9-02-US	69.5 65.5		0					
N306 N297	60.42 55.54		0					
E-B7-07-US N296	70.1		0					
N305 N304	57.19		0					
N61649 N298	64.45 63.35		0					
N367 N294	61.64 60.83		0.33					
E-B9-CULV3-HW E-B9-CULV3-DS	61.52 60.22		0.332		0.48	0	None	
E-B9-C0LV3-DS E-B10-01-US E-B10-02-US	63.5		0					
E-B10-02-05 E-B10-03-US E-B10-CULV1-HW	65.5 64.73		0.074		0.77	n	None	
E-B10-CULV1-DS E-B10-04-US	63.09 67		0.057		0.11		nono -	
E-B10-05-US E-B6-01-US	68 66.5		0					
E-B6-02-US E-B6-03-US	69.5 63.5		0					
E-B7-01-US E-B7-02-DS	69.57 69.66		0.146					
E-B7-03-DS E-B7-02-US	70.65		0.078					
E-B7-03-US E-B7-CULV1-HW	72 68.83		0.372		0.17	0	None	
Pit1448 E-B7-CULV1-DS	68.18 65.94	68.3	0.267	0.4	0	0	Outlet System	
E-B7-08-US E-B7-09-US	72 70		0					
E-B7-10-US E-B7-11-DS	69.5 65.92		0.628					
 E-B3-02-US E-B3-01-US	70.75		0					
E-B4-01-US E-B4-02-DS	72		0.277					
E-B4-02-US E-B1-01-US	73 58.5		0					
E-B1-CULV1-DS E-B1-02-US	59.98 60.5		0.156					
E-B1-03-SPLIT E-B1-03-US	65.7 68.5		0.266					
E-B1-04-DS E-B1-04-US	68.51 69.5		0.09					
Pit8 E-B7-CULV3-DS	68.57 67.25	69.17	0.173		0.43	0	Inlet Capacity	
N266 E-B8-01A-US	66.99 71.2		0.654					
E-B8-01B-US N388	73 55.51		0.056					
N511 N539	67.23 51.79		0.107					
 Pit1296 N61629	72.06 69.47	72.16	0.087	0.2	0	0	Outlet System	
 N299 HW1478	68.23 49.6		0		-0.1	0.545	Headwall height/system capacity	
 N59 HW1479	47.46 52.97		0.801		0.03		None	
N38873 HW1480	51.27 57.53		1.1 0.878		-0.03	0.088	Headwall height/system capacity	
N38880	55.7		0.383					
SUB-CATCHMENT DETAILS Name	Max		Grassed	Paved	Grassed		Due to Storm	
	Flow Q (cu.m/s)	Max Q (cu.m/s)	Max Q (cu.m/s)	Tc (min)	Tc (min)	Tc (min)		
EAST-B2-CAT E-B5	0.71	0	-0.013		7.2	0	1% AEP, 10 min burst, Storm 2 1% AEP, 10 min burst, Storm 4	
EAST-B5-CAT E-B7-A	0.264	0	0	3.8	19.2	0	1% AEP, 20 min burst, Storm 7 1% AEP, 10 min burst, Storm 4	
E-B9-A E-B9-B	0.602	0	0	1.19		0	1% AEP, 15 min burst, Storm 5 1% AEP, 15 min burst, Storm 8	
E-B9-C E-B9-D	0.297	0	0	1.65	4.18	1.87	1% AEP, 15 min burst, Storm 8 1% AEP, 10 min burst, Storm 4	
EAST-B6-CAT EAST-B8-CAT	1.694 0.28	0	824.713 443.483	2.18	5.06 2.58	0	1% AEP, 15 min burst, Storm 1 1% AEP, 15 min burst, Storm 8	
EAST-B9-CAT EAST-B1-CAT	0.035		0	2.13	2.24 4.96	2.42	1% AEP, 10 min burst, Storm 4 1% AEP, 10 min burst, Storm 10	
EAST-B7-CAT EAST-B10-CAT	0.078	61.47	0	1.65	3.83	1.87	1% AEP, 10 min burst, Storm 10 1% AEP, 15 min burst, Storm 8	
E-B10-A E-B10-03-CATA	0.122	0.362	60.712 72	1.31	2.5 3.04	1.48	1% AEP, 10 min burst, Storm 4 1% AEP, 15 min burst, Storm 8	
E-B7-02-CAT E-B7-03-CAT	0.155	0.011	57.552 63.5		6.08 5.04	2.46	1% AEP, 15 min burst, Storm 1 1% AEP, 10 min burst, Storm 9	
E-B7-B-CAT E-B7-C	0.298	73	0.121	2.5	12.03 5.81	2.83	1% AEP, 15 min burst, Storm 7 1% AEP, 15 min burst, Storm 9	
E-B7-10-CATB E-B7-11-CAT	0.041	10	0	0	6.53 4.04	0	1% AEP, 15 min burst, Storm 1 1% AEP, 15 min burst, Storm 8	
E-B4-02-CAT E-B1-02-CATA	0.48	0.137	0.023	1.89	0	2.15	1% AEP, 10 min burst, Storm 4 1% AEP, 15 min burst, Storm 8	
E-B1-03-US-CAT E-B1-04-CAT	0.356		0.145	0	5.58 2.55	0	1% AEP, 10 min burst, Storm 6 1% AEP, 10 min burst, Storm 4	
E-B7-01-CAT	0.29	56.369	0.054	2.55	5.94	2.89	1% AEP, 10 min burst, Storm 2	

Decode of the second	Cat314	0.078	0	0	0	7.02	0	1% AEP, 10 min burst, Storm 10	
Bate Mach Frage							0	1% AEP, 20 min burst, Storm 5	
Box Des Des <thdes< th=""> <thdes< th=""> <thdes< th=""></thdes<></thdes<></thdes<>	E-B7-10-CATA	0.182	0.174	0	2.57	5.96	2.91	1% AEP, 10 min burst, Storm 2	
manual product product <t< td=""><td>EAST-B4-CAT</td><td>0.05</td><td>0</td><td>68</td><td>3.56</td><td>8.26</td><td>4.03</td><td>1% AEP, 10 min burst, Storm 6</td><td></td></t<>	EAST-B4-CAT	0.05	0	68	3.56	8.26	4.03	1% AEP, 10 min burst, Storm 6	
Name No. No. </td <td> EAST-B3-CAT</td> <td>0.72</td> <td>0</td> <td>0.024</td> <td>2.15</td> <td>4.99</td> <td>2.43</td> <td>1% AEP, 10 min burst, Storm 10</td> <td></td>	 EAST-B3-CAT	0.72	0	0.024	2.15	4.99	2.43	1% AEP, 10 min burst, Storm 10	
	 Name	Max Q (cu.m/s)				Due to Storm			
Prop Prop <th< td=""><td></td><td>0.241</td><td>2.81</td><td>57.071</td><td></td><td></td><td></td><td></td><td></td></th<>		0.241	2.81	57.071					
No.50 Aug Aug </td <td>E-B5-CULV1</td> <td>0.386</td> <td>2.43</td> <td>67.978</td> <td>67.238</td> <td>1% AEP, 15 min burst, Storm 6</td> <td></td> <td></td> <td></td>	E-B5-CULV1	0.386	2.43	67.978	67.238	1% AEP, 15 min burst, Storm 6			
Solution 413 320 12	Pipe179	0.464	3.97	65.55	64.847	1% AEP, 1 hour burst, Storm 7			
Bestory 0.00 <					72.206	1% AEP, 10 min burst, Storm 3			
Pro01 Origination Origination <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>									
Prob Dots Dots <th< td=""><td>Pipe283</td><td>0.592</td><td>4.87</td><td>61.018</td><td>60.422</td><td>1% AEP, 30 min burst, Storm 2</td><td></td><td></td><td></td></th<>	Pipe283	0.592	4.87	61.018	60.422	1% AEP, 30 min burst, Storm 2			
PAG2 Add Add Pack P	Pipe184	0.024	0.88	70.56	70.103	1% AEP, 2 hour burst, Storm 3			
Pisk Boo Boo <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>									
Profile Disk Disk <thdisk< th=""> Disk Disk <</thdisk<>				57.192 65.212					
Parta Add Add </td <td>Pipe182</td> <td>0.702</td> <td>5.38</td> <td>64.452</td> <td>63.352</td> <td>1% AEP, 30 min burst, Storm 8</td> <td></td> <td></td> <td></td>	Pipe182	0.702	5.38	64.452	63.352	1% AEP, 30 min burst, Storm 8			
	Pipe186	0.55	3.01	61.644	60.87	1% AEP, 30 min burst, Storm 8			
ECOUNT BUD BUD<					60.258 63.085	1% AEP, 2 hour burst, Storm 3 1% AEP, 15 min burst, Storm 1			
Backbar Backbar <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>									
Partin BOD Disk Disk <thdisk< th=""> Disk <thdisk< th=""> <thd< td=""><td>E-B7-CULV3</td><td>0.284</td><td>2.02</td><td>68.38</td><td>67.373</td><td>1% AEP, 15 min burst, Storm 1</td><td></td><td></td><td></td></thd<></thdisk<></thdisk<>	E-B7-CULV3	0.284	2.02	68.38	67.373	1% AEP, 15 min burst, Storm 1			
Next Open Appendix App	Pipe178	0.201	1.26	71.099	70.758	1% AEP, 10 min burst, Storm 7			
Pipelon 1/20 3/20 1/20	Pipe177	0.282	2.77	69.466	68.233	1% AEP, 1 hour burst, Storm 2			
Paper Paye Sol									
New <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>									
processor box processor pro		Max Q	Max V			Due te Sterr			
NearNearNearNearNearNearNearNearNearNearNear00181000018001	Name					Due to Storm			
NearNearNearNearNearNearNearNearNearNearNear00181000018001	OVERFLOW ROUTE DETAILS								
Soft BLO 001 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 0 1 1 0 1 0 1 0 1 1 0 1 1 0 1 1 0 1	Name				Max D				
Box 660 002 0	EAST-B10-O	0.018	0	12.141		0	32	0	1% AEP, 30 min burst, Storm 8
Cellon C. O Out // DAS	EAST-B6-0	0.012	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 2
E B00 CAA 0 0.000 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>0.59</td><td>1% AEP, 15 min burst, Storm 1</td></th<>								0.59	1% AEP, 15 min burst, Storm 1
E 68:00 0 0.98 0.87 0.38 0.08 0.89 <th0.89< th=""> 0.89 0.89 <th0< td=""><td> E-B10-03A</td><td></td><td>0.095</td><td>0.885</td><td>0.176</td><td>0.09</td><td>2.11</td><td>0.66</td><td>1% AEP, 10 min burst, Storm 9</td></th0<></th0.89<>	 E-B10-03A		0.095	0.885	0.176	0.09	2.11	0.66	1% AEP, 10 min burst, Storm 9
68101 0 0.08 0.44 0.15 1.04 1.84.PF 1.06 <th< td=""><td>E-B10-04</td><td>0</td><td>0.059</td><td>0.787</td><td>0.319</td><td>0.06</td><td>3.83</td><td>0.59</td><td>1% AEP, 10 min burst, Storm 9</td></th<>	E-B10-04	0	0.059	0.787	0.319	0.06	3.83	0.59	1% AEP, 10 min burst, Storm 9
E8.638 0.212 0.233 0.84 0.21 2.23 1.13 1% ABP 1 mm bard Sem 1 C8.030 0 0.434 0.74 0.25 0.32 0.141 0.944	E-B1-01	0	0.092	0.36	0.144	0.13	1.73	1.04	1% AEP, 10 min burst, Storm 9
8 8 0									
	E-B1-03A	0	0.352	0.73	0.253	0.26	3.03	1.14	1% AEP, 10 min burst, Storm 6
E8-01 0 0.38 1.186 0.21 0.37 1.86 1.96 1.97 1.86 1.97 1.86 1.97 1.86 1.97 1.86 1.97 1.86 1.97 1.86 1.97 1.86 1.97 1.86 1.97 1.86 1.97 1.86 1.97 <th< td=""><td>E-B1-04</td><td>0</td><td>0.104</td><td>0.719</td><td>0.23</td><td>0.15</td><td>1.84</td><td>0.91</td><td>1% AEP, 15 min burst, Storm 1</td></th<>	E-B1-04	0	0.104	0.719	0.23	0.15	1.84	0.91	1% AEP, 15 min burst, Storm 1
E8-01 0 0.171 0.56 2.24 0.11 2.26 0.51 1.18, AP, 16 mb bar, 38 mb a E43-52 0.01 0.281 0.397 0.248 0.03 0.27 0.21 1.18, AP, 16 mb bar, 38 barn 4 E43-52 0 0.486 0.397 0.21 0.27 0.21 0.11 1.18, AP, 16 mb bar, 38 barn 4 E43-52 0 0.486 1.19 1.21 1.19, AP, 10 mb bar, 38 barn 4 E43-52 0 0.486 1.19 1.21 0.43 0.11 1.19, AP, 10 mb bar, 38 barn 4 E43-52 0 0.486 1.596 0.54 0.21 4 1.19, AP, 10 mb bar, 38 barn 4 E43-52 0 0.486 0.54 0.21 4 1.19, AP, 10 mb bar, 38 barn 4 E43-53 0 0.486 0.54 0.51 2.4 0.51 1.4, 40, 14 2.9 0.51 1.4, 40, 14 1.19, AP, 10 mb bar, 38 barn 4 E43-63 0 0.47 0.54 0.54 0.08 1.19, AP, 10 mb bar, 38 ba									
E8.02 0.01 0.281 0.287 0.788 0.04 0.059 0.11 1% APP 10 mbard. Some 1 E8.402 0 0.102 1.480 1.441 0.03 1.01 1% APP 10 mbard. Some 1 E8.502 0 0.486 1.397 0.43 9.97 1.11 1% APP 10 mbard. Some 1 E8.502 0 0.486 1.937 0.43 9.97 1.41 1% APP 10 mbard. Some 1 E8.502 0 0.486 1.937 0.43 1% APP 10 mbard. Some 1 E8.501 0 0.53 0.940 0.644 0.16 7.27 0.163 1% APP 10 mbard. Some 1 E8.501 0.051 0.286 0.840 0.24 0.241	E-B2-02		0.317	1.157	0.185			1.54	1% AEP, 10 min burst, Storm 2
E-B-02 0 0.428 0.292 0.348 0.038 2.79 1.11 1% AEP. 10 mbard. Stern A E-B-01 0 0.22 1.990 0.614 0.28 9.77 1.11 1% AEP. 10 mbard. Stern A E-B-01 0 0.22 1.990 0.614 0.21 0.21 1.991 1.942 <td>E-B3-02</td> <td>0.01</td> <td>0.291</td> <td>0.367</td> <td>0.749</td> <td>0.06</td> <td>8.99</td> <td>0.1</td> <td>1% AEP, 10 min burst, Storm 6</td>	E-B3-02	0.01	0.291	0.367	0.749	0.06	8.99	0.1	1% AEP, 10 min burst, Storm 6
6.86.02 0 0.948 1.99 1.297 0.43 0.977 1.04 1% AEP 15 min back_3 Sum 8 6.86.01 0 0.055 1.04 0.81 0.77 0.05 1% AEP 15 min back_3 Sum 8 6.86.701 0.055 0.04 0.034 0.61 2.43 0.051 1% AEP 15 min back_3 Sum 1 6.87.71 0.012 0.026 0.014 0.034 0.613 2.44 0.051 1% AEP 15 min back_3 Sum 1 6.87.741 0 0.127 0.526 0.013 2.44 0.051 1% AEP 15 min back_3 Sum 1 6.87.64 0 0.127 0.526 0.054 0.061 1% AEP 15 min back_3 Sum 1 6.87.66 0.020 0.596 0.554 0.61 0.61 1% AEP 15 min back_3 Sum 1 6.87.66 0.0122 0.606 0.521 0.66 0.61 1% AEP 15 min back_3 Sum 1 6.87.66 0.022 0.606 0.203 0.61 0.62 0.61 1% AEP 15 min back_3 Sum 1 6.87.66 0.017	E-B4-02	0	0.436	0.929	0.348	0.36	2.79	1.21	1% AEP, 10 min burst, Storm 4
E 68.62 0 0 0.16 1.59 0.614 0.21 4.91 1.19 1% AF, P.15 min bar, Sum B E 68.63 0.00 0.258 0.501 0.544 0.51 2.43 0.51 1% AF, P.15 min bar, Sum B E 67.63 0 0.212 0.542 0.161 0.44 0.15 2.43 0.01 1% AF, P.15 min bar, Sum B E 67.64 0 0.164 0.524 0.08 4.19 0.14 1% AF, P.10 min bar, Sum B E 67.65 0 0.0164 0.524 0.08 4.19 0.11 1% AF, P.10 min bar, Sum B E 67.66 0.207 0.280 0.139 0.17 6.81 0.421 0.44 0.91 1% AF, P.10 min bar, Sum B E 67.66 0.0 0.222 0.621 0.19 0.17 6.91 1% AF, P.10 min bar, Sum B E 67.60 0 0.122 0.61 0.19 0.12 2.44 0.91 1% AF, P.10 min bar, Sum B E 67.64 0 0.160 0.130									
E-86-03 0 0.655 0.614 0.28 7.71 0.761 ha AEP 15 mm bard, Stem 1 E-87-01 0.003 0.456 0.610 0.344 0.61 2.43 0.61 ha AEP 15 mm bard, Stem 1 E-87-02 0 0.128 0.396 0.151 2.43 0.63 ha AEP 15 mm bard, Stem 3 E-87-04 0 0.128 0.396 0.151 2.43 0.63 ha AEP 15 mm bard, Stem 3 E-87-05 0 0.063 1.356 0.554 0.01 4.19 0.11 ha AEP 15 mm bard, Stem 3 E-87-06 0.020 0.229 0.524 0.01 6.66 0.63 ha AEP 15 mm bard, Stem 3 E-87-06 0.041 0.122 0.524 0.524 0.521 0.51 0.51 0.51 ha AEP 15 mm bard, Stem 3 E-87-06 0.041 0.079 0.226 0.521 0.52 0.52 0.52 0.52 0.53 0.63 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53 0.53									
E87-02 0 0.18 0.395 0.15 2.34 0.83 is A&P. 15 min bard, Storm 6 E87-03 0 0.127 0.524 0.14 0.01 14.8 AP. 10 min bard, Storm 6 E87-04 0 0.164 0.034 0.241 0.251	 E-B6-03	0	0.655	0.45	0.614	0.26	7.37	0.76	1% AEP, 15 min burst, Storm 8
E87/4 0 0.194 0.294 0.084 4.19 0.34 (1% AEP, 10 mb bard, Storn 9 E87/05 0.027 0.289 1.589 0.844 0.271 0.88 1.71 1% AEP, 10 mb bard, Storn 9 E87/06 0.020 0.289 1.599 0.844 0.271 0.88 1.72 1% AEP, 15 mb bard, Storn 9 E87/06 0.020 0.174 0.770 0.228 0.13 2.71 0.061 (1% AEP, 15 mb bard, Storn 9 E87/08 0.174 0.770 0.228 0.13 2.71 0.061 (1% AEP, 15 mb bard, Storn 9 E87/18 0.199 0.174 0.707 0.228 0.13 2.71 0.061 (1% AEP, 15 mb bard, Storn 9 E87/11 0.522 0.579 0.089 0.81 0.43 0.32 0.154 AEP, 15 mb bard, Storn 9 E88/01 0.012 0.172 0.13 0.01 0.154 AEP, 15 mb bard, Storn 9 E88/01 0.012 0.172 0.153 0.211 0.02 0.154 AEP, 10 mb bard, Storn 9 E88/01 0.0102	E-B7-02	0	0.128	0.396	0.195	0.13	2.34	0.83	1% AEP, 15 min burst, Storm 8
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$								0.91	1% AEP, 10 min burst, Storm 6 1% AEP, 10 min burst, Storm 9
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$									
E87-09 0 0.222 0.606 0.203 0.12 2.44 0.691 18.4EP, 15 min burst, 3torm 9 E67-10A 0.169 0.170 0.226 0.13 2.71 0.611 18.4EP, 15 min burst, 3torm 8 E67-101 0.012 0.707 0.026 0.33 0.13 2.71 0.611 NAEP, 15 min burst, 3torm 8 E67-11 0.012 0.724 0.98 0.691 0.42 0.93 1.8AP, 15 min burst, 3torm 8 E68-01A 0.012 0.214 3 0 3.2 0.118 AEP, 15 min burst, 3torm 8 E68-01 0.012 0.25 0.211 0.02 2.53 0.611 1.8AP, 15 min burst, 3torm 8 E68-02 0 0.165 0.621 0.621 0.611 0.62 0.631 1.8AP, 15 min burst, 3torm 8 E68-04 0 0.165 0.622 0.014 9.62 0.631 1.8AP, 15 min burst, 3torm 8 E68-04 0 0.172 0.623 0.611 0.642 0.642 0.642 0.642 <td>E-B7-07</td> <td>0.024</td> <td>0.192</td> <td>1.226</td> <td>0.832</td> <td>0.14</td> <td>6.66</td> <td>0.63</td> <td>1% AEP, 15 min burst, Storm 6</td>	E-B7-07	0.024	0.192	1.226	0.832	0.14	6.66	0.63	1% AEP, 15 min burst, Storm 6
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	E-B7-09	0	0.222	0.606	0.203	0.12	2.44	0.59	1% AEP, 15 min burst, Storm 9
E B7-11 0.579 0.988 0.691 0.34 5.53 0.8 [19 AEP, 15 mn burst, Storm 8 E B7-01 0.013 0.732 0.53 0.06 4.24 0.29 [19 AEP, 15 mn burst, Storm 8 E B8-016 0 0.067 1412 0.53 0.066 4.24 0.26 [19 AEP, 15 mn burst, Storm 8 E B8-018 0 0.255 0.956 0.211 0.2 2.53 1.05 [19 AEP, 10 mn burst, Storm 9 E B8-04 0 0.163 0.962 0.802 0.141 9.62 0.81 [19 AEP, 15 mn burst, Storm 9 E B8-06 0 0.163 0.962 0.802 0.614 9.62 0.81 [19 AEP, 15 mn burst, Storm 9 E B8-06 0 0.023 1.146 0.266 0.99 1.65 0.41 [19 AEP, 15 mn burst, Storm 7 E B8-06 0 0.023 1.464 0.26 0.99 [19 AEP, 15 mn burst, Storm 7 E B8-06 0 0.023 1.464 0.26 0.99 [19 AEP, 15 mn burst, Storm 7 D B025 0.012 0 1.2141 3		0.169	0.193	1.036		0.19	3.45	0.82	1% AEP, 15 min burst, Storm 8
E-88-01A 0 0.113 0.732 0.53 0.06 4.24 0.28 (% AEP, 15 min burs, Storm 8) E-88-01B 0 0.0257 0.955 0.211 0.22 2.53 1.05 (% AEP, 15 min burs, Storm 9) E-89-02 0 0.115 0.0351 0.092 0.011 0.05 0.011 0.05 0.011 0.05 0.011 0.05 0.011 0.05 0.011 0.05 0.011 0.012 0.011 <td></td> <td></td> <td></td> <td></td> <td>0.691</td> <td></td> <td></td> <td>0.8</td> <td>1% AEP, 15 min burst, Storm 8 1% AEP, 30 min burst, Storm 8</td>					0.691			0.8	1% AEP, 15 min burst, Storm 8 1% AEP, 30 min burst, Storm 8
E89.0100.2550.04550.2110.022.531.061% AEP, 10 min burs, Storm 9 $E89.02$ 00.1150.6310.2110.092.530.611% AEP, 15 min burs, Storm 9 $E89.04$ 00.1630.0620.020.149.620.51% AEP, 15 min burs, Storm 8 $E89.04$ 00.1321.1320.2030.161.620.831% AEP, 15 min burs, Storm 8 $E89.06$ 00.0731.1460.2060.091.1650.47% AEP, 15 min burs, Storm 8 $E89.06$ 00.1220.4900.7810.296.250.991% AEP, 15 min burs, Storm 7 $D0.05$ 0.012012.1410320.1% AEP, 16 min burs, Storm 7 $D0.05$ 0.012012.1410320.1% AEP, 16 min burs, Storm 7 $D2292$ 0.018012.1410320.1% AEP, 16 min burs, Storm 8 $D23068$ 0.013012.1410320.1% AEP, 16 min burs, Storm 8 $D23068$ 0.013012.1410320.1% AEP, 16 min burs, Storm 8 $D23069$ 0.013012.1410320.1% AEP, 16 min burs, Storm 8 $D31546$ 0.013012.1410320.1% AEP, 16 min burs, Storm 8 $D31546$ 0.013012.1410320.1% AEP, 16 min burs, Storm 8 $D31546$ 0.013012.1410320.1% AEP, 16 min burs, Storm 7 </td <td>E-B8-01A</td> <td>0</td> <td>0.113</td> <td>0.732</td> <td></td> <td>0.06</td> <td>4.24</td> <td>0.29</td> <td>1% AEP, 15 min burst, Storm 8</td>	E-B8-01A	0	0.113	0.732		0.06	4.24	0.29	1% AEP, 15 min burst, Storm 8
E-69-03 0 0.163 0.962 0.002 0.14 9.62 0.081 % AEP, 15 min burst, Storm 8 E-69-05 0 0.115 0.685 0.802 0.07 9.62 0.51 % AEP, 15 min burst, Storm 8 E-69-06 0 0.132 1.632 0.203 0.16 1.62 0.83 1% AEP, 15 min burst, Storm 8 E-69-07 0 0.402 1.254 0.781 0.29 6.25 0.99 1% AEP, 15 min burst, Storm 10 E-69-08 0 0.122 0.12 12.141 3 0 32 0.1% AEP, 15 min burst, Storm 10 Iow-25 0.012 0 12.141 3 0 32 0.1% AEP, 10 min burst, Storm 17 Iow25 0.018 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 18 Io23965 0.018 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 2 IO23965 0.013 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 2 IO31	E-B9-01	0	0.255	0.955	0.211	0.2	2.53	1.05	1% AEP, 10 min burst, Storm 9
E-89-05 0 0.132 1.632 0.0203 0.16 1.62 0.83 1% AEP, 15 min burst, Storm 8 E-89-07 0 0.402 1.254 0.208 0.29 6.25 0.99 1% AEP, 15 min burst, Storm 6 E-89-08 0 0.125 0.949 0.781 0.029 6.25 0.091 % AEP, 15 min burst, Storm 6 Iow-5 0.012 0 12.411 3 0 32 0 % AEP, 15 min burst, Storm 7 Iow05 0.012 0 12.411 3 0 32 0 % AEP, 15 min burst, Storm 7 Iow05 0.018 0 12.411 3 0 32 0 % AEP, 30 min burst, Storm 8 023058 0.013 0 12.411 3 0 32 0 % AEP, 30 min burst, Storm 9 031545 0.013 0 12.411 3 0 32 0 % AEP, 10 min burst, Storm 8 031545 0.013 0 12.411 3 0 3	E-B9-03	0	0.163	0.962	0.802	0.14	9.62	0.89	1% AEP, 15 min burst, Storm 8
E-89-06 0 0.073 1.146 0.206 0.09 1.65 0.471 1% AEP, 15 min burst, Storm 9 E-89-07 0 0.402 1254 0.781 0.29 6.25 0.991 % AEP, 10 min burst, Storm 10 Iow-25 0.012 0 12.141 3 0 32 0.1% AEP, 10 min burst, Storm 7 Iow05 0.012 0 12.141 3 0 32 0.1% AEP, 10 min burst, Storm 7 O22992 0.018 0 12.141 3 0 32 0.1% AEP, 10 min burst, Storm 7 O22056 0.018 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 O22066 0.013 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 2 O31544 0.013 0 12.141 3 0 32 0.1% AEP, 10 min burst, Storm 2 O31559 0.013 0 12.141 3 0 32 0.1% AEP, 10 min burst, Storm 2 O72267 <								0.83	1% AEP, 15 min burst, Storm 8
E-B9-08 0 0.125 0.941 0.05 6.25 0.27 1% AEP, 10 m burst, Storm 10 low 5 0.012 0 12.141 3 0 32 0.1% AEP, 10 m burst, Storm 7 022992 0.018 0 12.141 3 0 32 0.1% AEP, 10 m burst, Storm 7 023058 0.018 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 023068 0.013 0 12.141 3 0 32 0 1% AEP, 30 min burst, Storm 8 023069 0.014 0 12.141 3 0 32 0 1% AEP, 30 min burst, Storm 8 031534 0.013 0 12.141 3 0 32 0 1% AEP, 10 mu burst, Storm 1 031545 0.013 0 12.141 3 0 32 0 1% AEP, 10 mu burst, Storm 2 072267 0.012 0 12.141 3 0 32 0 1% AEP, 10 mu burst, Storm 1 072283	 E-B9-06	0	0.073	1.146	0.206	0.09	1.65	0.47	1% AEP, 15 min burst, Storm 9
low6.5 0.012 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 7 023058 0.018 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 023068 0.013 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 029069 0.014 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 031534 0.013 0 12.141 3 0 32 0.1% AEP, 10mr burst, Storm 2 031545 0.013 0 12.141 3 0 32 0.1% AEP, 11mr burst, Storm 2 031559 0.013 0 12.141 3 0 32 0.1% AEP, 10mr burst, Storm 2 072283 0.012 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 3 0F139 0 0 1.2.141 3 0 32 0.1% AEP, 10mr burst, Storm 2 0F139 0.016 0 1.2.141 0	E-B9-08	0	0.125	0.949	0.781	0.05	6.25	0.27	1% AEP, 10 min burst, Storm 10
O22992 0.018 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 O23058 0.013 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 O23069 0.014 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 O31534 0.013 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 O31534 0.013 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 O31545 0.013 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 O72267 0.012 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 O72283 0.016 0 12.141 3 0 32 0.1% AEP, 3 min burst, Storm 1 OF139 0 0 1 0 0 2 0.1% AEP, 1 hour burst, Storm 1 OF153 0.239 0.242 0.242 <th< td=""><td>low0.5</td><td>0.012</td><td>0</td><td>12.141</td><td>3</td><td>0</td><td>32</td><td>0</td><td>1% AEP, 1 hour burst, Storm 7</td></th<>	low0.5	0.012	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 7
Q29065 0.013 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 Q29069 0.014 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 8 Q31534 0.013 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 Q31559 0.013 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 Q72267 0.012 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 Q72267 0.012 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 Q72267 0.012 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 Q69296 0.016 0 12.141 0 32 0.1% AEP, 1 hour burst, Storm 1 QF139 0 0 1 0 0 0 0 QF144 0.232 0.487 0.242 0.242 0.242 0					3			0	1% AEP, 30 min burst, Storm 8
O31534 0.013 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 O31545 0.013 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 O31559 0.012 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 O72267 0.012 0 12.141 3 0 32 0.1% AEP, 3 min burst, Storm 2 O72283 0.012 0 12.141 3 0 32 0.1% AEP, 3 min burst, Storm 2 O8296 0.016 0 12.141 3 0 32 0.1% AEP, 1 hour burst, Storm 2 OF139 0 0 1.7 0 0 0 0 OF144 0.131 0.282 0.247 0.242 0.26 2.9 1.51 % AEP, 15 min burst, Storm 1 OF153 0.284 0.312 0.242 0.26 2.9 1.51 % AEP, 15 min burst, Storm 1 OF165 0.592 0.837 1.126 0.972 0.64<	O29065	0.013	0	12.141		0	32	0	1% AEP, 30 min burst, Storm 8
O31559 0.013 0 12.141 3 0 32 0.1% AEP. 1 how burst, Storm 2 O72287 0.012 0 12.141 3 0 32 0.1% AEP. 3 min burst, Storm 2 O72283 0.012 0 12.141 3 0 32 0.1% AEP. 3 min burst, Storm 2 O8296 0.016 0 12.141 3 0 32 0.1% AEP. 3 min burst, Storm 2 OF139 0 0 1.7 0 0 0 0 OF144 0.131 0.282 0.847 0.201 0.24 2.41 1.19 1% AEP. 15 min burst, Storm 1 OF153 0.284 0.319 0.482 0.242 0.26 2.9 1.51 % AEP. 15 min burst, Storm 1 OF159 0.284 0.319 0.488 0.222 2.98 0.941 % AEP. 15 min burst, Storm 1 OF18 0.259 0.837 1.126 0.972 0.54 11.67 2.21% AEP. 15 min burst, Storm 1 OF26 0.951 <	O31534	0.013	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 2
O72283 0.012 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 2 O6296 0.016 0 12.141 3 0 32 0.1% AEP, 30 min burst, Storm 7 OF139 0 0 1.7 0 0 0 1% AEP, 1 hour burst, Storm 7 OF144 0.131 0.282 0.847 0.201 0.24 2.41 1.19 1% AEP, 15 min burst, Storm 1 OF153 0.239 0.277 1.234 0.242 0.26 2.9 1.51 % AEP, 15 min burst, Storm 1 OF159 0.284 0.319 0.484 0.242 0.28 0.94 1% AEP, 15 min burst, Storm 1 OF165 0.592 0.837 1.126 0.972 0.54 11.67 0.424 AEP, 15 min burst, Storm 10 OF22 0 0 1.33 0 0 0 0 0 0 OF22 0.93 0.953 19.201 0.413 0.03 32 0.11 % AEP, 10 min burst, Storm 2 0.61 32 0.61	O31559	0.013	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 2
09296 0.016 0 12.141 3 0 32 0.1% AEP, 1 hour burst, 5torm 7 0F139 0 0 1.7 0 0 0 0 0F144 0.131 0.282 0.847 0.201 0.24 2.41 1.19 1% AEP, 15 min burst, Storm 1 0F153 0.239 0.277 1.234 0.242 0.26 2.9 1.57 1% AEP, 15 min burst, Storm 1 0F159 0.284 0.319 0.448 0.248 0.222 2.96 0.91 % AEP, 15 min burst, Storm 1 0F165 0.592 0.837 1.126 0.972 0.54 11.67 2.21 % AEP, 15 min burst, Storm 1 0F165 0.592 0.837 1.124 0.972 0.54 11.67 2.21 % AEP, 15 min burst, Storm 1 0F22 0 0 1% AEP, 10 min burst, Storm 1 0.252 0.051 0.41 % AEP, 10 min burst, Storm 1 0F226 0.953 0.953 1.9201 0.413 0.03 2 0.11 % AEP, 10 min burst, Storm 3									
OF144 0.131 0.282 0.847 0.201 0.24 2.41 1.19 1% AEP, 15 min burst, Storm 1 OF153 0.239 0.277 1.234 0.242 0.26 2.9 1.57 % AEP, 15 min burst, Storm 1 OF159 0.284 0.319 0.488 0.242 0.26 2.9 0.94 % AEP, 15 min burst, Storm 1 OF165 0.592 0.837 1.126 0.972 0.54 11.67 2.21% AEP, 15 min burst, Storm 1 OF18 0.252 19.227 0.266 0.01 32 0.41 % AEP, 15 min burst, Storm 1 OF22 0 0 1.33 0 0 0 0 0 OF24 1.294 1.924 1.924 0.972 0.04 32 0.051 % AEP, 15 min burst, Storm 2 OF24 1.294 1.924 1.924 0.972 0.04 32 0.051 % AEP, 30 min burst, Storm 3 OF262 0 0 0 0 0 0 0	O9296	0.016	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 7
OF159 0.284 0.319 0.488 0.248 0.22 2.98 0.941 1% AEP, 10 min burst, Storm 2. OF165 0.562 0.837 1.126 0.972 0.54 11.67 2.2 1% AEP, 15 min burst, Storm 1. OF18 0.253 0.252 19.227 0.286 0.01 32 0.41 1% AEP, 140 min burst, Storm 10. OF22 0 0 1.33 0 0 0 0 OF226 0.953 0.953 19.201 0.413 0.03 32 0.11% AEP, 140 min burst, Storm 2. OF244 1.294 19.201 0.413 0.03 32 0.11% AEP, 100 min burst, Storm 3. OF266 0.03 0.972 0.04 32 0.051 1% AEP, 30 min burst, Storm 3. OF266 0.36 0.375 0.802 0.28 9.62 1.37 1% AEP, 30 min burst, Storm 9. OF283 0 0 19.916 0 0 0 0 0 0 OF309 0.089 0.085 19.13	OF144	0.131	0.282	0.847	0.201	0.24	2.41	1.19	1% AEP, 15 min burst, Storm 1
OF165 0.592 0.837 1.126 0.972 0.54 11.67 2.2 1% AEP, 15 min burst, Storm 1 OF18 0.253 0.252 19.227 0.266 0.01 32 0.41 1% AEP, 15 min burst, Storm 1 OF22 0 0 1.33 0 0 0 0 OF26 0.953 0.953 19.201 0.413 0.03 32 0.11% AEP, 14 our burst, Storm 10 OF244 1.294 1.294 19.201 0.972 0.04 32 0.05 1% AEP, 15 min burst, Storm 3 OF266 0 0 0 0 0 0 0 0 OF266 0.86 0.915 0.802 0.29 9.62 1.31 1% AEP, 30 min burst, Storm 9 OF233 0 0 19.16 0 0 0 0 0 0 OF315 0 0 0 0 0 0 0 0 0	OF159	0.284	0.319	0.488	0.248	0.22	2.98	0.94	1% AEP, 10 min burst, Storm 2
OF22 0 0 1.33 0 0 0 0 OF226 0.953 0.953 19.201 0.413 0.03 32 0.11% AEP, 10 min burst, Storm 2 OF244 1.204 1.204 19.201 0.972 0.04 32 0.05 1% AEP, 30 min burst, Storm 3 OF262 0 0 10.302 0 0 0 0 OF266 0.36 0.916 0.802 0.29 9.62 1.37 1% AEP, 30 min burst, Storm 9 OF293 0 0 19.196 0 0 0 0 OF309 0.809 0.085 19.31 0.206 0.32 0.29 %AEP, 15 min burst, Storm 9 OF315 0 0 1.403 0 0 0 0	OF165	0.592	0.837	1.126	0.972	0.54	11.67	2.2	1% AEP, 15 min burst, Storm 1
OF244 1.294 1.924 1.924 1.924 1.927 0.04 32 0.05 (1% AEP, 30 min burst, Storm 3) OF262 0 0 10.302 0 0 0 0 OF286 0.36 0.36 0.915 0.802 0.29 9.62 1.37 1% AEP, 30 min burst, Storm 9 OF286 0.36 0.19,196 0 0 0 0 0 OF309 0.099 0.085 19.13 0.206 0 32 0.29 1% AEP, 15 min burst, Storm 9 OF311 0 0 0 0 0 0 0 0 0	OF22	0	0	1.333	0	0	0	0	
OF266 0.36 0.936 0.915 0.802 0.29 9.62 1.37 1% AEP, 30 min burst, Storm 9 OF293 0 0 19.196 0 0 0 0 OF309 0.089 0.085 19.13 0.206 0 32 0.29 1% AEP, 15 min burst, Storm 9 OF311 0 0 0 0 0 0 0 OF355 0 0 1.403 0 0 0 0	OF244	1.294	1.294	19.201	0.972	0.04	32	0.05	1% AEP, 30 min burst, Storm 3
OF293 0 0 19.196 0 0 0 OF309 0.089 0.085 19.13 0.206 0 32 0.29 1% AEP, 15 min burst, Storm 9 OF311 0 0 0 0 0 0 0 OF315 0 0 1.403 0 0 0 0									
OF311 0 0 0.9 0 0 0 0 OF315 0 0 1.403 0 0 0 0 0	OF293	0	0	19.196	0	0	0	0	
	OF311	0	0	0.9	0	0	0	0	

OPC:NPT 0.284 0.087 1.189 0.28 0.51 1.28 1.48								
6F32 0.08 0.03 1.33 0.47 0.06 4 6.34 [15 AEP]. Inter burd, Sen CP32200 0F32200 0.056 0.56 0.564 0.066 0.07 11.31 127 [15 AEP]. Inter burd, Sen CP32206 0F32210 1.389 1.389 1.380 1.381 0.061 0.07 11.31 127 [15 AEP]. Inter burd, Sen CP32216 1.121 MAEP. Inter burd, Sen CP32218 1.131 1.121 MAEP. Inter burd, Sen CP32217 0.051 0.04 1.122 0.04 0.0 0 </td <td>OF32192</td> <td></td> <td></td> <td></td> <td>0.347</td> <td>0.36</td> <td>2.78</td> <td>1.03 1% AEP, 1 hour burst, Storm 7</td>	OF32192				0.347	0.36	2.78	1.03 1% AEP, 1 hour burst, Storm 7
0F3200 0.766 0.766 0.689 1.189 0.62 9.51 2.17 [1% AEP.] Inter bark. Steep 0.5220 0F32200 0.519 0.545 0.546 0.646 0.07 11.31 1.07 [1% AEP.] Inter bark. Steep 0.5220 0F32210 0.19 0.19 0.19 0.19 0.01 0.0 0.0 1.0 0F32210 0.244 0.243 0.040 1.12 0.28 0.86 1.24 1.74.8 1.74.87.2								
GF3228 G43 G43								
OF3209 OF320 OF3 OF3	OF32200	0.706	0.706	0.069	1.189	0.62		2.17 1% AEP, 1 hour burst, Storm 2
e P3213 e P3213 e P3214 e P321 e P32 e P3 e P32 e P3 e P3	OF32206	0.545	0.545	0.644	0.046	0.07	11.31	1.57 1% AEP, 1 hour burst, Storm 6
or 62216 0 0 7.74 0 0 0 0 0F32260 0.244 0.243 0.049 1.122 0.28 8.69 1.23 1.164, P. Zhou burd, Stor 0F32270 0.088 0.58 0.56 0.022 0.02 0.74 0.02 1.02 1.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.03 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.01 <td>OF32209</td> <td>0.919</td> <td>0.919</td> <td>17.383</td> <td>0.051</td> <td>0.03</td> <td></td> <td>0.56 1% AEP, 1 hour burst, Storm 6</td>	OF32209	0.919	0.919	17.383	0.051	0.03		0.56 1% AEP, 1 hour burst, Storm 6
or 62216 0 0 7.74 0 0 0 0 0F32260 0.244 0.243 0.049 1.122 0.28 8.69 1.23 1.164, P. Zhou burd, Stor 0F32270 0.088 0.58 0.56 0.022 0.02 0.74 0.02 1.02 1.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.02 0.03 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.05 0.01 <td></td> <td>1.385</td> <td>1.385</td> <td>19,179</td> <td>1.041</td> <td>0.04</td> <td>32</td> <td>1.12 1% AEP, 30 min burst, Storm 2</td>		1.385	1.385	19,179	1.041	0.04	32	1.12 1% AEP, 30 min burst, Storm 2
GF3218 GF3218 GF3219 GF321 GF321 GF321 GF321 GF32 GF33 GF33								
6 673220 0.244 0.245 0.649 1.122 0.28 8.88 1.29 1% AFP. 2 hour burk. Stor 0673227 0.698 0.698 0.676 0.602 0.622 0.62 7.74 0.69 1.129 0.44 9.88 1.138 1% AFP. 2 hour burk. Stor 0673227 0.088 0.646 0.41 0.622 0.63 2.34 1.138 1% AFP. 2 hour burk. Stor 0.67 0.62 0.77 4.01 0.24 1.121 0.644 0.63 2.34 1.131 1% AFP. 2 hour burk. Stor 0.67 0.67 4.01 0.22 0.141 0.24 1.154 0.614 0.67 4.01 2.24 1% AFP. 3 hour burk. Stor 0.67 0.640 1.033 0.22 0.141 4.02 2.11% AFP. 3 hour burk. Stor 0.67 0.640 0.640 0.640 0.640 0.640 0.640 0.640 0.641 0.65 0.39 7.86 0.759 0.759 1.116 0.649 0.65 0.39 7.86 0.751 1.59 1.59 1.59 1.59 1.59 1.59								
OF 5222 0.68 0.578 0.04 1.12 0.44 8.88 1.38 1% AEP. 30 mb bard, Store OF 52227 0.68 0.576 0.622 0.62 7.74 0.88 0.578 OF 5222 0.24 0.31 0.56 0.522 0.58 2.34 1.31 1% AEP. 2 hour burst. Store OF 524 0.346 0.451 0.522 0.52 0.34 0.31 6.08 1.57 30m burst. Store OF 530 0.447 0.457 1.346 0.522 0.11 1.05 2.21 % AEP. 30m burst. Store OF 534 0.459 0.471 1.346 0.522 0.14 4 2.31 % AEP. 30m burst. Store OF 534 0.406 1.333 0.228 0.14 4 2.31 % AEP. 15m burst. Store OF 543 0.406 0.455 0.269 0.260 0.28 7.81 1.82 1.82 1.82 1.82 1.82 1.82 1.82 1.82 1.82 1.82 1.								
OF 52227 0.088 0.088 0.576 0.022 0.02 7.74 0.82 1% AEP, 2 hour bars, Store OF 5229 0.45 0.45 0.45 0.45 0.45 0.41 0.222 0.38 2.34 1.32 1% AEP, 2 hour bars, Store OF 326 1.224 1.53 0.614 0.67 4.91 0.24 1% AEP, 30 min bars, Store OF 336 0.759 0.759 1.115 0.049 0.049 0.049 0.049 0.049 0.041 0.041 0.041 0.041 0.049 0.049 0.049 0.049 0.049 0.041 0.041 0.040 0.040 0.049 0.0								
OF3229 0.46 0.46 0.041 0.282 0.38 2.34 1.32 1% AEP, 2 how burk, Stor OF326 OF326 1.224 1.224 1.533 0.614 0.67 4.91 2.48 1% AEP, 3 how burk, Stor OF330 OF330 0.467 1.484 0.552 0.17 4 2.11% AEP, 3 how burk, Stor OF330 0.276 0.276 0.216 2.01% AEP, 3 how burk, Stor OF330 0.467 1.484 0.552 0.11 10.95 2.01% AEP, 3 how burk, Stor OF330 0.20% AEP, 1 sm burk, Stor OF330 0.469 0.414 0.655 0.39 7.86 1.67 1% AEP, 1 sm burk, Stor OF341 0.0 0<								
0F324 0.046 0.0376 0.328 0.01 31.6 0.66 1% AEP, 30m hburd, Store 0F326 1.224 1.234 1.33 0.614 0.87 4.91 2.48 1% AEP, 9hour burd, Store 0F330 0.447 0.447 1.345 0.552 0.17 4 3.21 1% AEP, 30m hburd, Store 0F334 0.759 1.150 0.453 0.111 0.055 2.9 1% AEP, 30m hburd, Store 0F334 0.468 0.468 1.339 0.228 0.14 4 2.31 1% AEP, 15m hburd, Store 0F343 0.499 0.499 1.491 0.655 0.39 7.66 1.67 1% AEP, 15m hburd, Store 0F343 0.499 0.499 1.491 0.655 0.39 7.66 1.67 1% AEP, 15m hburd, Store 0F345 0.255 0.256 0.39 7.68 1.67 1% AEP, 15m hburd, Store 0F363 0 0 0 0 0 0 0 0F363 0 0 0.1347 0 0 0 0<								
OF226 1.224 1.234 1.234 0.532 0.11 0.67 4.91 2.48 1% AEP, 9 hour burk, Sten OF334 OF334 0.759 0.759 1.115 0.043 0.11 10.95 2.9 1% AEP, 3 hour burk, Sten OF336 OF336 0.466 1.337 0 0 0 0 OF341 0 0 1.337 0 0 0 0 OF343 0.467 1.337 0 0 0 0 0 OF343 0.468 0.469 0.459 0.655 0.39 7.6 1.71 1% AEP, 16 min burs, Stor OF345 0.258 0.258 0.258 0.258 0.40 0 0 0 OF363 0 0 0.766 0 0 0 0 0 0 OF363 0 0 0 0.252 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444 0.444								
OF33 0.497 0.497 1.456 0.352 0.17 4 3.21 1% AEP, 9 how burk, Skor OF33 0.406 0.406 1.559 0.228 0.14 4 2.31 1% AEP, 9 how burk, Skor OF33 0.406 0.406 1.539 0 0 0 OF34 0.409 0.409 0.60 0 0 0 OF34 0.228 0.14 4 2.31 1% AEP, 15 min burk, Skor 0 OF43 0.255 0.255 0.256 0.059 0.26 7.31 1.65 1% AEP, 2 how burk, Skor OF43 0.255 0.255 0.255 0 0 0 0 0 OF33 0 0 0.756 0 0 0 0 0 0 OF36 0 0 0.522 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0								
OF34 0.759 0.759 0.115 0.043 0.11 10.95 2.9 1% AEP, 30 mb burs, Stor OF33 0 0 1.333 0 0 0 0 OF34 0 0 1.337 0 0 0 0 OF341 0 0 1.559 0 0 0 0 OF343 0.498 0.449 1.411 0.655 0.39 7.86 1.187 1% AEP, 2 how bard, Stor OF345 0.258 1.266 0.609 0 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>								
OF330 0.406 1.333 0.228 0.14 4 2.31 [% AEP, 15 min burs, Stor OF341 0								
O F339 0 0 1 337 0 0 0 O F341 0 0 1 559 0 0 0 0 0 O F343 0.499 0.499 1.491 0.655 0.39 7.86 1.87 1% AEP, 15 min burst, Stor O F345 0.255 0.255 0.256 0.256 7.81 1.58 1% AEP, 2 hour burst, Stor O F360 0 0 1.342 0 0 0 0 0 O F363 0 0 7.86 0								
OF341 0 0 1.599 0								
OF33 0.499 0.499 1.491 0.655 0.39 7.86 1.87 1% AEP, 15 nm burst. Stor OF351 0 0 1.347 0 0 0 0 OF363 0 0 1.343 0 0 0 0 OF363 0 0 1.343 0 0 0 0 OF363 0 0 1.755 0 0 0 0 OF365 0 0 1.125 0 0 0 0 OF366 0 0 0.551 0 0 0 0 OF369 0 0 0.551 0 0 0 0 0 OF526 0.464 0.649 0.639 0.45 2.24 1.66 1% AEP, 30 min burst. Stor OF5303 0 0 0 0 0 0 0 0 OF5403 0 0.494 0.28 0.45<								
OF345 0.255 0.255 1.266 0.609 0.26 7.31 1.58 1% AEP, 2 hour burst. Stor OF350 0 0 1.343 0 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
OF351 0 0 1.347 0 0 0 0 OF360 0 0 1.347 0 0 0 0 OF363 0 0 0.766 0 0 0 0 OF365 0 0 1.125 0 0 0 0 OF369 0 0 0.581 0 0 0 0 0 OF566 0.484 0.484 1639 0.28 0.45 2.24 1.66 1% AEP, 30 min burst. Stor OF5303 0 0 0 1.291 0 0 0 0 0 DETENTION BASIN DETAILS								1.87 1% AEP, 15 min burst, Storm 1
OF380 0 0 1.343 0 0 0 0 OF383 0 0 0.768 0 0 0 0 0 OF385 0 0 0.551 0 0 0 0 0 OF399 0 0 0.551 0 0 0 0 OF530 0.484 0.489 0.28 0.451 2.24 1.66 1% AEP. 30 min burst. Stor OF5303 0 <t< td=""><td>OF345</td><td>0.255</td><td>0.255</td><td>1.266</td><td>0.609</td><td>0.26</td><td>7.31</td><td>1.58 1% AEP, 2 hour burst, Storm 3</td></t<>	OF345	0.255	0.255	1.266	0.609	0.26	7.31	1.58 1% AEP, 2 hour burst, Storm 3
OF380 0 0 1.343 0 0 0 0 OF383 0 0 0.768 0 0 0 0 0 OF385 0 0 0.551 0 0 0 0 0 OF399 0 0 0.551 0 0 0 0 OF530 0.484 0.489 0.28 0.451 2.24 1.66 1% AEP. 30 min burst. Stor OF5303 0 <t< td=""><td>OF351</td><td>0</td><td>0</td><td>1.347</td><td>0</td><td>0</td><td>0</td><td>0</td></t<>	OF351	0	0	1.347	0	0	0	0
OP365 O 1125 O O O O OP369 0 0 0.531 0 0 0 0 OP369 0 0.484 0.483 0.28 0.45 2.24 1.66 1% AEP, 30 min burst, Stor OP536 0.484 0.484 1.639 0.28 0.45 2.24 1.66 1% AEP, 30 min burst, Stor OP53403 0 0 1.291 0 0 0 0 0 OP53403 0 0 1.291 0 0 0 0 0 0 OP53403 0 0.484 1.639 0.28 0.445 0.012 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0.77 0 0.784 0.714 0 0.744 0.77 0.784 0 0.784 0.784 0 0 0 0 0 0 0		0	0	1.343	0	0	0	0
OF365 0 0 1125 0 0 0 0 OF367 0 0 0.531 0 0 0 0 0 OF369 0.484 1.639 0.28 0.451 2.24 1.66 1% AEP. 30 min burst, Stor OF536 0.484 0.39 0.28 0.45 2.24 1.66 1% AEP. 30 min burst, Stor OF536 0.484 0.483 0.28 0.45 2.24 1.66 1% AEP. 30 min burst, Stor OF537 0 0 0 0 0 0 0 OF53403 0 0 1.291 0 0 0 0 OF536 0.484 1.639 0.28 0.28 0.28 0.28 0 0 0 0 DETENTION BASIN DETAILS Item Item 2 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.07 0.024 0.07<								
OF367 0 0 0.582 0 0 0 0 OF369 0 0.484 0.484 1.639 0.28 0.45 2.24 1.66 1% AEP, 30 min burst, Stor OF53603 0 0 1.291 0		0						
OF369 0 0 0.531 0								
OF526 0.484 0.484 1.639 0.28 0.45 2.24 1.661 % AEP, 30 min burst, Stor OF53403 0								
OF53403 0 0 1.291 0 0 0 0 DETENTION BASIN DETAILS <								
DETENTION BASIN DETAILS Max WL MaxVol MaxQ MaxQ <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>								
Name Max WL Max QL Max Q Max Q <t< td=""><td>01 00400</td><td>- · ·</td><td>l .</td><td>1.201</td><td>- °</td><td></td><td>0</td><td>0</td></t<>	01 00400	- · ·	l .	1.201	- °		0	0
Name Max WL Max Q Max Q <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>								
Name Max WL Max Q Max Q <th< td=""><td>DETENTION PASIN DETAILS</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	DETENTION PASIN DETAILS							
Total Total Work High Level EAST-B2 57.65 0 0.254 0.241 0.012 EAST-B5 67.23 0 0.494 0.07 0.074 EAST-B6 61.61 0 1.387 0.552 0.794 0.074 EAST-B6 61.61 0 1.387 0.552 0.794 0.012 0.012 EAST-B6 61.61 0 0.255 0 0 0.014 0.011		Max M/I	MaxVal	May O	May O	May O		
EAST-B2 57.65 0 0.254 0.241 0.012 EAST-B5 67.23 0 0.494 0.424 0.07 EAST-B6 61.61 0 1.387 0.592 0.794 EAST-86 61.61 0 1.387 0.592 0.794 EAST-89 63.65 0 0.255 0 0 EAST-87 65.97 0 1.199 0.663 0.535 EAST-81 59.06 0 0.496 0.098 0 Bio-retention 73.19 0 0 0 0 EAST-83 70.75 0 0.281 0.291 0.09 EAST-84 71.41 0 0.201 0 0 0 EAST-83 70.75 0 0.281 0.241 0.04 0 EAST-83 70.75 0 0.281 0.241 0.04 0 0 Bio-retention 70.75 0 0.281 0.241 <t< td=""><td>Inallie</td><td>IVIAN VVL</td><td>IVIAAVOI</td><td></td><td></td><td></td><td></td><td></td></t<>	Inallie	IVIAN VVL	IVIAAVOI					
EAST-B5 67.23 0 0.494 0.07 EAST-B6 61.61 0 1.387 0.592 0.794 EAST-B6 61.61 0 0.255 0.255 0 0 EAST-B0 63.65 0 0.255 0.255 0 0 EAST-B1 59.06 0 0.464 0.45 0.014 0 EAST-B7 65.97 0 1.199 0.663 0.355 0 0 EAST-B10 62.52 0 0.596 0.496 0.098 0	EAST R2	E7.65	-					
EAST-86 61.61 0 1.387 0.592 0.794 EAST-88 71.04 0 0.024 0 0 EAST-89 63.65 0 0.255 0 0 EAST-81 59.06 0 4.46 0.014 0 EAST-87 65.97 0 1.199 0.663 0.355 EAST-810 62.52 0 0.996 0.098 Bio-retention 73.19 0 0 0 0 EAST-83 70.75 0 0.241 0.04 0 0 EAST-83 70.75 0 0.241 0.04 0 0 0 Run Log for 12546218 AlbanyMotorPark east run at 03.50.40 on 13/7/2021 using version 2020.036 1 1 1 0.241 0.04 1								
EAST-88 71.04 0 0.024 0 EAST-89 63.65 0 0.255 0.255 0 EAST-81 59.06 0 0.484 0.45 0.014 EAST-81 59.06 0 0.484 0.45 0.014 EAST-817 65.97 0 1.199 0.663 0.535 EAST-810 62.52 0 0.595 0.486 0.008 Bio-retention 73.19 0 0 0 0 EAST-813 70.75 0 0.281 0.241 0.04 Run Log for 12546218 AlbanyMotorPark east run at 03:50:40 on 13/7/2021 using version 2020.036								
EAST-89 63.65 0 2.255 0 EAST-81 59.06 0 0.464 0.45 0.014 EAST-87 65.97 0 1.199 0.663 0.535 EAST-810 62.52 0 0.595 0.466 0.098 Bio-retention 73.19 0 0 0 0 EAST-83 77.5 0 0.201 0.046 0.046 Run Log for 12546218 AlbanyMotorPark east run at 03:50:40 on 13/7/2021 using version 2020.036 0.241 0.04 0 B10-return unat 03:50:40 on 13/7/2021 using version 2020.036 0 0 0 0 B10-03 The maximum water level in these storages exceeds the maximum elevation you specified: EAST-B10, EAST-B6. DRAINS has extrapolated the Elevation vs Storage table to a higher Elevation. Please provide accurate values for higher elevations. No water upwelling from any pit. No Freeboard was less than 0.15m at Pit1448, Pit1296 0 0 0 0 Peak water levels spilled in these overflow Routes: OF324 spilled. You cannot rely on these results. You really MUST specify data for higher levels for these cross sections. 0 0 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
EAST-B1 59.06 0 0.464 0.45 0.014 EAST-B7 65.97 0 1.199 0.663 0.535 EAST-B10 62.52 0 0.595 0.496 0.098 Bio-retention 73.19 0 0 0 0 EAST-B4 71.41 0 0.201 0 0 EAST-B3 70.75 0 0.241 0.04 0 Run Log for 12546218 AlbanyMotorPark east run at 03.50.40 on 13/7/2021 using version 2020.036 0 0 0 0 F00-03 The maximum water level in these storages exceeds the maximum elevation you specified: EAST-B10. EAST-B6. 0 0 DANNs has extrapolated the Elevation vs Storage table to a higher Elevation. Please provide accurate values for higher elevations. 0 0 0 No water upwelling from any pit. Freeboard was less than 0.15m at Pit148, Pit1296 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 </td <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
EAST-B7 65.97 0 1.199 0.663 0.535 EAST-B10 62.52 0 0.595 0.496 0.098 Bio-retention 73.19 0 0 0 0 EAST-B4 71.41 0 0.201 0 0 EAST-B3 70.75 0 0.241 0.04 0 Run Log for 12546218 AlbanyMotorPark east run at 03:50:40 on 13/7/2021 using version 2020.036 0 0 0 B10-04 0 0 0.241 0.04 0 0 B10-05 0 13/7/2021 using version 2020.036 0 0 0 0 B10-03 The maximum water level in these storages exceeds the maximum elevation you specified: EAST-B10, EAST-B6. 0								
EAST-B10 62.52 0 0.965 0.496 0.098 Bio-retention 73.19 0								
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Figure G.2 East-1 schematic diagram

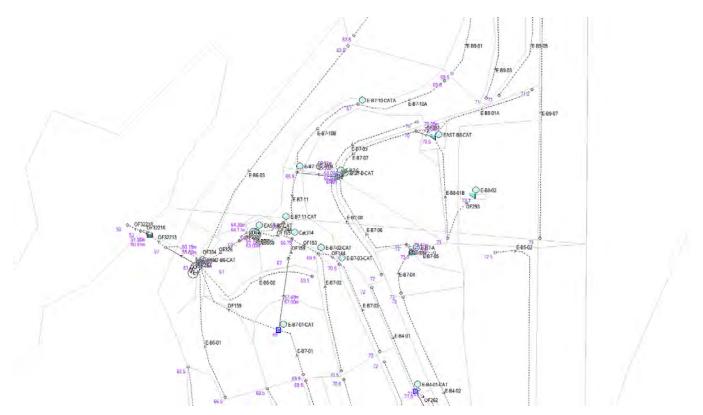


Figure G.3 East-2 schematic diagram

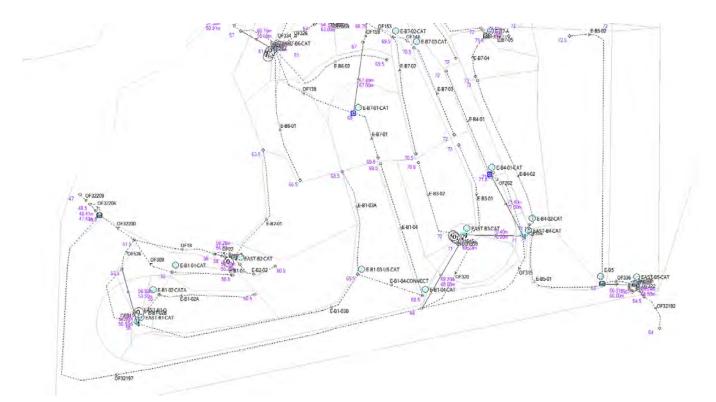


Figure G.4 East-3 and East-4 schematic diagram

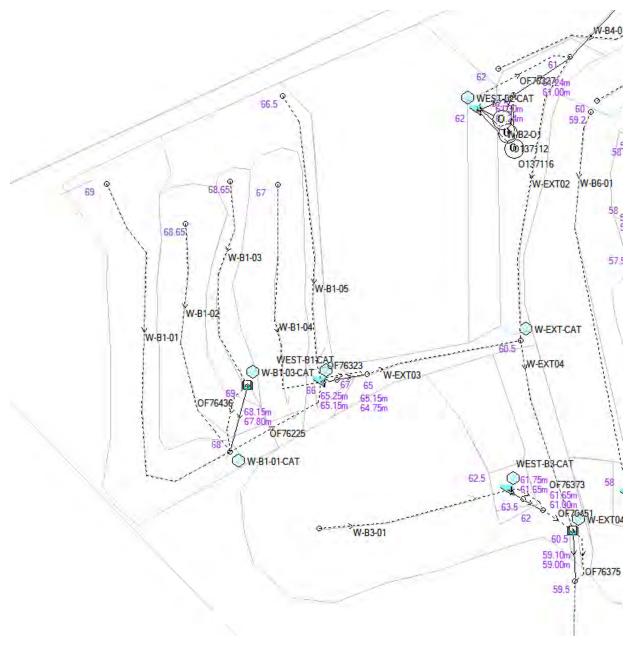


Figure G.5 West-3 schematic diagram

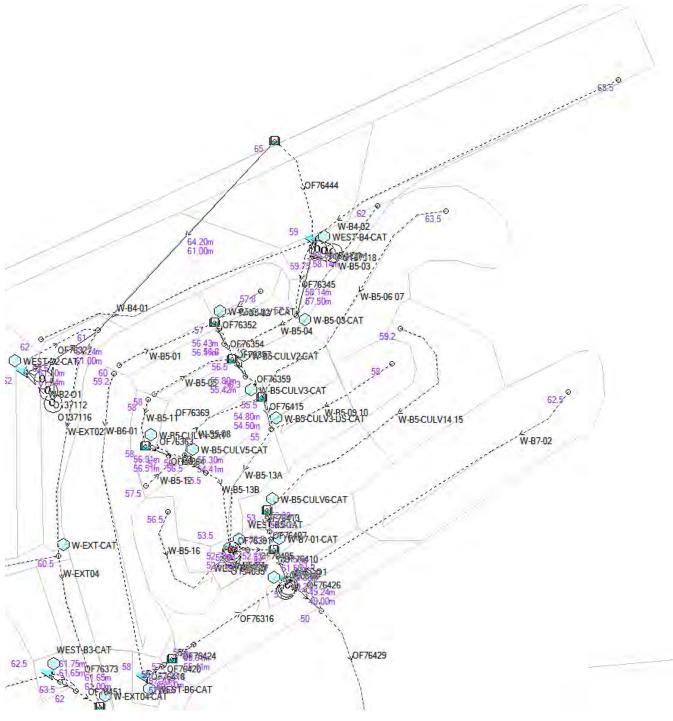
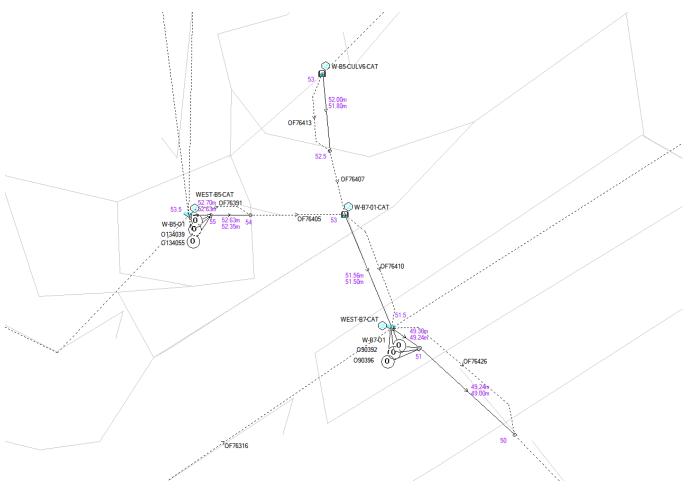


Figure G.6 West-2 schematic diagram





Appendix H Site and soil evaluation for onsite

Site and soil evaluation for onsit wastewater management

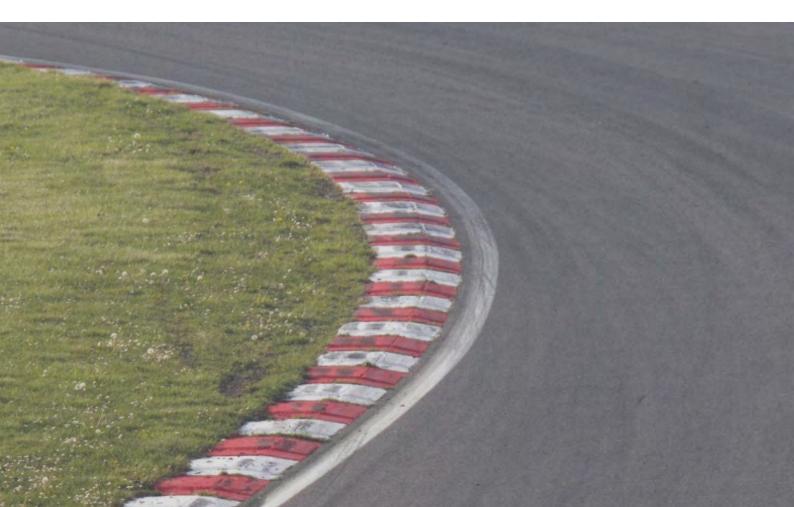


Albany Motorsport Park – Development Application

Site and Soil Evaluation for Onsite Wastewater Management

City of Albany 19 August 2021

→ The Power of Commitment



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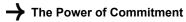
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Last saved date	19 August 2021
File name	https://projectsportal.ghd.com/sites/pp18_05/albanymotorsportpark/ProjectDocs/Effluent Disposal Investigation/12546218-REP-A_SSE report.docx
Author	Jeff Foley/ Vicki Davies
Project manager	Vicki Davies
Client name	City of Albany
Project name	Albany Motorsport Park - Development Application
Document title	Albany Motorsport Park – Development Application Site and Soil Evaluation for Onsite Wastewater Management
Revision version	0
Project number	12546218

Document status

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S4	0	J. Foley/ V. Davies	J. Foley	1.11 A	J. Foley	1.11 A.	19.08.21		
				11.0					
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Executive summary

The City of Albany (CoA) has engaged GHD to prepare a Site and Soil Evaluation for Onsite Wastewater Management report for the staged construction of the Albany Motorsport Park (AMP) at Lot 5780 (No. 54) Down Road South, Drome (the Site) (Figure 1, Appendix A). The project Proponent is the Great Southern Motorplex Group Inc. (GSMG).

Due to the scale and nature of the proposed development, the works have been broken down into two key stages which comprise the following:

- Stage 1:
 - Stage 1A: Construction of motocross track and 4WD driver training, ATV area and associated infrastructure.
 - Stage 1B: Construction of racetrack and associated infrastructure (subject to funding).
- Future Development: Construction and replacement of final permanent structures to support the function of the motorsports complex (subject to funding). Stage 2 will be addressed as a separate Development Application.

This Site and Soil Evaluation for Onsite Wastewater Management report has been developed as per the Department of Health, Western Australia (DOHWA) template report based on the *Health (Treatment of Sewage and Disposal of Effluent and Liquid Waste) Regulations 1974*, Government Sewerage Policy 2019, State Planning Policy 2.9, AS/NZS 1547 and other supporting documentation (DOHWA, 2021).

The purpose of this Site and Soil Evaluation (SSE) report is to outline the site, soil and groundwater conditions at the proposed AMP site with regarding to suitability for onsite effluent disposal during operation of the AMP. This report provides supporting information for the Development Application for the Stage 1 of the Site.

Based on an assessment of the soil physical and chemical results for the six test pit locations, it is recommended that the LAAs for the Race Track Precinct and Motocross Precinct are located at TP01 and TP06, respectively. The sizing for a wastewater treatment system and LAA has been developed in this SSE report for Stage 1A in the Motocross Precinct only.

The proposed clubhouse within the Motocross Precinct will be constructed in Stage 1A of the development. It is anticipated that this will be an unlicenced facility (15 L/ person/ day) however provision has been made for anticipated wastewater volumes for a licenced facility (35 L/ person/ day), to allow for possible increased loading at the site if it were to become a licenced facility.

The Motocross Precinct clubhouse is expected to have intermittent use throughout the Motocross season and on a weekly basis, with up to 300 patrons on Sunday or Saturday followed by minimal usage during the week and off-season downtime. Therefore, for the purpose of calculating anticipated wastewater volumes it is assumed that there is an average of 100 people/ day.

In order to accommodate spikes in wastewater volumes on event days when there is up to 300 patrons using the Motocross Precinct clubhouse facilities, it is proposed to install a 15,000 L holding tank, to balance storage over the course of a typical week.

The results of a water balance for the Motocross Precinct, for an average of 100 persons/day, indicate that 1,100 m² will be required for the sub-soil irrigation area. There is adequate area of land available within the vicinity of TP01 to accommodate the site of the required LAA.

As per the requirements of the Department of Water *WQPN 100* (DoW, 2007) and the *Government Sewerage Policy* (DPLH, 2019) a 'Secondary' wastewater treatment plant, with engineering certification to meet effluent quality of Biological Oxygen Demand (BOD) < 20 mg/L; Total Suspended Solids (TSS) < 30 mg/L; Total Nitrogen (TN) < 10 mg/L; Total Phosphorus (TP) < 1 mg/L; and *Escherichia coli* < 10 cfu/100mL is required in a Priority 2 PDWSA.

It is recommended that a DOHWA approved 'Secondary' treatment system, certified to AS1546.3:2008, is selected and installed for the Motocross Precinct during Stage 1A of development.

At time of writing, an onsite effluent disposal system was not proposed to be installed in the Race Track Precinct. All liquid waste from transportable buildings, toilets and washdown facilities is proposed to be removed offsite, as required, by an approved contractor. If onsite effluent disposal is proposed in the future is it expected a similar system, with holding tank, will be utilised to manage spikes in wastewater volumes for events and off-season downtime.

This report is subject to, and must be read in conjunction with, the limitations set out in section 1.2 and the assumptions and qualifications contained throughout the Report.

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1. Introduction

1.1 Background

The City of Albany (CoA) has engaged GHD to prepare a Site and Soil Evaluation for Onsite Wastewater Management report for the staged construction of the Albany Motorsport Park (AMP) at Lot 5780 (No. 54) Down Road South, Drome (the Site) (Figure 1, Appendix A). The project Proponent is the Great Southern Motorplex Group Inc. (GSMG).

The Great Southern Motorplex Group Inc. (GSMG), the Proponent, in partnership with the City of Albany, intend to develop the site as a regional motorsport facility. In October 2018, the City of Albany Council resolved to purchase the site and settlement of the land purchase was concluded in 2019. Once constructed, the AMP will be operated and managed by Albany Motorsport Venue Incorporated (AMV Inc.).

The proposed AMP forms part of the CoA's strategy to expand upon its existing motorsports facilities within the greater Albany area. The AMP is to be the largest facility of its kind in Western Australia and will support the local economy.

1.2 Purpose of this report

This Site and Soil Evaluation for Onsite Wastewater Management report has been developed as per the Department of Health, Western Australia (DOHWA) template report based on the *Health (Treatment of Sewage and Disposal of Effluent and Liquid Waste) Regulations 1974*, Government Sewerage Policy 2019, State Planning Policy 2.9, AS/NZS 1547 and other supporting documentation (DOHWA, 2021).

The purpose of this Site and Soil Evaluation (SSE) report is to outline the site, soil and groundwater conditions at the proposed AMP site with regarding to suitability for onsite effluent disposal during operation of the AMP. This report provides supporting information for the Development Application for the Stage 1 of the Site.

1.3 Evaluator's qualifications, experience and professional indemnity

The SSE has been undertaken by Dr Jeff Foley who is a Chemical Engineer with 20 years' technical experience specialising in the areas of wastewater treatment and recycling and integrated water management. His involvement in water cycle projects has ranged from policy and planning, concept design and process modelling, through to detailed design, construction, commissioning and process optimisation.

GHD's site evaluation has been supported in the field by Great Southern Geotechnics (GSG), who specialise in high-quality testing of construction materials and consultancy services to the civil construction, agriculture, environmental, mining and resources industries across WA's Great Southern region. GSG operates an independent NATA Accredited Construction Materials Testing Laboratory, in compliance with AS ISO/IEC 17025 and ISO 9001.

Dr Foley is suitably qualified to provide interpretation of site, soil and climate conditions, undertake water balances, selection and design of appropriate wastewater treatment systems, disposal and reuse options. A summary of the Dr Foley's site evaluator details has been provided in Table 1 and a copy of his CV and qualifications can be provided on request.

A copy of GHD's Professional Indemnity Insurance certificate is included in Appendix C.

Table 1 Site Evaluator Details

Site evaluator details	
Name	Dr Jeff Foley, Technical Director – Wastewater process engineering
Company	GHD Pty Ltd
Phone	(08) 9840 5101
Email	Jeff.Foley@ghd.com
Qualification	MIEAust, BE(Chem) (Hons I), BA, PhD (UQ) - Life cycle assessment of
Knowledge, skills and practical experience	wastewater treatment systems
	Employed as a wastewater process designer (inc. on-site systems) by GHD 2001 – 2021.
Date of site assessment	16/08/2021
Signature	2.11 A
Date	19.08.202/1

1.4 Scope and limitations

This report: has been prepared by GHD for City of Albany and may only be used and relied on by City of Albany for the purpose agreed between GHD and City of Albany as set out in section 1.2 of this report.

GHD otherwise disclaims responsibility to any person other than City of Albany arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.

The opinions, conclusions and any recommendations in this report are based on information obtained from, and testing undertaken at or in connection with, specific sample points. Site conditions at other parts of the site may be different from the site conditions found at the specific sample points.

Investigations undertaken in respect of this report are constrained by the particular site conditions, such as the location of buildings, services and vegetation. As a result, not all relevant site features and conditions may have been identified in this report.

Site conditions (including the presence of hazardous substances and/or site contamination) may change after the date of this Report. GHD does not accept responsibility arising from, or in connection with, any change to the site conditions. GHD is also not responsible for updating this report if the site conditions change.

GHD has prepared this report on the basis of information provided by City of Albany and others who provided information to GHD (including Government authorities), which GHD has not independently verified or checked beyond the agreed scope of work. GHD does not accept liability in connection with such unverified information, including errors and omissions in the report which were caused by errors or omissions in that information.

2. Site development description

The AMP is proposed to be developed at Lot 5780 Down Road South, Drome which is located approximately 20 km to the north of the Albany CBD and is 192.34 ha in size. The AMP comprises 141.7 ha (including 0.2 ha for crossovers) in the eastern portion of the Site. Two areas within Lot 5780 are excluded from the AMP development and include 49.47 ha at the western end of the Site which is covered with native vegetation and a dam area (1.37 ha) on the northern boundary which is subleased to Plantation Energy.

The Site is zoned as 'Special Use – SU26' under Local Planning Scheme No. 1, Scheme Amendment No. 35.

At full development, the proposed AMP will consist of:

- Sealed, configurable multi-use track (3.5 km long × 12 m wide) for motor car racing, motorcycle racing, drifting, driver training and cycling:
 - Designed to comply with Motorsport Australia Track Operator's Safety Guide (CAMS, 2012) and Motorcycling Australia (MA) Track Guidelines (MA, 2011)
 - To be licensed by Motorsport Australia for Fédération Internationalé de l'Automobile (FIA) Grade 2 and Fédération Internationalé Motocyclisme (FIM) Grade B (i.e. up to second-tier international motor racing)
- A motocross circuit designed and constructed in association with MA guidelines.
- An off-road four-wheel drive (4WD) and all-terrain vehicle (ATV) training area.
- Associated buildings and infrastructure.

2.1 Staging of the development

Due to the scale and nature of the proposed development, the works have been broken down into two key stages which comprise the following:

- Stage 1:
 - Stage 1A: Construction of motocross track and 4WD driver training, ATV area and associated infrastructure.
 - Stage 1B: Construction of racetrack and associated infrastructure (subject to funding).
- Future Development: Construction and replacement of final permanent structures to support the function of the motorsports complex (subject to funding). Stage 2 will be addressed as a separate Development Application.

A Master Plan, which illustrates the various aspects of the Site and staging areas, has been developed by the GSMG and CoA to support the Development Application for the AMP (Figure 2, Appendix A).

2.2 Anticipated wastewater volumes

The proposed clubhouse within the Motocross Precinct will be constructed in Stage 1A of the development. It is anticipated that this will initially be an unlicenced facility (15 L/ person/ day) however provision has been made for anticipated wastewater volumes for a licenced facility (35 L/ person/ day), to allow for possible increased loading at the site if it were to become a licenced facility.

The Motocross Precinct clubhouse is expected to have intermittent use throughout the Motocross season (approx. March to October) and on a weekly basis, with up to 300 patrons on Sunday or Saturday followed by minimal usage (max. 20 persons per day) during the week and off-season downtime. Therefore, for the purpose of calculating anticipated wastewater volumes (Table 2) it is assumed that there is an <u>average</u> of 100 people/ day (Appendix B).

In order to accommodate spikes in wastewater volumes on event days when there is up to 300 patrons using the Motocross Precinct clubhouse facilities, it is proposed to install a 15,000 L holding tank, to balance out wastewater flows over the course of a typical week. The holding tank will also help store effluent during the off-season period.

At this stage, an onsite effluent disposal system is not proposed to be installed in the Race Track Precinct. All liquid waste from transportable buildings, toilets and washdown facilities is proposed to be removed offsite, as required, by an approved contractor. If onsite effluent disposal is proposed in the future is it expected a similar system, with holding tank, will be utilised to manage spikes in wastewater volumes for events and off-season downtime.

Table 2	Anticipated wastewater volumes
---------	--------------------------------

Туре	Daily flow (L/day)			
Stage 1A – Motocross Precinct				
Permanent building (5 x sinks, 4 x toilet pans, urinal)	Up to 300 persons (average 100 persons/day)	35 L/person/day	3,500 L/day (average)	
Transportable toilets	One permanent block and additional transportables for special events	35 L/person/day	Liquid waste to be removed offsite by an approved contractor, as	
Washdown area	Variable	-	required	
Total			3,500 L/day (average)	
Stage 1B – Racetrack Precinct				
Transportable building	500 persons	35 L/person/day	Liquid waste to be removed offsite by an approved contractor, as	
Transportable toilets	Special events	35 L/person/day		
Washdown area	Variable	-	required	
Total				

2.3 Site development description

The AMP site development description is outlined in Table 3.

Table 3	Description of the development
Table 3	Description of the development

Development characteristic	Description									
Site address	Lot 5780 (No. 54) Down Road South, Drome									
Owner/ developer	City of Albany	City of Albany								
Proponent	Great Southern Motor	Great Southern Motorplex Group (GSMG)								
Postal address	PO Box 484, ALBANY	WA 6331								
Contact for SSE	Ph: 9840 5101	Ph: 9840 5101 Mob: 0410 541 971 Email: jeff.foley@ghd.com								
Date of field work	25 June 2021									
Local Government	City of Albany									
Zoning	Special Use	Special Use								
Lot size	192.34 ha	192.34 ha								
Proposal	Albany Motorsport Par	ĸ								
Water supply	Bore and rainwater									
Availability of sewer	Unavailable									
Development located within:	Public drinking water source area:Sewage sensitive areasYes – Priority 2 PDWSAYes – Sewerage Category (f) Within 1 km of significant wetlands									
Anticipated wastewater volume:	Sewage (L): Motocross Precinct 3,500 L/day (average)									

3. Site and soil assessment

3.1 Site assessment

GHD have undertaken a number of site walkovers for the AMP site from 2018 to 2021 and are very familiar with the existing site conditions. In addition, an intrusive field investigation was undertaken, by Great Southern Geotechnics, on 25 June 2021. This investigation involved excavating six test pits to a depth of 2500 mm below ground level (bgl), using a mini excavator with a 300 mm auger. Soil types, profiles and groundwater levels were then visually assessed and recorded onsite at time of site investigation, as per the DOHWA (2021) SSE template guidelines (Great Southern Geotechnics, 2021).

The findings of the desktop and field assessment, level of constraint and proposed mitigation measures, for the proposed Motocross Precinct and Race Track Precinct onsite effluent disposal locations, have been summarised in Table 4.

Site characteristics	Investigations and reporting												Level of constraint	Mitigation measures	
Climate	 Albany is located on the south coast of Western Australia and the climate is broadly described as Mediterranean, with warm dry summers and mild wet winters. The nearest Bureau of Meteorology (BoM) official recording station that has mean daily evaporation data (1968 to 2012) is the Albany Airport Comparison weather station (Site number 9741) (BoM, 2021). Mean monthly rainfall levels at the Albany Airport Comparison weather station (BoM, 2021) and pan evaporation data (DPIRD, 1987) are presented below. This shows that mean monthly evaporation exceeds mean monthly rainfall for seven months of the year, from November to April. 									High	Divert stormwater from upslope around sub- soil irrigation area				
	Month	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec		
	Mean Rainfall (mm)	23.6	22.3	33.6	61.3	89.8	108.0	119.3	106.3	88.5	70.8	47.0	27.8		
	Evap. (mm)	220	171	150	91	63	47	49	67	84	106	150	199		
	Evap. Exceeds Rainfall	Yes	Yes	Yes	Yes	No	No	No	No	No	Yes	Yes	Yes		
Exposure	The propos						Race Tra	ck and Mc	otocross P	recincts ł	nave a hi	gh expos	ure to	Nil to Low	Not required

 Table 4
 Key site characteristics, level of constraint and proposed mitigation measures for the proposed Motocross Precinct and Race Track Precinct effluent disposal areas

Site characteristics	Investigations and reporting	Level of constraint	Mitigation measures
Vegetation	The majority of the Site has been previously cleared for agriculture with isolated stands of trees (112.9 ha). The proposed Land Application Area (LAA) is open grassland. Refer to site photographs in the Great Southern Geotechnics (2021) Site Investigation report (Appendix D).	Nil to Low	Maintain grassed area within the LAA
Landform and drainage	 The Site is mapped as the following Department of Primary Industries and Regional Development (DPIRD) landscape mapping units (Figure 3, Appendix A): TP01-TP03 – 242KgDMc Sands on laterite on elongate crests. TP04-TP05 – 242ReDMc Sands on laterite on elongate crests. TP06 – Broad valleys in sedimentary in sedimentary rocks; 30 m relief, smooth slopes. Deep sands and iron podzols on slopes. 		Not required
Slope	Slope of land within the site investigation areas for the Race Track Precinct and Motocross Precinct is approximately 6% (Figure 4, Appendix A).	Nil to Low	Diversion of stormwater from upslope around sub- soil irrigation area proposed
Fill (imported)	No imported fill was encountered during the site investigation	Nil to Low	Not required
Surface gravel and rock outcrops	During the Site Investigation, the soil profile (to 2500 mm blg) was generally found to have Topsoil over Sandy GRAVEL over Sandy CLAY. No rock outcrops were observed within the test pit location areas and gravel soils had approximately 10% coarse fragments (Great Southern Geotechnics, 2021)		Not required
Erosion potential	The water erosion risk mapped by DPIRD indicates that for test pit locations TP01 – TP05 "<3% of map unit has a high to extreme water erosion risk". TP06 is mapped as "3-10% of map unit has a high to extreme water erosion risk" (Figure 5, Appendix A). The test pit locations within the Site are currently grassed and considered likely to be Nil or low if sub-soil irrigation is installed and grassed surface is maintained. Refer to photos in the Site Investigation report (Appendix D).	Nil to Low	Maintain as grassed area and divert stormwater from upslope around sub- soil irrigation area to maintain Nil or Low risk rating
Separation from groundwater	During the Site Investigation, undertaken in late June (Appendix D), ground water was not intercepted at 2500 mm bgl at any of the six test pit locations (Figure 4, Appendix A). These locations meet the vertical separation of greater than 2 m separation to groundwater in PDWSA.	Nil to Low	Not required
Public Drinking Water Source Area (PDWSA) and Sewage Sensitive Area (SSA)	The Site is located in a Priority 2 PDWSA – Marbellup Brook Catchment Area and SSA (<1 km from conservation category wetland) (Figure <mark>4</mark> , Appendix A).	High	Maintain >2 m vertical separation to groundwater

Site characteristics	Investigations and reporting	Level of constraint	Mitigation measures
Surface waters and separation from water resources	All sub-soil irrigation areas will be located >100 m to Protected Exclusion Area and Marbelup Flats (Conservation Class wetland) (Figure 3, Appendix A).	Nil to Low	Not required
Rainfall run-off and seepage	The test pit location areas, in both the Race Track Precinct and Motocross Precinct, are located on waxing upperslope (UX) (National Committee on Soil and Terrain, 2009). No evidence of evidence of water pooling on the surface or seepage was observed during the Site Investigation (Great Southern Geotechnics, 2021) or during site walkovers undertaken by GHD.	Nil to Low	Diversion of stormwater from upslope around sub- soil irrigation area proposed
Flood potential	The flood erosion risk mapped by DPIRD indicates that test pit locations TP01 – TP05 that "<3% of map unit has a moderate to high flood risk". TP06 is mapped as "3-10% of map unit has a moderate to high flood risk" (Figure 9, Appendix A).	Nil to Low	Not required
Horizontal setback distances	All sub-soil irrigation areas will be setback >100 m to site boundaries, Protected Exclusion Area and Marbelup Flats (Conservation Class wetland) (Figure 3, Appendix A).	Nil to Low	Not required
Available Land Application Area (LAA)	Sufficient land is available within the Race Track and Motocross Precinct area for sub-soil irrigation of wastewater.	Nil to Low	Not required

3.2 Soil assessment

During the Site Investigation, undertaken by Great Southern Geotechnics, three test pits were excavated in each of the Motocross Track Area and Race Track Area. Table 5 includes a summary of the soil physical and chemical characteristics (Appendix E) for SSE at the six test pit locations.

Location	Layer depth	Sample depth	Soil strata	Depth to GW	Coarse fragments (%)	Soil colour & mottling	Soil field texture	Soil structure	Indicative soil permeability	Design loading Trenches and b	rate (DLR) (mr eds	n/d)	pH EC (dS/m)	EC (dS/m)		Phosphate Sorption
	(mm)	(mm)							(m/d) (<i>K</i> sa ⁻¹)	Primary treated	effluent	Secondary	1		(%)	Capacity (mg P
			Conservative rate	Maximum rate	treated effluent				sorbed/kg)							
Race Track	<pre></pre>															
TP01	0-180		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP01	180- 490		Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 250 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub- angular, (F:20% / M:20% / C:15%)	Structureless	>3.0	20	35	50	-	-	-	-
TP01	550- 2500	900- 1100	Sandy CLAY	•	NA	Brown/red mottled Light brown/orange (40%)	Light Clay - Low to medium plasticity	Massive	<0.06	NA	NA	8	6.1	0.022	5.8	688
TP02	0-140		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP02	140- 400		Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Moderately cemented - Fine to coarse, sub-rounded to sub-angular, (F:20% / M:20% / C:15%)	Structureless	>3.0	20	35	50	-	-	-	-
TP02	400- 1400	500-900	Sandy CLAY		NA	Light brown	Low to medium plasticity	Massive	<0.06	NA	NA	8	6.1	0.025	4.8	1650
TP02	1400- 2500		Sandy CLAY		NA	Brown/red mottled Light brown/orange (40%)	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP03	0-250		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey to grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP03	250- 830	300-600	Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to medium, sub-rounded to sub-angular, (F:30% / M:30%)	Structureless	>3.0	20	35	50	5.7	0.028	5.7	3660
TP03	830- 1600		Sandy CLAY		NA	Light brown	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP03	1600- 2500		Sandy CLAY		NA	Brown/red mottled Light brown/grey (30%)	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-

Table 5 Summary of soil physical and chemical characteristics for SSE of the AMP site

Location	Layer depth	Sample depth	Soil strata	Depth to GW	Coarse fragments (%)	Soil colour & mottling	Soil field texture	Soil structure	Indicative soil permeability	Design loading Trenches and b	rate (DLR) (mn eds	n/d)	pH	EC (dS/m)	Sodicity (ESP)	Phosphate Sorption
	(mm)	(mm)							(m/d) (<i>K</i> sa ⁻¹)	Primary treated	effluent	Secondary	1		(%)	Capacity (mg P
										Conservative rate	Maximum rate	treated effluent				sorbed/kg)
Motocross	Precinct															
TP04	0-220		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP04	220- 1250	400-800	Sandy GRAVEL	-	Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub- angular, (F:25% / M:20% / C:10%)	Structureless	>3.0	20	35	50	5.8	0.028	6.2	3000
TP04	1250- 1750		Sandy CLAY	-	NA	Light brown/ orange	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP04	1750- 2500		Sandy CLAY	-	NA	Grey mottled red (30%) & orange (10%).	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP05	0-230		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP05	230- 880	400-800	SAND with silt	-	NA	Grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	5.4	0.004	<0.1	<250
TP05	880- 2500		Sandy GRAVEL	-	Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub- angular, (F:15% / M:30% / C:10%).	Structureless	>3.0	20	35	50	-	-	-	-
TP06	0-350		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP06	350- 1200	500-800	Sandy GRAVEL	-	Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub- angular, (F:20% / M:20% / C:10%)	Structureless	>3.0	20	35	50	5.9	0.02	1.4	966
TP06	1200- 1800		Sandy GRAVEL			Brown	Gravel and sand - Fine to coarse, sub-rounded to sub- angular, (F:20% / M:30% / C:10%)	Structureless	>3.0	20	35	50	-	-	-	-
TP06	1800- 2500		Sandy GRAVEL			Brown	Gravel and sand - Fine to coarse, sub-rounded to sub- angular, (F:40% / M:20%)	Structureless	>3.0	20	35	50	-	-	-	-

3.3 Site assessment results

Based on an assessment of the soil physical and chemical results for the six test pit locations in Table 5, it is recommended that the LAAs for the Race Track and Motocross Precincts are located at TP01 and TP06, respectively.

- Motocross Precinct (TP06):
 - AS1547 soil type = Gravel
 - Indicative soil permeability (Ksat) = > 3.0 m/d
 - Design irrigation rate = 5 mm/d
- Race Track Precinct (TP01):
 - AS1547 soil type = Light clay
 - Indicative soil permeability (Ksat) = < 0.06 m/d
 - Design irrigation rate = 3 mm/d

As per the DOHWA (2021) guidance, a Level of Constraint (Low, Moderate or High) is determined by applying a risk assessment to each site characteristic and the following mitigation measures may be applied:

- Nil or Low
 - If all constraints are Low, standard designs are generally satisfactory and no mitigation measures are required.
- Moderate
 - For each Moderate constraint an appropriate mitigation measure or design modification over and above that of a standard design, should be outlined.
- High
 - Any High constraint might prove an impediment to successful on-site wastewater management, or alternatively will require in-depth investigation and incorporation of sophisticated mitigation measures in the design to permit compliant onsite wastewater management.

A summary of site assessment results, including the level of constraint for each characteristic, within the Motocross Precinct in Table 6 and Race Track Precinct is outlined in Table 7.

3.3.1 Motocross Precinct

A summary of site assessment results for SSE for the recommended LAA within the Motocross Precinct (TP06) has been provided in Table 6.

Table 6

Summary of site assessment results for SSE of the proposed LAA within the Motocross Precinct (TP06)

Characteristic		Level of Constraint		Results for TP06	Assessed				
	Nil or Low	Moderate	High		Level of Constraint for Site				
General Characteristic	General Characteristics								
Climate (difference between average annual rainfall and average pan evaporation, mm/year)	Excess of evaporation over rainfall in the wettest months	Rainfall approximates to evaporation	Excess of rainfall over evaporation in the wettest months	Rainfall in excess of evaporation from May to September	High				
Exposure to sun and wind	Full sun and/or high wind or minimal shading and North / North-East	Dappled light East / West / South-East / South-West aspect	Limited patches of light and little wind to heavily shaded all day and South aspect	Full sun	Nil or Low				

Characteristic		Level of Constraint		Results for TP06	Assessed	
	Nil or Low	Moderate	High		Level of Constraint for Site	
	/North-West aspect					
Vegetation coverage over the site	Plentiful vegetation with healthy growth and good potential for nutrient uptake Turf or pasture	Limited variety of vegetation	Sparse vegetation or no vegetation, dense forest with little understorey	Good cover of existing pasture	Nil or Low	
Landslip (or landslip potential)	Nil	Low to moderate	High or Severe	No landslip evident	Nil or Low	
Slope Form (affects water shedding ability)	Hill crests, convex or divergent side- slopes and plains	Straight side- slopes and footslopes	Floodplains, concave or convergent side- slopes and incised channels	Straight waxing upperslope (UX)	Moderate	
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	Nil or Low	
Slope gradient (%)						
(a) for absorption trenches and beds	<5%	5-15%	>15%	Approximately 6%	Moderate	
(b) for surface/ subsurface irrigation	<10%	10-20%	>20%	Approximately 6%	Nil or Low	
Erosion (or potential for erosion)	Nil or Low	Moderate	Severe	Good cover of existing pasture, upslope stormwater diversion and sub- surface irrigation proposed	Nil or Low	
Fill (imported)	No fill at present or fill is good quality topsoil or minimal fill required	Moderate coverage and good quality fill	Extensive poor- quality fill and variable quality fill	No fill at present	Nil or Low	
Flood frequency (AEP)	Less than 1 in 100 years	Between 100 and 20 years	More than 1 in 20 years	Less than 1 in 100 years	Nil or Low	
Private bore used for household/drinking water purposes	No bores onsite or on neighbouring properties	>30 m to the nearest private bore	<30 m to the nearest private bore	APEC bores located >30 m	Moderate	
Proximity to water resources	>100 m	<100 m but reduced setback is supported (refer to Section 5.2.2 of the GSP)	<100 m and reduced setback is not supported (refer to Section 5.2.2 of the GSP)	>100 m to Protected Exclusion Area and Marbellup Flats	Nil or Low	

Characteristic		Level of Constraint		Results for TP06	Assessed
	Nil or Low	Moderate	High		Level of Constraint for Site
Public Drinking Water Source Areas (PDWSA) and Sewage Sensitive Areas (SSA)	Site not located within a PDWSA or SSA	Site located within a PDWSA or SSA	Site located within both a PDWSA and SSA	Priority 2 PDWSA – Marbellup Brook Catchment Area SSA (<1 km from conservation category wetland)	High
Groundwater (wettest time of the year)	>2 m	2.0 – 0.6 m need for fill to achieve setbacks listed in Appendix 1	<0.6 m fill is not practical to achieve setbacks listed in Appendix 1	Groundwater not intercepted >2.5 m	Nil or Low
Land area available for LAA	Exceeds the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Meets the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Insufficient area available for LAA as per AS1547 or Schedule 2 of the GSP	550 m ² available for sub-surface irrigation	Nil or Low
Rock outcrops (% of surface)	<10%	10-20%	>20%	No rock outcrops observed	Nil or Low
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit.	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	Nil or Low
Stormwater run- on/run-off	Low likelihood of stormwater run- on/run-off	Moderate likelihood of stormwater run- on/run-off, need for diversionary structures	High likelihood of inundation by stormwater run- on/run-off, diversion not practical	Upslope stormwater diversion proposed	Nil or Low
Soil profile characteri	stics				
Soil permeability Category (AS1547)	2 and 3	4 and 5	1 and 6	1	High
Profile depth	>2 m	2.0-1.0	< 1.0 m	2.5 m bgl	Nil or Lov
Hardpan or bedrock	>1.5 m	1.5-0.6 m Special design requirements and distribution techniques or soil modification will be necessary, depends on quality of treated wastewater and type of LAS	<0.6 m	Sandy GRAVEL encountered to 2.5 m bgl	Nil or Low
Presence of mottling	None	Moderate	Extensive	None	Nil or Low
Coarse fragments	< 10%	10-40%	>40%	10% Cobbles and boulders in excess of 400 mm diameter	Nil or Low

Characteristic		Level of Constraint		Results for TP06	Assessed
	Nil or Low	Moderate	High		Level of Constraint for Site
рН	6.0 - 8.0	4.5 - 6.0	<4.5, >8	5.9 - pH between <5 and >8 therefore likely to be suitable for plant growth	Moderate
Electrical Conductivity (ECe)(dS/m)	<0.3	0.3 - 2	>2	0.02	Nil or Low
Sodicity ESP%	<3	3.0 - 8.0	>8	1.4	Nil or Low
Phosphorus adsorption (mg/kg)	>500	200-500	<200	966	Nil or Low

3.3.2 Race Track Precinct

A summary of site assessment results for SSE for the recommended LAA within the Race Track Precinct (TP01) has been provided in Table 7.

 Table 7
 Summary of site assessment results for SSE of the proposed LAA within the Race Track Precinct (TP01)

Characteristic	Level of Constraint			Results for TP01	Assessed
	Nil or Low	Moderate	High		Level of Constraint for Site
General Characteristics					
Climate (difference between average annual rainfall and average pan evaporation, mm/year)	Excess of evaporation over rainfall in the wettest months	Rainfall approximates to evaporation	Excess of rainfall over evaporation in the wettest months	Rainfall in excess of evaporation from May to September	High
Exposure to sun and wind	Full sun and/or high wind or minimal shading and North / North- East /North-West aspect	Dappled light East / West / South-East / South-West aspect	Limited patches of light and little wind to heavily shaded all day and South aspect	Full sun	Nil or Low
Vegetation coverage over the site	Plentiful vegetation with healthy growth and good potential for nutrient uptake Turf or pasture	Limited variety of vegetation	Sparse vegetation or no vegetation, dense forest with little understorey	Good cover of existing pasture	Nil or Low
Landslip (or landslip potential)	Nil	Low to moderate	High or Severe	No landslip evident	Nil or Low
Slope Form (affects water shedding ability)	Hill crests, convex or divergent side- slopes and plains	Straight side- slopes and footslopes	Floodplains, concave or convergent side-slopes and incised channels	Straight waxing upperslope (UX)	Moderate

Characteristic	Level of Constraint			Results for TP01	Assessed
	Nil or Low	Moderate	High		Level of Constraint for Site
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	Nil or Low
Slope gradient (%)					
(a) for absorption trenches and beds	<5%	5-15%	>15%	Approximately 6%	Moderate
(b) for surface/ subsurface irrigation	<10%	10-20%	>20%	Approximately 6%	Nil or Low
Erosion (or potential for erosion)	Nil or Low	Moderate	Severe	Good cover of existing pasture, upslope stormwater diversion and sub-surface irrigation proposed	Nil or Low
Fill (imported)	No fill at present or fill is good quality topsoil or minimal fill required	Moderate coverage and good quality fill	Extensive poor- quality fill and variable quality fill	No fill at present	Nil or Low
Flood frequency (AEP)	Less than 1 in 100 years	Between 100 and 20 years	More than 1 in 20 years	Less than 1 in 100 years	Nil or Low
Private bore used for household/drinking water purposes	No bores onsite or on neighbouring properties	>30 m to the nearest private bore	<30 m to the nearest private bore	APEC bores located >30 m	Moderate
Proximity to water resources	>100 m	<100 m but reduced setback is supported (refer to Section 5.2.2 of the GSP)	<100 m and reduced setback is not supported (refer to Section 5.2.2 of the GSP)	>100 m to Protected Exclusion Area and Marbellup Flats	Nil or Low
Public Drinking Water Source Areas (PDWSAs) and Sewage Sensitive Areas (SSA)	Site not located within a PDWSA or SSA	Site located within a PDWSA or SSA	Site located within both a PDWSA and SSA	Priority 2 PDWSA – Marbellup Brook Catchment Area and SSA (<1 km from conservation category wetland)	High
Groundwater (wettest time of the year)	>2 m	2.0 – 0.6 m need for fill to achieve setbacks listed in Appendix 1	<0.6 m fill is not practical to achieve setbacks listed in Appendix 1	Groundwater not intercepted >2.5 m	Nil or Low
Land area available for LAA	Exceeds the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Meets the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Insufficient area available for LAA as per AS1547 or Schedule 2 of the GSP	Sufficient area available for sub- surface irrigation	Nil or Low
Rock outcrops (% of surface)	<10%	10-20%	>20%	No rock outcrops observed	Nil or Low

Characteristic	Level of Constraint			Results for TP01	Assessed	
	Nil or Low	Moderate	High		Level of Constraint for Site	
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit.	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	Nil or Low	
Stormwater run- on/run-off	Low likelihood of stormwater run- on/run-off	Moderate likelihood of stormwater run- on/run-off, need for diversionary structures	High likelihood of inundation by stormwater run- on/run-off, diversion not practical	Upslope stormwater diversion proposed	Nil Low	
Soil profile characteristic	cs					
Soil permeability Category (AS1547)	2 and 3	4 and 5	1 and 6	5	Moderate	
Profile depth	>2 m	2.0-1.0	< 1.0 m	2.5 m bgl	Nil or Low	
Hardpan or bedrock	>1.5 m	1.5-0.6 m Special design requirements and distribution techniques or soil modification will be necessary, depends on quality of treated wastewater and type of LAS	<0.6 m	Sandy CLAY intercepted at 550 mm bgl	High	
Presence of mottling	None	Moderate	Extensive	Sandy CLAY mottled	Moderate	
Course fragments	< 10%	10-40%	>40%	10% Cobbles and boulders in excess of 250 mm diameter	Nil or Low	
рН	6.0 - 8.0	4.5 - 6.0	<4.5, >8	6.1	Nil or Low	
Electrical Conductivity (ECe)(dS/m)	<0.3	0.3-2	>2	0.022	Nil or Low	
Sodicity Exchangeable sodium percentage (ESP%)	<3	3.0 - 8.0	>8	5.8 – no evidence of dispersion, slaking, or structural decline	Moderate	
Phosphorus adsorption (mg/kg)	>500	200-500	<200	688	Nil or Low	

3.3.3 Mitigation measures

The majority of constraints assessed in 3.3.1 and 3.3.1 were found to be Nil or Low, however several key constraints were found to be High or Moderate. Proposed mitigation measures for the aspects which are considered to have a High or Moderate constraint within the Race Track Precinct and Motocross Precinct are included in Table 8.

Table 8

Proposed mitigation measures for High and Moderate constraints

Cons	traints	
Race Track Precinct	Motocross Precinct	Proposed mitigation measures
High		
Climate - Rainfall in excess of evaporat	ion from May to September	Diversion of stormwater from upslope around sub-soil irrigation area
Priority 2 PDWSA – Marbellup Brook Conservation category wetland)	The proposed LAA achieves a 2 m vertical separation to groundwater	
Hardpan or bedrock <0.6 m - Sandy CLAY intercepted at 550 mm bgl	-	Amend soils in LAA
-	Soil permeability Category (AS1547) – (1) Gravels and sands	Accommodate permeability via Design Loading Rates (DLRs) and Design Irrigation Rates (DIRs)
Moderate		
Slope Form (affects water shedding abi	Diversion of stormwater from upslope around sub-soil irrigation area	
Slope gradient (%) (a) for absorption tre	enches and beds – 5-15%	No absorption trenches or beds proposed
APEC bores located >30 m		APEC bore located 250 m away – no modification considered necessary
Presence of mottling - Sandy CLAY mottled	-	Amend soils in potential LAA
Soil permeability Category (AS1547) – (5) Light clay	-	Accommodate permeability via Design Loading Rates (DLRs) and Design Irrigation Rates (DIRs)
Sodicity ESP – 5.8%	-	No evidence of dispersion, slaking or structural decline in the soils on or near the potential LAA
-	pH 5.9	No evidence of scald or bare areas on or near the potential LAA

4. Wastewater management system type and design

4.1 Specific assessment SSE – Sizing for treatment system and land application area

The sizing for a wastewater treatment system and LAA has been developed in this SSE report for Stage 1A in the Motocross Precinct only.

As per the requirements of the Department of Water *WQPN 100* (DoW, 2007) and the *Government Sewerage Policy* (DPLH, 2019) a 'Secondary' wastewater treatment plant, with engineering certification to meet effluent quality of Biological Oxygen Demand (BOD) < 20 mg/L; Total Suspended Solids (TSS) < 30 mg/L; Total Nitrogen (TN) < 10 mg/L; Total Phosphorus (TP) < 1 mg/L; and *Escherichia coli* < 10 cfu/100mL is required in a Priority 2 PDWSA.

It is recommended to install a 'Secondary' treatment system, with nutrient removal such as Aquarius Wastewater Systems Pty Ltd, which provide DOHWA approved systems. An example of the type of system that would meet the requirement of a 'Secondary' treatment system is provided in Appendix F. These systems have a nutrient reduction capability of which includes reduction of TN to < 10 mg/L and TP to < 1 mg/L and are certified to AS1546.3:2008.

4.1.1 Water balance

A water balance has been developed for the operation of the wastewater system, as per the water balance in the DOHWA (2021) guidance, for Stage 1A of the AMP development in the Motocross Precinct and included in Appendix B.

The water balance has been developed based on the following:

- A design wastewater flow of 3,500 L/day (average of 100 persons and 15,000 L storage tank)
- Design irrigation rate for sub-surface irrigation of 5.0 mm/day
- Rainfall run-off factor of 0.9
- Mean monthly rainfall levels at the Albany Airport Comparison weather station (BoM, 2021)
- Pan evaporation data (DPIRD, 1987)

The results of the water balance for the Motocross Precinct, for an average of 100 persons/day, indicate that 1,100 m² will be required for the sub-soil irrigation area. There is adequate area of land available within the vicinity of TP06 to accommodate the site of the required LAA.

4.2 Siting and configuration of the Land Application Area

4.2.1 Setback distances

Based on an assessment of the soil physical and chemical results for the six test pit locations in Table 5, it is recommended that the LAAs for the Race Track and Motocross Precincts are located at TP01 and TP06, respectively.

All sub-soil irrigation areas will be located >100 m to Protected Exclusion Area and Marbelup Flats (Conservation Class wetland) (Figure 3, Appendix A).

The sub-soil irrigation area will be fenced and will be separate from the activities within the Precinct to maintain public amenity.

4.2.2 Stormwater management

Stormwater management will include diversion drains, water treatment areas and attenuation basins to control stormwater across the Race Track Precinct and Motocross Precinct as per the Stormwater Management Plan (GHD, 2021) prepared for the Development Application for the AMP.

5. Monitoring, operation and maintenance

Baseline groundwater and surface water quality sampling of the Site was undertaken by Bio Diverse Solutions in 2018 and 2019 (Bio Diverse Solutions, 2018). DWER has been consulted during the development of the Site Local Water Management Strategy (LWMS) (GHD, 2021) as part of the Scheme Amendment process. The following surface and groundwater pre-development, construction and post-development monitoring is outlined as per the approved LWMS.

5.1 Surface water monitoring

5.1.1 Pre-development and construction monitoring

Ongoing quarterly monitoring of existing Site surface water conditions shall be continued prior to development, and during construction of the AMP as per the Local Water Management Strategy approved by DWER as part of the Scheme Amendment process.

In combination with the existing 2018 and 2019 data, the ongoing monitoring will be used as a baseline for ongoing assessment of the potential impact of the development on shallow groundwater and surface water quality. Additionally, pre-development water monitoring data will be used to identify water quality trigger levels at which a response is required.

For surface water monitoring during the construction phase of the development, a CEMP shall be prepared by the Contractor which will include erosion and sedimentation control measures, as well as drainage and dewatering systems (if required) in order to minimise potential pollution impacts and prevent contamination to surface water and groundwater.

5.1.2 Post-development monitoring

Ongoing monthly monitoring of surface water conditions shall be continued post-development (for the duration of the operation of the facility), with continued monitoring at sites CS01 and CS02, and establishment of a new upstream monitoring location. Additional sampling shall also be undertaken in response to any spill events.

The post-development monitoring program will also involve the collection of grab samples from the compensating basins. Sampling of basins should comprise 3-4 events per year, during or immediately following significant rainfall events (1EY, 1 year ARI event). It is assumed the first flush events will have the highest level of nutrients and chemicals, therefore sampling should occur at the time/after the first significant rainfall events of each wet season, and after extended dry periods. Field notes should include details of the rainfall events, site conditions, time of sampling and time of sample testing.

Monitoring of the compensation basin inlet and outlet water quality will be used to assess performance of the basins in improving stormwater quality.

Annual water monitoring reports shall be submitted to DWER and the Water Corporation. A water quality response and contingency plan will be prepared and provided to the Water Corporation, City of Albany and DWER for advice.

5.1.3 Monitoring program summary

The recommended monitoring parameters for the ongoing pre-development, construction and postdevelopment monitoring program are outlined in Table 9.

Site	Frequency	Duration	Parameters
Surface water - Upstream of the site (TBC)	Monthly	Ongoing, with annual reporting	In-situ: pH, EC, temperature
- Mid-stream (CS02) - Downstream of the site (CS01)			Unfiltered sample: pH, EC, TN, FRP, TKN, ammonia, TP, TRH, PAH, BTEXN, Surfactants, microbial analysis
Compensating basin - Inlet (4 No.) - Outlet (4 No.)	3-4 events per year following 1EY rainfall events		
			Filtered sample: Filtered total nitrogen and filtered total phosphorus (to quantify organic component), NO ₂ /NO ₃ , PO ₄ , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)

Table 9 Summary of surface water monitoring

5.2 Groundwater monitoring

5.2.1 Pre-development and construction monitoring

Ongoing monitoring of existing Project Site shallow groundwater conditions shall be continued prior to development, and during construction of the AMP. In combination with the existing 2018 and 2019 data, the ongoing monitoring will be used as a baseline for ongoing assessment of the potential impact of the development on shallow groundwater and surface water quality.

Additionally, pre-development water monitoring data will be used to identify water quality trigger levels at which a response is required.

5.2.2 Post-development monitoring

A groundwater monitoring network should be established post development, the locations of which will be based on groundwater monitoring strategy.

Ongoing monitoring of the groundwater monitoring bores shall be conducted for the duration of the operation of the facility and in accordance with the groundwater monitoring program in Table 10.

Annual water monitoring reports will be submitted to DWER and the Water Corporation.

A water quality response and contingency plan will be prepared and provided to the Water Corporation, City of Albany and DWER for advice.

In addition if the development proposal seeks a licence to take water and approval to install a production bore for abstraction of groundwater as a water supply source for the development, then six-monthly groundwater monitoring for water levels and salinity will be a required.

5.2.3 Monitoring program summary

The program and parameters outlined in Table 10 will provide a suitable representation of groundwater quality at the site. The groundwater bores established for pre-development monitoring will be used for construction phase and incorporated into the post-development monitoring network.

Site	Frequency	Duration	Parameters
Monitoring bores Monthly Production bore	Pre-development, during construction, on-going throughout the life of development.	Water level	
		In-situ: pH, EC, temperature	
		Unfiltered sample: pH, EC, TN, FRP, TKN, ammonia, TP, TRH, PAH, BTEXN, Surfactants, microbial analysis	
			Filtered sample: Filtered total nitrogen and filtered total phosphorus (to quantify organic component), NO ₂ /NO ₃ , PO ₄ , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)

 Table 10
 Summary of groundwater monitoring

5.2.4 Contingency measures

Pre-development water monitoring data shall be used to identify water quality trigger levels at which a management response is required. A water quality response and contingency plan shall be included in the surface and groundwater monitoring plans.

In the event of a major water quality incident at the Site, it is recommended that increased monitoring be undertaken to quantify if there is any impact to surface and groundwater quality. Contingency monitoring and response measures shall be developed in consultation with DWER and documented in the post-development monitoring program.

Potential incidents due to system failure and/ or mechanical breakdown during operation and maintenance of the installed system shall be addressed, as required, as per the manufacturer and installation instructions.

6. Conclusion and recommendations

The SSE report for the AMP site involved evaluation of site and soil, physical and chemical properties, to identify appropriate onsite effluent disposal LAAs within the Race Track Precinct and Motocross Precinct. Based on an assessment of the soil physical and chemical results for the six test pit locations, it is recommended that the LAAs for the Race Track Precinct and Motocross Precinct are located at TP01 and TP06, respectively.

The sizing for a wastewater treatment system and LAA has been developed in this SSE report for Stage 1A in the Motocross Precinct only.

The proposed clubhouse within the Motocross Precinct will be constructed in Stage 1A of the development. It is anticipated that this will be an unlicenced facility (15 L/ person/ day) however provision has been made for anticipated wastewater volumes for a licenced facility (35 L/ person/ day), to allow for possible increased loading at the site if it were to become a licenced facility.

The Motocross Precinct clubhouse is expected to have intermittent use throughout the Motocross season and on a weekly basis, with up to 300 patrons on Sunday or Saturday followed by minimal usage during the week and off-season downtime. Therefore, for the purpose of calculating anticipated wastewater volumes it is assumed that there is an average of 100 people/ day.

In order to accommodate spikes in wastewater volumes on event days when there is up to 300 patrons using the Motocross Precinct clubhouse facilities, it is proposed to install a 15,000 L holding tank, to balance storage over the course of a typical week.

The results of a water balance for the Motocross Precinct, for an average of 100 persons/day, indicate that 1,100 m² will be required for the sub-soil irrigation area. There is adequate area of land available within the vicinity of TP06 to accommodate the site of the required LAA.

As per the requirements of the Department of Water *WQPN 100* (DoW, 2007) and the *Government Sewerage Policy* (DPLH, 2019) a 'Secondary' wastewater treatment plant, with engineering certification to meet effluent quality of Biological Oxygen Demand (BOD) < 20 mg/L; Total Suspended Solids (TSS) < 30 mg/L; Total Nitrogen (TN) < 10 mg/L; Total Phosphorus (TP) < 1 mg/L; and *Escherichia coli* < 10 cfu/100mL is required in a Priority 2 PDWSA.

It is recommended that a DOHWA approved 'Secondary' treatment system, certified to AS1546.3:2008, is selected and installed for the Motocross Precinct during Stage 1A of development.

At time of writing, an onsite effluent disposal system was not proposed to be installed in the Race Track Precinct. All liquid waste from transportable buildings, toilets and washdown facilities is proposed to be removed offsite, as required, by an approved contractor. If onsite effluent disposal is proposed in the future is it expected a similar system, with holding tank, will be utilised to manage spikes in wastewater volumes for events and off-season downtime.

In addition it is recommended, as per the DOHWA (2021) guidelines, that the following is undertaken:

- Have a suitably qualified maintenance contractor service the secondary and advanced secondary treatment system every three months, as required by Council under the approval to operate.
- Annual inspections should be undertaken on treatment tanks and desludging undertaken on annual, two yearly or four yearly cycles depending on the size of the tank installed.
- All land application systems should be sited in an area that will not be frequented by vehicle or foot traffic or will not be built on or covered with paved over.
- Any subsurface irrigation areas should be vegetated (i.e. with grass that can be mown regularly) to encourage growth and maximise nutrient uptake.
- Irrigation lines should be maintained as per manufacturer's instructions (e.g. flushing).
- Stormwater and surface run-on should be diverted around, or away from, land application areas.

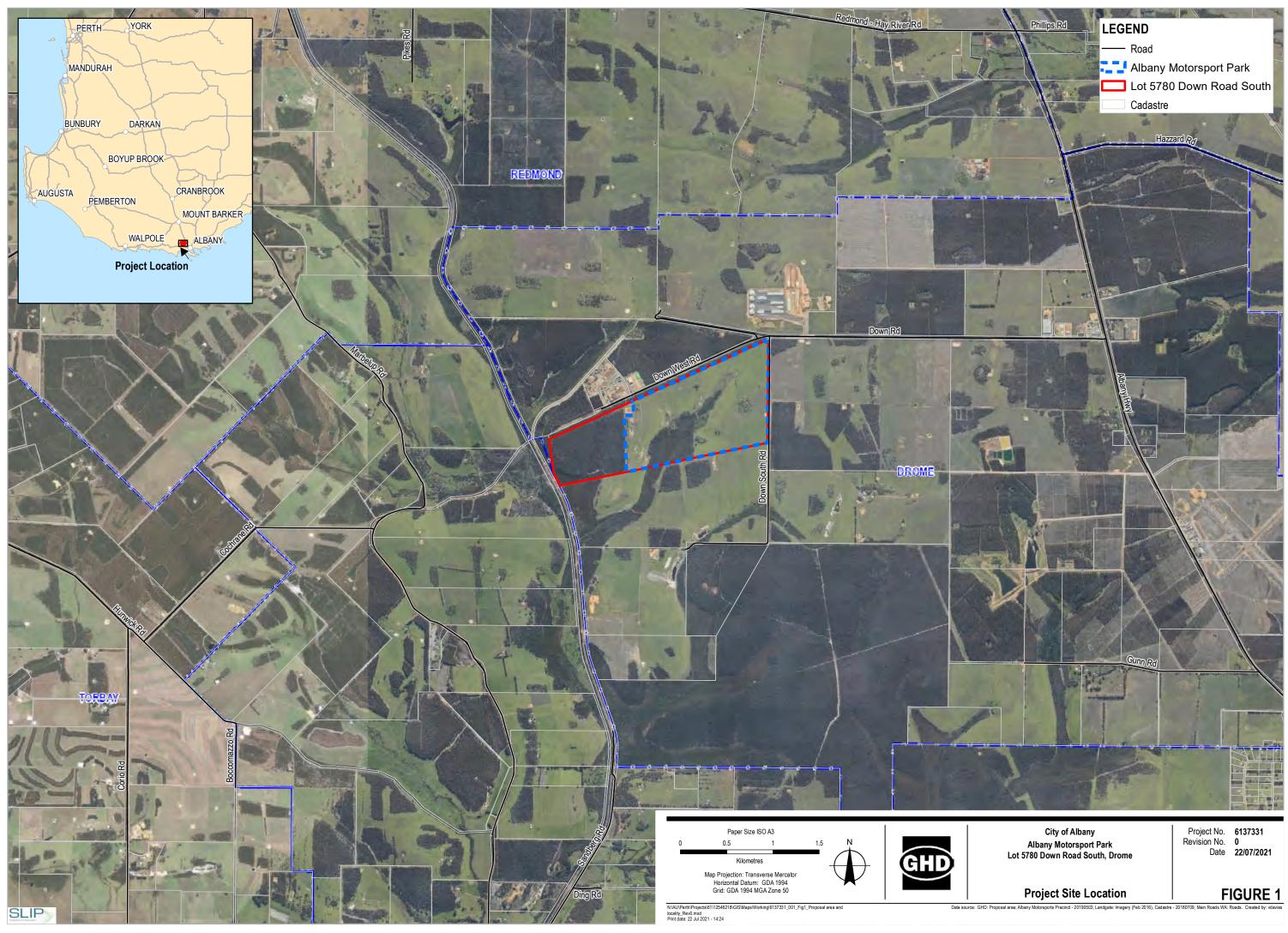
- Landowners should be cognisant of the operation of their system and monitor the treatment and land application area to identify any potential issues (e.g. insufficient septic treatment, clogging of the system, pooling of treated effluent).
- The volume of wastewater produced should remain the same and not exceed the operational capacity of the system, it will ensure the effective long-term operation of the systems
- Chemicals, large quantities of cleaning products, fats, oils and grease, and food scraps should not be discharged to the wastewater treatment and disposal system, as they risk overloading or interfering with the functioning of the system.

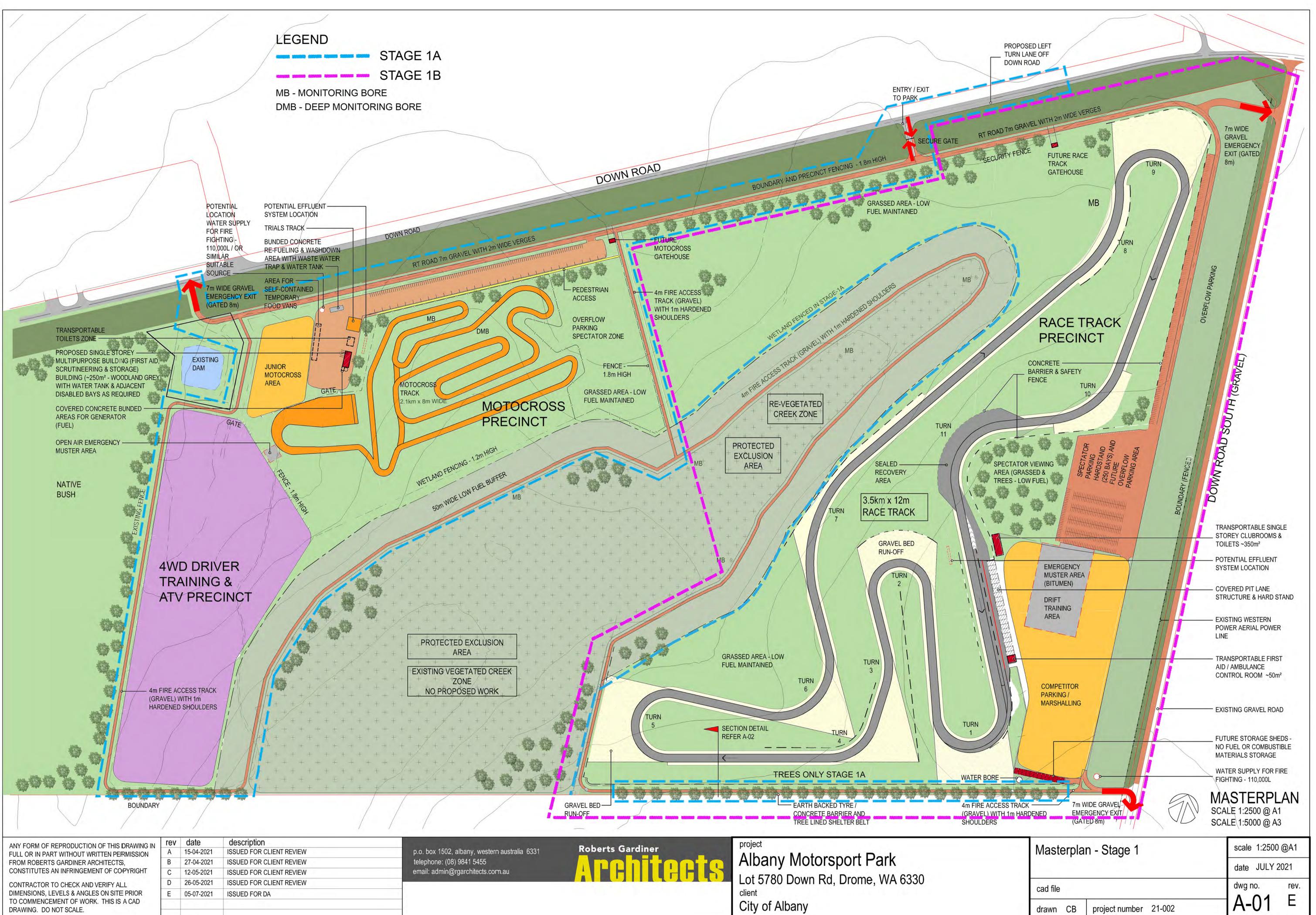
7. References

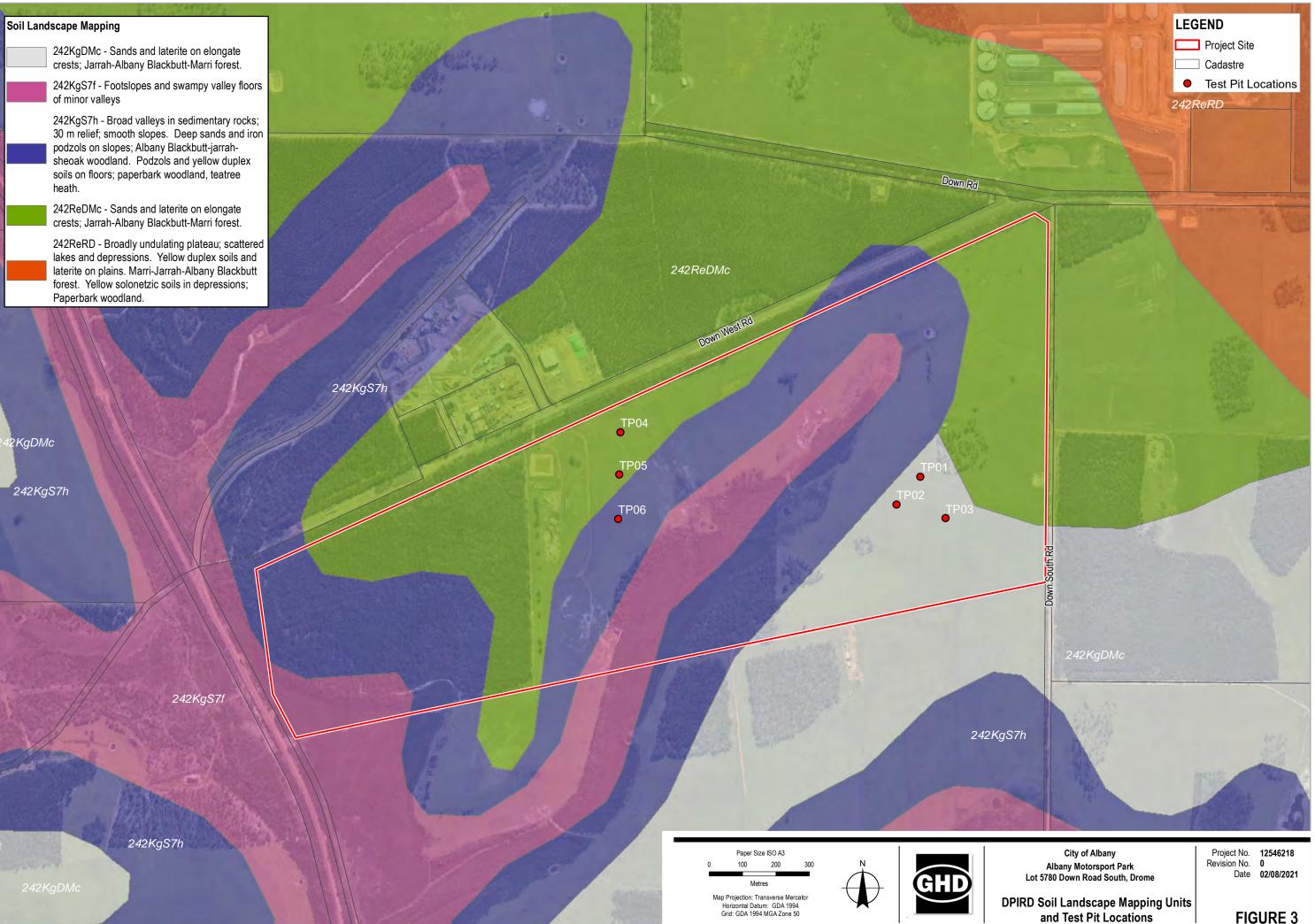
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Appendix A Figures

Figure 1	Project Site Location
Figure 2	Albany Motorsport Park Master Plan – Stage 1 (Roberts Gardiner Architects, 2021)
Figure 3	DPIRD Soil Landscape Mapping Units and Test Pit Locations
Figure 4	Groundwater Conditions, Topography and Test Pit Locations
Figure 5	Water Erosion Risk (DPIRD-013)
Figure 6	Hydrology and Hydrogeology
Figure 7	PDWSA and Water Management Areas
Figure 8	Master Plan – 100 m Setback to Protected Exclusion Area and Marbellup Flats (Conservation Class)
Figure 9	Flood Risk (DPIRD-007)







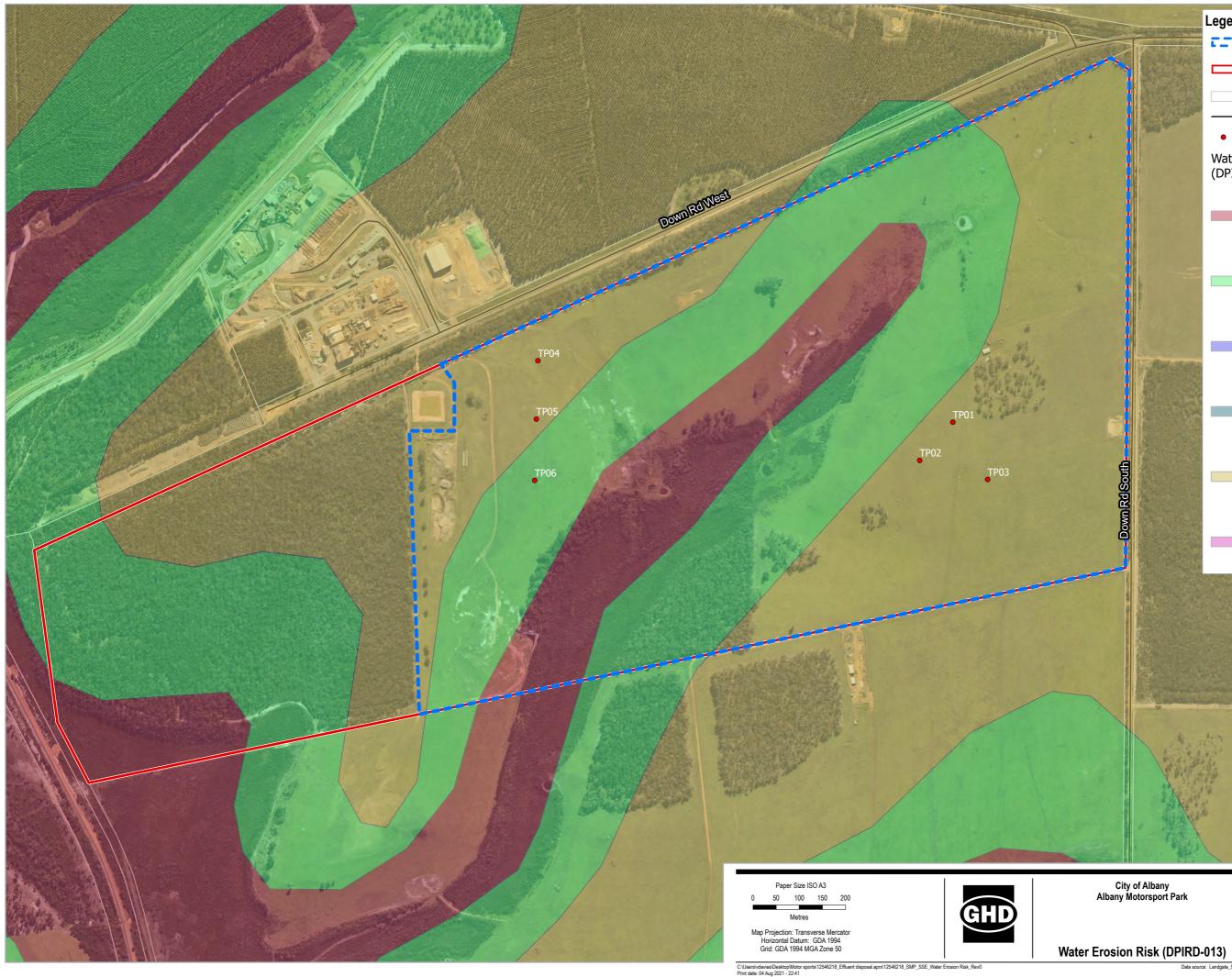
and Test Pit Locations

FIGURE 3

Data source: GHD: Project Site - 20180702; Landgate: Imagery (Feb 2016), Cadastre, Roads - 20180709: DPIRD: Soil Landscane Manning (Res



N:AU/Perth/Projectsi61112546218/GIS/Maps/Working112546218/12546218_Effluent disposal.aprx112546218_SMP_GroundwaterConditions_RevA Print date: 02 Aug 2021 - 23:41



Legend

- CC Albany Motorsport Park
- Lot 5780 Down Road South
- Cadastre
- ----- Road
- Test Pit Locations

Water Erosion Risk (DPIRD-013)

10-30% of map unit has a high to extreme water erosion risk

> 3-10% of map unit has a high to extreme water erosion risk

30-50% of map unit has a high to extreme water erosion risk

> 50-70% of map unit has a high to extreme water erosion risk

<3% of map unit has a high to extreme water erosion risk

>70% of map unit has a high to extreme water erosion risk

SLIP

Project No. 12546218 Revision No. 0

Date 4/08/2021

Figure 5

Water Erosion Risk (DPIRD-013)

Data source: Landgate_Subscription_Imagery\WANow: Landgate / SLIP. Created by: vdavies



LEGEND

Albany Motorsport Park Project Site \triangle Shallow Bores Deep Bore Groundwater Level (BGL) August 2019 Regional Groundwater Flow Direction Shallow Aquifer Flow Direction South Coast Significant Wetland

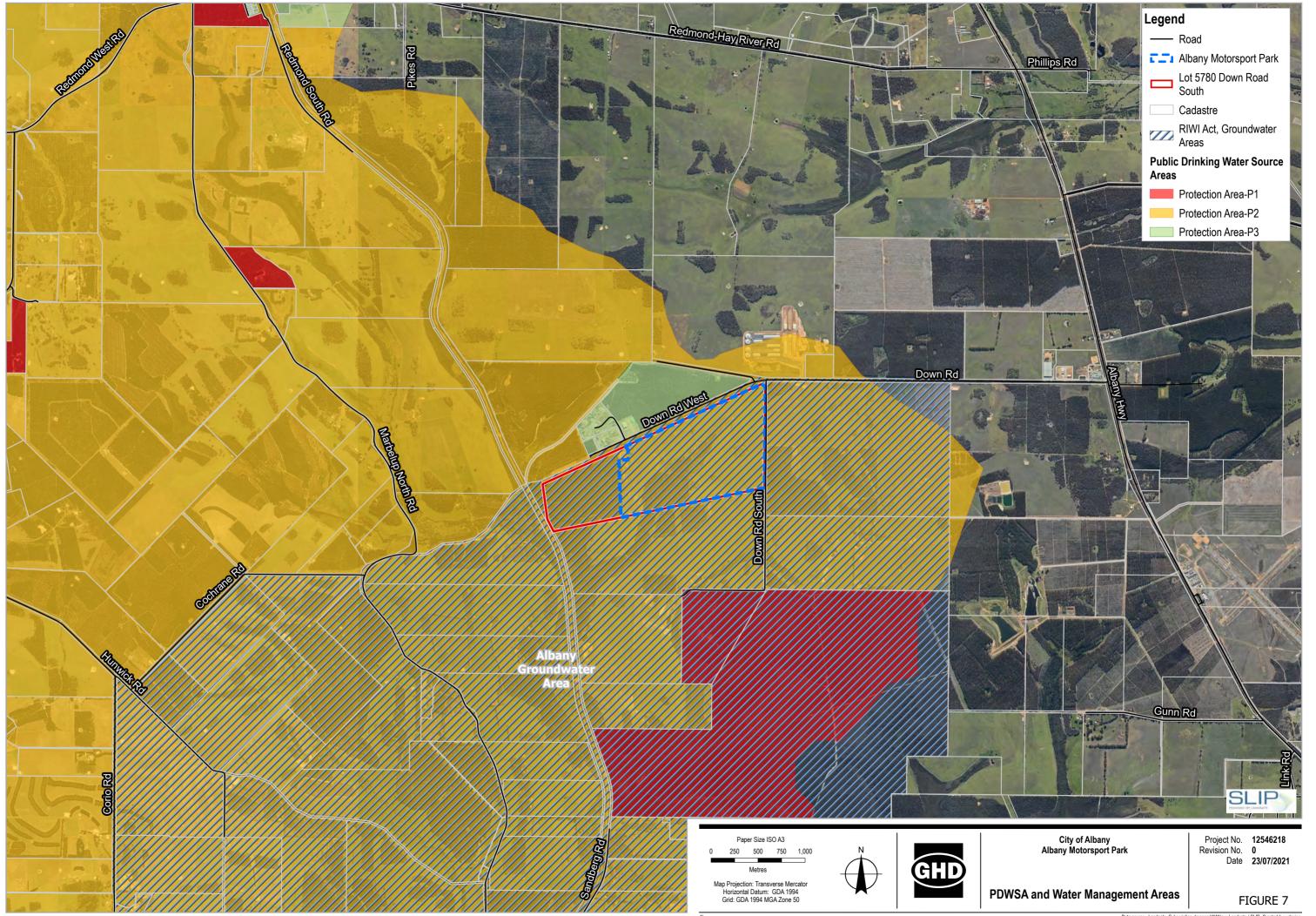
City of Albany Great Southern Motor Sports Park Feasibility Study Lot 5780 Down Road South, Drome

Project No. **12546218** Revision No. **0**

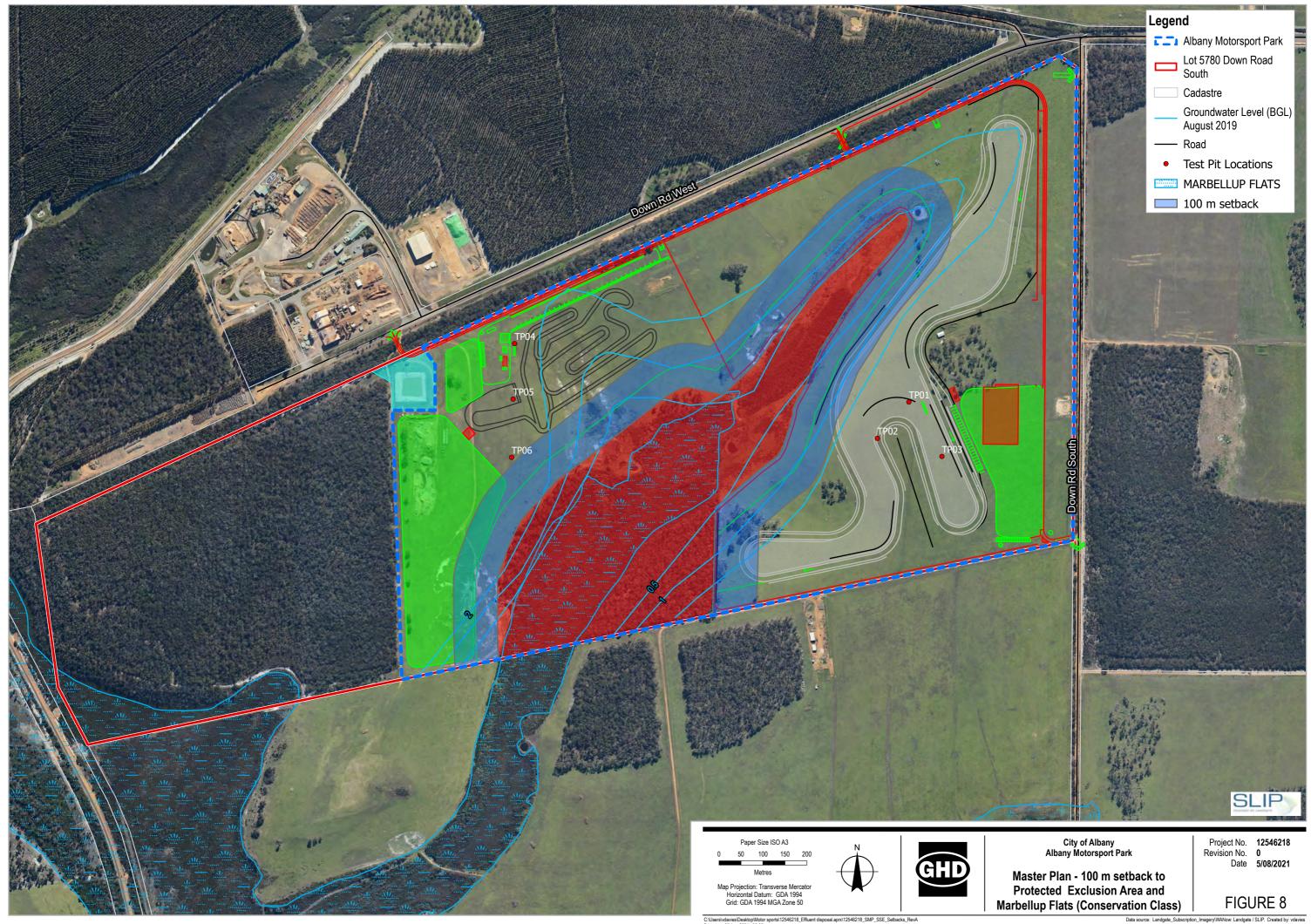
Date 05/08/2021

Hydrology and hydrogeology

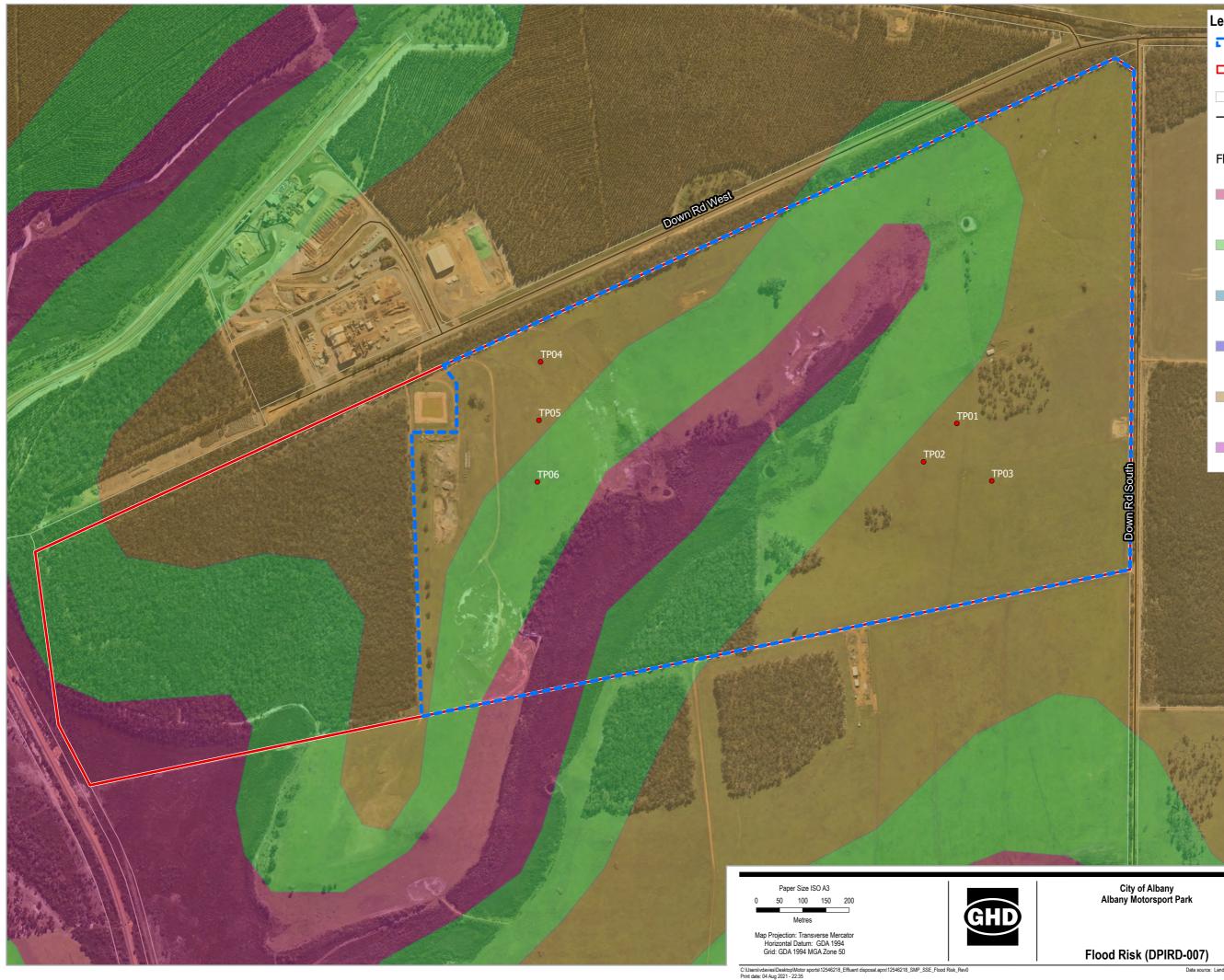
FIGURE 6 nerv - (Feb 2016) Cadastre



Nul/Perth/Projects/61112546218(GISMaps/Working)12546218(12546218_StormwaterManagementPlan)12546218_Stormw Print date: 23 Jul 2021 - 11:25 aterManagementPlan.aprx\12546218



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Legend

- CC Albany Motorsport Park
- Lot 5780 Down Road South
- Cadastre

----- Road

• Test Pit Locations

Flood Risk (DPIRD-007)

10-30% of the map unit has a moderate to high flood risk

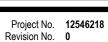
3-10% of the map unit has a moderate to high flood risk

30-50% of the map unit has a moderate to high flood risk

50-70% of the map unit has a moderate to high flood risk

<3% of the map unit has a moderate to high flood risk

>70% of the map unit has a moderate to high flood risk



Date 4/08/2021

FIGURE 9

SLIP

Data source: Landgate_Subscription_Imagery\WANow: Landgate / SLIP. Created by: vdavies

Appendix B Water balance

Albany Motorsport Park

Motocross - Effluent Disposal Water Balance

Hydraulic loading:

35 L/person/d

Section 29 of Health (Treatment of Sewage and Disposal of Effluent and Liquid Waste) Regulations 1974

Activity	Mon	Tues	Wed	Thu	Fri	Sat	Sun			
Training - attendees	20	20	20	20	20					
Club event - attendees	;					300	300			
Flow	700	700	700	700	700	10500	10500	24,500	L/week (tot	al)
								3,500	L/d (averag	je)
									100	persons
Cum. IN	700	1400	2100	2800	3500	14000	24500			
Cum. OUT	3,500	7,000	10,500	14,000	17,500	21,000	24,500			
	11,200	8,400	5,600	2,800	0	7,000	14,000		Tank size:	14,000

Site Address:	Lot 578) Down R	oad So	uth, Dro	me											
Date:	Thursda	y, 12 Aug	ust 2021		Assesso	or:	Jeff Fo	ey								
NPUT DATA																
Design Wastewater Flow	Q	3,500	L/dav	Based on ma	ximum potential	occupancy	and derived fr	om the Supr	lement to R	egulation 29	and Schedu	e 9 - Wastev	vater system	loading rate	s	
Design Irrigation Rate	DIR	5.0	mm/day		oil texture class											
Nominated Land Application Area	L	1100	m ²	1			,									
Crop Factor	C	0.8-1.0	unitless	Estimates e	evapotranspirati	on as a fra	ction of pan	evaporation	· varies wi	th season ar	nd crop typ	2				
Rainfall Runoff Factor	RF	0.9	untiless		of rainfall that re							5				
Aean Monthly Rainfall Data		mate/averages/ta			n and number			ates, anowi	ing for any	lanon						
Aean Monthly Pan Evaporation Data		ny - Agric refere			n and number o	r data from	the Evapora	ation Data f	or Westerr	Australia R	eport					
	1100	ing rightereter.			archlibrary.agric.						opon					
Parameter	Symbol	Formula	Units	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
Days in month	D		days	31	28	31	30	31	30	31	31	30	31	30	31	365
Rainfall	R		mm/month	23.6	22.3	33.6	61.3	89.8	108	119.3	106.8	88.5	70.8	47	27.8	798.8
Evaporation Crop Factor	E		mm/month unitless	220 1.00	171 1.00	150 0.90	91 0.90	63 0.80	47 0.80	59 0.80	67 0.80	84 0.90	106 1.00	150 1.00	199 1.00	1407
	U		unitiess	1.00	1.00	0.90	0.90	0.80	0.80	0.80	0.80	0.90	1.00	1.00	1.00	
Evapotranspiration	ET	ExC	mm/month	220	171	135	82	50	38	47	54	76	106	150	199	1327.3
Percolation	B	DIRxD	mm/month	155.0	140	155.0	82 150.0	50 155.0	38 150.0	47	54 155.0	150.0	155.0	150	155.0	1327.3
Outputs	D	ET+B	mm/month	375.0	311	290.0	231.9	205.4	187.6	202.2	208.6	225.6	261.0	300.0	354.0	3152.3
NPUTS																
Retained Rainfall	RR	RxRF	mm/month	20.06	18.955	28.56	52.105	76.33	91.8	101.405	90.78	75.225	60.18	39.95	23.63	678.98
Applied Effluent	W	(QxD)/L	mm/month	98.6	89.1	98.6	95.5	98.6	95.5	98.6	98.6	95.5	98.6	95.5	98.6	1161.4
Inputs		RR+W	mm/month	118.7	108.0	127.2	147.6	175.0	187.3	200.0	189.4	170.7	158.8	135.4	122.3	1840.3
STORAGE CALCULATION																
Storage remaining from previous month			mm/month	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Storage for the month		(RR+W)-(ET+B)	mm/month	-256.3	-203.0	-162.8	-84.3	-30.4	-0.3	-2.2	-19.2	-54.9	-102.2	-164.6	-231.7	
Cumulative Storage Maximum Storage for Nominated Area	M		mm	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Maximum Storage for Norminated Area	N V	NxL	mm	0.00	-											
AND AREA REQUIRED FOR ZE	v		 m ²	306	336	415	584	841	1096	1076	921	698	540	404	328	
		-			_	415	564	841	1096	1076	921	098	540	404	328	
MINIMUM AREA REQUIRED FOR	R ZERO STO	RAGE:		1097	m²											
CELLS																

NOTES

¹ This value should be the largest of the following: land application area required based on the most limiting nutrient balance or minimum area required for zero storage ² Values selected are suitable for grass in WA

Appendix C GHD Pty Ltd Professional Indemnity Insurance Certificate

WillisTowersWatson I.I"IIII

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Fax:	+61 2 9995 7297
Website:	www.willistowerswatson.com.au
Direct Line:	+61 2 9285 4060
Email:	tanya.stevenson@willistowerswatson.com

Issue Date: 24 November 2020

To Whom It May Concern

Certificate of Placement – Professional Indemnity

In our capacity as Insurance Broker to the Named Insured shown below, we confirm having arranged the following insurance, the details of which are correct as at the Issue Date:

Named Insured:	GHD Group Limited and Subsidiaries including GHD Pty Ltd
Form:	Civil Liability Wording which includes coverage for the Trade Practices Act and the Competition and Consumer Act
Policy Number:	B080113856P20
Limit of Indemnity:	AUD2,000,000 any one claim and in the aggregate
Period of Insurance:	1 December 2020 at 4.00pm to 1 December 2021 at 4.00pm
Insurer:	Certain Underwriters at Lloyd's of London



Signed for and on behalf of Willis Australia Ltd ("Willis Towers Watson")

Disclaimer:

This document has been prepared at the request of our client and does not represent an insurance policy, guarantee or warranty and cannot be relied upon as such. All coverage described is subject to the terms, conditions and limitations of the insurance policy and is issued as a matter of record only. This document does not alter or extend the coverage provided or assume continuity beyond the Expiry Date. It does not confer any rights under the insurance policy to any party. Willis Towers Watson is under no obligation to inform any party if the insurance policy is cancelled, assigned or changed after the Issue Date.

Willis Australia Limited ABN 90 000 321 237 AFSL No: 240600 Version 2016 1.0 18 Apr 2016

Appendix D

Albany Motorsport Park Development -Site Investigation Report 4626/1 (Great Southern Geotechnics, 2021)



GREAT SOUTHERN GEOTECHNICS CONSTRUCTION MATERIALS TESTING

Site Investigation

Report 4626/1 Monday, 28 June 2021



Albany Motorsport Park Development

GREAT SOUTHERN GEOTECHNICS

1.0 INTRODUCTION

As authorised by GHD an investigation for the proposed Albany Motorsport Park Development adjacent to Down Rd, Mirambeena was performed on the 25/06/2021

2.0 GENERAL

The intent of the investigation was to determine the following:

- Soil types and profiles.
- Groundwater levels at time of investigation.

3.0 SITE INVESTIGATION

Site conditions and test pit locations were recorded and are displayed in Appendix A - Maps. Test pits logs/ soil profiles are noted in Appendix B - Test Pit Logs

The field investigation consisted of 6 Boreholes excavated on-site to depths of up to 2.5 meters using a Kubota KX41-3V mini excavator with a 300mm Auger.

Test pits were spread across the extent of the proposed development and locations were predetermined by GHD.

All soil layers encountered were visually assessed and classified on-site.

Samples gathered from site were the taken back to Great Southern Geotechnics Albany Laboratory then

IMPORTANT NOTE: The test pits have been spread so that they are representative of the subsurface materials across the intended reconstruction area, however, soil conditions may change dramatically over short distances and our investigations may not locate all soil variations across the site.

4.0 LABORATORY TESTING

No laboratory testing have been undertaken at Great southern Geotechnics laboratory. Sampled taken have been transported by freight to Eurofins Scientific for further analysis. Testing requirements will be confirmed by GHD post review of investigation findings.

This report and associated documentation was undertaken for the specific purpose described in the report and shall not be relied on for other purposes.

This report was prepared solely for the use by GHD any reliance assumed by other parties on this report shall be at such parties own risk.



Appendix A Maps

Figure 1 Test Pits 1 to 6 Test Pit Locations





Job No:4626Client:GHDProject:Albany Motorsport Park Development





Appendix B

Test Pit Logs

B Image: Signed Sector Se	GREA GEO COMSTRUC	AT SOUT DTECHI	THERN NICS	Job No 4626	Test Pit N 1	1o.	Sample No. 4626G1		Sheet	1	of	12	
Image: Control of the set of the	Project: Alb Project No. QU	bany Motors U-0498		·	25/06/202 Logged B	21 3y	Equipment type: Excavation Method	Kubota KX41-3V d : 300mm Auger					
Image: Normal Standard State State Image: Normal State	Depth Below Surface (mm)	Layer Depth (mm)	Ρε	SOIL TY	PE, Plasticity, Colo		nponents	Moist. Condition	Classification Symbol	Sample/Test			
Image: Normal state	0 - 180	180	(Topsoi	I) SAND with silt: Dark	grey, fine to mediu	m. Roots	and root fibres.	M L-MD					
Image: Normal state	400 400	24.0	0				ude en ander						
Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter. Image: Contains approximately 10% Cobbles & Boulde	180 - 490	310	Sand	-									#
580 - 2500 1950 Sandy CLAY: Low to medium plasticity, Brown/red motiled Light brown/orange (40%). M F I <tdi< td=""> I<!--</td--><td></td><td></td><td>Contains a</td><td>•</td><td>•</td><td>-</td><td></td><td colspan="5"></td><td></td></tdi<>			Contains a	•	•	-							
Fine to medium grained sand. Image: Construction of the sector of th													
Image: Second	550 - 2500	1950	Sandy CLAY	: Low to medium plastici	ity, Brown/red mottl	led Light I	prown/orange (40%).	%). M F					#
Image: Construct of the sector of the sec				Fine to m	edium grained san	d.					Э		
Image: Construct of the sector of the sec											ntere		
Image: Construct of the sector of the sec											ncou		
Image: Construct of the sector of the sec											ole ei		
Image: Construct of the sector of the sec											er tak		
Image: Construct of the sector of the sec											wate		
TP1 - 180mm to 490mm Cave In Cave In TP1 - 900mm to 1100mm Refusal Refusal Cave In Refusal Refusal Near Refusal Near Refusal VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Indurated S - Soft L - Loose VL - Very Low PC - Poorly Cemented General F - Firm MD - Medium Dense L - Low MC - moderately Cemented D - Dry M - Moist W - Wet St - Stiff D - Dense M - Medium MC - moderately Cemented D - Dry M - Moist W - Wet											Å		
TP1 - 180mm to 490mm Cave In Cave In TP1 - 900mm to 1100mm Refusal Image: Colspan="4">Cover In TP1 - 900mm to 1100mm Refusal Image: Colspan="4">Cover In TP1 - 900mm to 1100mm Refusal Image: Colspan="4">Cover In Refusal Image: Colspan="4">Near Refusal Cohesive Non-Cohesive Rock Cementation Flooding Image: Colspan="4">Image: Colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: Colspan="4">Image: Colspan="4">Image: Colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: Colspan="4">Image: Colspan="4" Image: Colspan="4">Image: Colspan="4" Image: Colspan="4" Ima													
TP1 - 180mm to 490mm Cave In TP1 - 900mm to 1100mm Refusal Image: Colspan="4">Cave In TP1 - 900mm to 1100mm Refusal Image: Colspan="4">Cover In Refusal Image: Colspan="4">Near Refusal Cohesive Non-Cohesive Rock Cementation Flooding Image: Colspan="4">Image: Colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: Colspan="4">Image: Colspan="4">Image: Colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: Colspan="4">Image: Colspan="4">Image: Colspan="4">Image: Colspan="4">Cohesive S - Soft L - Loose VL - Very Low PC - Poorly Cemented Image: Colspan="4">Image: Colspan="4" VS - Very Soft U - Loose U - Loow MC - moderately D - Dry M - Moist W - Wet St - Stiff U - Very Dense													
TP1 - 180mm to 490mm Cave In Cave In TP1 - 900mm to 1100mm Refusal Refusal Cave In Refusal Refusal Near Refusal Near Refusal VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Indurated S - Soft L - Loose VL - Very Low PC - Poorly Cemented General F - Firm MD - Medium Dense L - Low MC - moderately Cemented D - Dry M - Moist W - Wet St - Stiff D - Dense M - Medium MC - moderately Cemented D - Dry M - Moist W - Wet													
TP1 - 180mm to 490mm Cave In TP1 - 900mm to 1100mm Refusal Image: colspan="4">Cave In TP1 - 900mm to 1100mm Refusal Image: colspan="4">Cover In Refusal Image: colspan="4">Near Refusal Cohesive Non-Cohesive Rock Cementation Flooding Image: colspan="4">Image: colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: colspan="4">Image: colspan="4" VS - Very Soft VL - Very Lows PC - Poorly Cemented Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4" St - Stiff D - Dense M - Medium MC - moderately D - Dry M - Moist W - Wet VSt - Very Stiff VD - Very Dense H - High MC - mod													
TP1 - 180mm to 490mm Cave In TP1 - 900mm to 1100mm Refusal Image: colspan="4">Cave In TP1 - 900mm to 1100mm Refusal Image: colspan="4">Cover In Refusal Image: colspan="4">Near Refusal Cohesive Non-Cohesive Rock Cementation Flooding Image: colspan="4">Image: colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: colspan="4">Image: colspan="4" VS - Very Soft VL - Very Lows PC - Poorly Cemented Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4" St - Stiff D - Dense M - Medium MC - moderately D - Dry M - Moist W - Wet VSt - Very Stiff VD - Very Dense H - High MC - mod													
TP1 - 180mm to 490mm Cave In Cave In TP1 - 900mm to 1100mm Refusal Refusal Cave In Refusal Refusal Near Refusal Near Refusal VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Indurated S - Soft L - Loose VL - Very Low PC - Poorly Cemented General F - Firm MD - Medium Dense L - Low MC - moderately Cemented D - Dry M - Moist W - Wet St - Stiff D - Dense M - Medium MC - moderately Cemented D - Dry M - Moist W - Wet													
TP1 - 180mm to 490mm Cave In TP1 - 900mm to 1100mm Refusal Refusal TP1 - 900mm to 1100mm Refusal Near Refusal Cohesive Non-Cohesive Rock Cementation VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: Communication of the second of th													
TP1 - 180mm to 490mm Cave In TP1 - 900mm to 1100mm Refusal Image: colspan="4">Cave In TP1 - 900mm to 1100mm Refusal Image: colspan="4">Cover In Refusal Image: colspan="4">Near Refusal Cohesive Non-Cohesive Rock Cementation Flooding Image: colspan="4">Image: colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4">Cohesive VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: colspan="4">Image: colspan="4" VS - Very Soft VL - Very Lows PC - Poorly Cemented Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4">Image: colspan="4" St - Stiff D - Dense M - Medium MC - moderately D - Dry M - Moist W - Wet VSt - Very Stiff VD - Very Dense H - High MC - mod													
TP1 - 180mm to 490mm Cave In C				Samples Taken				Ta	arget De	oth	✓	25	00
Non-Cohesive Rock Cementation Near Refusal VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach S - Soft L - Loose VL - Very Low PC - Poorly Cemented F - Firm MD - Medium Dense L - Low St - Stiff D - Dense M - Medium MC - moderately Cemented D - Dry M - Moist W - Wet VSt - Very Stiff VD - Very Dense H - High MC - moderately Cemented D - Dry M - Moist W - Wet				TP1 - 180mm to 490mm									
CohesiveNon-CohesiveRockCementationFloodingImage: Sector of the sec			Т	P1 - 900mm to 1100mm	ı			Refusal					
VS - Very Soft VL - Very Loose EL - Extremely Low IN - Indurated Lack of Reach Image: Constraint of Constraints S - Soft L - Loose VL - Very Low PC - Poorly Cemented Image: Constraints Image: Constraints F - Firm MD - Medium Dense L - Low PC - Poorly Cemented Image: Constraints Image: Constraints St - Stiff D - Dense M - Medium MC - moderately Cemented D - Dry M - Moist W - Wet VSt - Very Stiff VD - Very Dense H - High Image: Constraints N/A - Not Applicable								N					
S - Soft L - Loose VL - Very Low PC - Poorly Cemented F - Firm MD - Medium Dense L - Low St - Stiff D - Dense M - Medium VSt - Very Stiff VD - Very Dense H - High													
F - Firm MD - Medium Dense L - Low St - Stiff D - Dense M - Medium VSt - Very Stiff VD - Very Dense H - High	-		-			11	I - Indurated	La	ck of Re				
F - Firm MD - Medium Dense L - Low St - Stiff D - Dense M - Medium VSt - Very Stiff VD - Very Dense H - High D - Dry M - Moist W - Moist W - Wet					-	PC - F	Poorly Cemented	d General					
VSt - Very Stiff VD - Very Dense H - High Cemented N/A - Not Applicable		N					_	<u> </u>					
									-				t
	-		-		-		Comented						
H - Hard CO - Compact VH - Very High WC - Well Cemented N/D - Not Determined	H - Hard		CO - Com			WC -	Well Cemented		N/E) - Not l	Jetermi	ned	



Excavation



Spoil



Job No:4626Client:GHDProject:Albany Motorsport Park Development

Sheet 2 of 12

GR GR GR GR GR	EAT SOU EOTECH	THERN INICS RIALS TESTING	Job No 4626	Test Pit No 2	о.	Sample No. 4626G2		Sheet	3	of	12		
Client: Project: Project No. Location:	QU-0498	orsport Park De S 117°44'50.2"		Date Commen 25/06/2021 Logged By M.Coffey	1 y	Operator/Contractor Equipment type: Excavation Method Position:							
Depth Below Surface (mm)	Layer Depth (mm)	F		rial Description PE, Plasticity, Colou condary and other n		nponents	Moist. Condition Consistency / Strength Cementation Water Table						
0 - 140	140	(Topso	oil) SAND with silt: Dark	grey, fine to medium	n. Roots	and root fibres.	fibres. M L-MD						
140 400	000	<u> </u>		. to oppose - 1	م م م	uh angular							
140 - 400	260	Sar	dy GRAVEL: Brown, fine (F:20% / M:20% / C:15				M VD MC						
		Contains	approximately 10% Cobb		-								
		Contains											
400 - 1400	1000		Sandy CLAY: Low to	medium plasticity,	Light bro	wn.	M _ F						
			-	edium grained sand	-					ď.		#	
										o water table encountered.			
1400 - 2500	1100	Sandy CLA	Y: Low to medium plastici	ty, Brown/red mottle	ed Light b	rown/orange (40%).	М	F		ncon		#	
			Fine to m	edium grained sand	1.					ble e			
										ter ta			
										o wat			
										ž			
		1											
			Samples Taken					Farget Dep		~	25	500	
		-	TP2 - 500mm to 900mm TP2 - 1700mm to 2000mm				Cave In						
							Refusal Near Refusal						
Cohesive		Non-Cohe	esive	Rock	(Cementation	'	Flooding					
VS - Very Sof	ft	VL - Very I		xtremely Low		N - Indurated	L	ack of Rea					
S - Soft		L - Loo		- Very Low	5.5				Ger	eral			
F - Firm		MD - Medium	n Dense I	L - Low	PC -	Poorly Cemented							
St - Stiff		D - Den	se M·	- Medium	MC -	dorotoly Comt-	1	D - Dry	/ M-N	<i>N</i> oist V	V - Wet		
VSt - Very Sti	ff	VD - Very [Dense H	H - High		oderately Cemented		Ν	I/A - Not	Applicab	le		
H - Hard		CO - Corr	ipact VH -	· Very High	WC	- Well Cemented		N	/D - Not I	Determin	ed		
			EH - E	xtremely High	VVC		iented						



Excavation



Spoil



Job No:4626Client:GHDProject:Albany Motorsport Park Development

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	UCTION MATERIA	NICS	Job No 4626	Test Pit N 3	lo.	Sample No. 4626G3		Sheet	5	of	12		
Project: A Project No. Q	U-0498	sport Park De 117°44'56.4"E		Date Commer 25/06/202 Logged B M.Coffey	1 y	Operator/Contractor Equipment type: Excavation Method Position:	Kubota KX41-3V						
Depth Below Surface (mm)	Layer Depth (mm)	Ρ		erial Description (PE, Plasticity, Colo econdary and other i		iponents	Moist. Condition Consistency / Strength Cementation Water Table						
0 - 250	250	(Topsoil) S	SAND with silt: Dark gre	ey to grey, fine to me	edium. Ro	ots and root fibres.	М	L-MD					
050 000	500												
250 - 830	580	San	dy GRAVEL: Brown, fine	e to medium, sub-rol . Fine to medium gra		v .	M MD-D						
		Contains	approximately 10% Cob	-			-+-+						
		Contains				dameter.							
830 - 1600	770		Sandy CLAY: Low to	o medium plasticity.	Liaht bro	wn.	M F					#	
	-		-	nedium grained sand	-			·		Р			
				_						Itere			
1600 - 2500	900	Sandy CLA	AY: Low to medium plast	ticity, Brown/red mot	ttled Light	brown/grey (30%).	М	F		Incor		#	
			Fine to n	nedium grained sand	d.				o water table encountered.				
										er tak			
										wate			
										No			
_													
 								$\left - \right $					
							· · · · · ·						
			Samples Taken				Т	arget Dep	th	~	25	500	
			TP3 - 300mm to 600mm	n			Cave In						
			TP3 - 900mm to 1200mr				Refusal						
			FP3 - 1600mm to 2000m				N	ear Refus	al				
Cohesive		Non-Cohe		Rock		ementation		Flooding					
VS - Very Soft		VL - Very L		Extremely Low	11	N - Indurated	La	ack of Rea					
S - Soft		L - Loos		- Very Low	PC - I	Poorly Cemented	General						
F - Firm		MD - Medium		L - Low									
St - Stiff		D - Den		- Medium	MC - mo	derately Cemented		D - Dry		Aoist V			
VSt - Very Stiff H - Hard		VD - Very D		H - High					/A - Not				
		CO - Com	pact VH	- Very High	WC-	Well Cemented	nted N/D - Not Determined						



Excavation



Spoil



Job No:4626Client:GHDProject:Albany Motorsport Park Development

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G GF G	REAT SOU EOTEC	UTHERN HNICS ERIALS TESTING	Job No 4626	Test Pit No 4	o.	Sample No. 4626G4		Sheet	7	of	12	
Client: Project: Project No. Location:	QU-0498	torsport Park De "S 117°44'17.6"l		Date Commen 25/06/2021 Logged By M.Coffey	1 y	Operator/Contractor Equipment type: Excavation Methoo Position:	Kubota KX41-3V					
Depth Below Surface (mm)	Layer Depth (mm)	Р		erial Description PE, Plasticity, Colou econdary and other n		iponents	Moist. Condition	Classification Symbol	Sample/Test			
0 - 220	220	(Topso	bil) SAND with silt : Dark	grey, fine to medium	n. Roots a	and root fibres.	М	L-MD				
000 4050	4000											
220 - 1250	1030	Sar	dy GRAVEL: Brown, fine (F:25% / M:20% / C:10			-	M D					
		Contains	approximately 10% Cobb	•	-							
		Contains				oomin diameter.	+ $+$ $+$ $+$ $+$					
1250 - 1750	500		Sandy CLAY: Low to me	dium plasticity. Ligh	ht brown/o	orange.	M F					#
			-	edium grained sand		5				ъ.		
										Itere		
1750 - 2500	750	Sandy CI	LAY: Low to medium plas	sticity, grey mottled re	red (30%)	& orange (10%).	М	F		o water table encountered.		#
			Fine to m	edium grained sand	ł.					le er		
										er tab		
										wate		
										Å		
	ļ											
	<u> </u>											
												ļ
			Samples Taken				Target Depth ✓ 250					500
			TP4 - 400mm to 800mm				Cave In					
		-	TP4 - 1350mm to 1650mr				Refusal					
		-	TP4 - 1800mm to 2200mr	n			Near Refusal					
Cohesive		Non-Cohe	esive	Rock	C	ementation		Flooding				
VS - Very Sc	oft	VL - Very L	Loose EL - E	xtremely Low	11	N - Indurated	L	ack of Rea	h			
S - Soft		L - Loo:	se VL	- Very Low		Poorly Cemented	General					
F - Firm		MD - Medium	n Dense	L - Low								
St - Stiff		D - Den	se M	- Medium	MC - mo	derately Cemented		D - Dry	/ M - N	Moist V	V - Wet	
VSt - Very St	tiff	VD - Very [Dense H	H - High		Contented	N/A - Not Applicable					
H - Hard		CO - Com	npact VH	- Very High	WC.	Well Cemented	N/D - Not Determined					
			EH - E	xtremely High								



Excavation



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Job No:4626Client:GHDProject:Albany Motorsport Park Development

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GR GE CONST	EAT SOU OTECH	THERN INICS HALS TESTING	Job No 4626	Test Pit N 5	No.	Sample No. 4626G5		Sheet	9	of	12	
Project: Project No.	QU-0498	orsport Park De S 117°44'17.5"		Date Comme 25/06/202 Logged E M.Coffey	21 3y	Operator/Contractor Equipment type: Excavation Methoo Position:			30	GSG oota KX4 0mm Au er to site	ger	
Depth Below Surface (mm)	Layer Depth (mm)	F		erial Description (PE, Plasticity, Colo econdary and other		nponents	Moist. Condition	Classification Symbol	Sample/Test			
0 - 230	230	(Topso	bil) SAND with silt : Dark	grey, fine to mediu	ım. Roots	and root fibres.	M L-MD					
230 - 880	650		SAND with s	silt: Grey, fine to me	edium.		M MD					#
880 - 2500	1620			a ta agarag ayık ya	unded to .	uh angular	M MD-D					
880 - 2500	1620	Sar	ndy GRAVEL: Brown, fin (F:15% / M:30% / C:10									#
		Contains	approximately 10% Cob		-		+ $+$ $+$ $+$ $+$					
		-								ъ.		
										water table encountered.		
										Incort		
										ole er		
										er tak		
										wate		
										Ň		
								$\left \right $				
			Samples Taken				Т	arget Dep	th	✓	25	500
			TP5 - 400mm to 800mm	1			Cave In					
			TP5 - 1200mm to 1500m	m			Refusal					
							N	Near Refusal				
Cohesive		Non-Cohe		Rock		Cementation		Flooding				
VS - Very Soft	τ	VL - Very I		Extremely Low		IN - Indurated	Lack of Reach					
S - Soft		L - Loo		- Very Low	PC -	Poorly Cemented	General					
F - Firm		MD - Medium		L - Low								
St - Stiff		D - Den		- Medium	MC - m	oderately Cemented		D - Dry		Aoist V		
VSt - Very Stif		VD - Very [H - High						Applicab		
H - Hard	<u> </u>	CO - Com		- Very High	WC	- Well Cemented		N	יט - Not l	Determin	ea	
			EH - E	Extremely High								



Excavation



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GR GR GR	REAT SOU EOTECI STRUCTION MATE	UTHERN HNICS ERIALS TESTING	Job No 4626	Test Pit N 6	lo.	Sample No. 4626G6		Sheet	11	of	12	1
Client: Project: Project No. Location:	QU-0498	torsport Park De "S 117°44'17.4"		Date Comme 25/06/202 Logged B M.Coffey	1 9 y	Operator/Contractor Equipment type: Excavation Methoor Position:		Kubota KX41-3V				
Depth Below Surface (mm)	Layer Depth (mm)	F		erial Description /PE, Plasticity, Colo econdary and other		nponents	Moist. Condition	Classification Symbol	Sample/Test			
0 - 350	350	(Topso	bil) SAND with silt: Dark	grey, fine to mediu	m. Roots	and root fibres.	M L-MD					
		_										
350 - 1200	850	Sar	ndy GRAVEL: Brown, fin				M D-VD					#
		Oantaina	(F:20% / M:20% / C:10		-							
		Contains	approximately 10% Cobl	bies & Boulders in e	excess of	400mm diameter.						
1200 - 1800	600	Sandy	GRAVEL: Light brown,	fine to coarse sub-	rounded	o sub-angular	M D					#
1200 - 1000	000	Gana	(F:20% / M:30% / C:10				IVI					#
			(1.20%) (1.00%) (1.00%)		graniea					tered		
1800 - 2500	700	Sandy	GRAVEL: Brown/orange,	fine to medium, sul	b-rounde	to sub-angular,	М	MD-D		water table encountered.		#
			0	Fine to medium gra		.				e en		
			· · ·	<u> </u>						r tabl		
										vatei		
										Š		
		_										
												ļ
			Samples Taken				Target Depth ✓ 2500					500
			TP6 - 500mm to 800mm	1			Cave In					
			TP6 - 1300mm to 1600m				Refusal					
			TP6 - 2000mm to 2300m	m			Ν	lear Refus	al			
Cohesive		Non-Cohe	esive	Rock		Cementation		Flooding				
VS - Very So	ft	VL - Very I	_oose EL - E	Extremely Low		N - Indurated	La	ack of Rea	h			
S - Soft		L - Loo	se VL	- Very Low	PC	Poorly Cemented	General					
F - Firm		MD - Mediun	n Dense	L - Low	FU-							
St - Stiff		D - Der	ise M	- Medium	MC - m	oderately Cemented	D - Dry M - Moist W - Wet					
VSt - Very Sti	iff	VD - Very I	Dense	H - High	1010 - 111			Ν	I/A - Not	Applicab	le	
H - Hard		CO - Com	npact VH	- Very High	WC	- Well Cemented		N	/D - Not I	Determin	ed	
			EH - E	Extremely High	110	Wen Gemented						



Excavation



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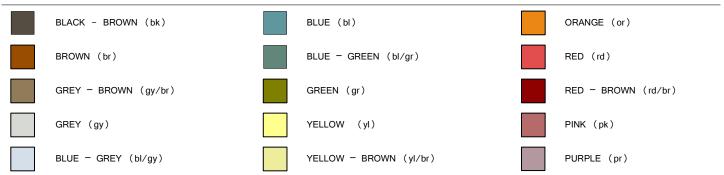


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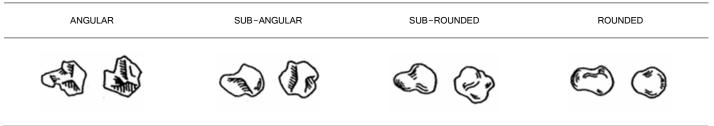
COLOURS



MOISTURE CONDITION OF SOIL

TERM	DESCRIPTION
Dry	Cohesive soils; hard and friable or powdery, well dry of plastic limit. Granular soils; cohesionless and free-running.
Moist	Soil feels cool, darkened in colour. Cohesive soils can be moulded. Granular soils tend to cohere.
Wet	Soil feels cool, darkened in colour. Cohesive soils usually weakened and free water forms on hands when handling. Granular soils tend to cohere and free water forms on hands when handling.

PARTICLE SHAPES



PARTICLE SIZES

BOULDERS	COBBLES	COARSE GRAVEL	MEDIUM GRAVEL	FINE GRAVEL	COARSE SAND	MEDIUM SAND	FINE SAND	SILT	CLAY
>200mm	63- 200mm	20- 63mm	6- 20mm	2.36- 6mm	0.6- 2.36mm	0.2- 0.6mm	0.075- 0.2mm	0.002- 0.075mm	<0.002mm

GRAIN SIZE

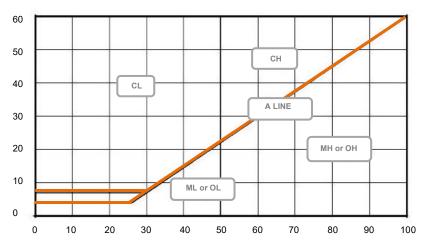
SOIL TYPE (ABBREV.)	CLAY (CL)	SILT (SI)	←	SAND (SA)	\longrightarrow	<	GRAVEL (GR)	\longrightarrow	COBBLES (CO)
SIZE	< 2µm	2-75µm	Fine 0.075- 0.2mm	Medium 0.2-0.6mm	Coarse 0.6-2.36mm	Fine 2.36-6mm	Medium 6-20mm	Coarse 20-63mm	63-200mm
SHAPE & TEXTURE	Shiny	Dull	<	a	ngular or sub an	gular or sub ro	unded or rounded	i ———	\longrightarrow
FIELD GUIDE	Not visible under 10x	Visible under 10x	Visible by eye	Visible at < 1m	Visible at < 3m	Visible at < 5m	Road gravel	Rail ballast	Beaching



CLASSIFICATION CHART

	FIELD IDENTIFICATION PROCEDURES (Excluding particles larger than 60mm and basing fractions on estimated mass)							TYPICAL NAMES	
E	fraction	EAN VELS or no is)	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength Predominantly one size or range of sizes with some intermediate sizes missing, not enough fines to bind earner grains and due to the size of the size					Well graded gravels, gravel-sand mixtures, little or no fines	
han 0.075	GRAVELS 60% of coarse 1 er than 2.36mn	CLE GRAN (Little fine	Predominar		with some intermediate sizes rse grains, no dry strength	missing, not	GP	Poorly Graded gravels and gravel-sand mixtures, little or no fines, uniform gravels	
COARSE GRAINED SOILS More than 50% of material less than 63 mm is larger than 0.075 mm	GRAVELS More than 50% of coarse fraction is larger than 2.36mm	GRAVELS WITH FINES (Appreciable amount of fines)	Dirty'n	naterials with excess of non-pla	astic fines, zero to medium dry	strength	GM	Silty gravels, gravel-sand-silt mixtures	
GRAINED SOILS than 63 mm is	More t	GRAVEL WITH FIN (Apprecia amount fines)	'Dirty	materials with excess of plas	tic fines, medium to high dry s	trength	GC	Clayey gravels, gravel-sand-clay mixtures	
COARSE GR erial less tha	fraction	CLEAN SANDS (Little or no fines)	Wide range	-	mounts of all intermediate sizes grains, no dry strength	s, not enough	sw	Well graded sands, gravelly sands, little or no fines	
CC of materia	SANDS More than 50% of coarse fraction is smaller than 2.36mm	CLEAN (Little fine	Predominar	antly one size or range of sizes with some intermediate sizes missing, not enough fines to bind coarse grains, no dry strength '				Poorly graded sands and gravelly sands; little or no fines, uniform sands	
than 50%	SAr than 50% smaller th	Sanaret u SANDS WITH FINES (Appreciable amount of fines)	Dirty' materials with excess of non-plastic fines, zero to medium dry strength				SM	Silty sands, sand-silt mixtures	
More	More	SANDS FIN (Appr amou	'Dirty	\mathbf{y}^{\prime} materials with excess of plastic fines, medium to high dry strength			SC	Clayey sands, sand-clay mixtures	
			IDENTIFICATIO	ON PROCEDURES ON FRACTI	ONS <0.2mm				
han			DRY STR	RENGTH	DILATANCY	TOUGHNESS			
FINE GRAINED SOILS material less than 63 mm is smaller than 0.075 mm	SILTS AND CLAYS Liquid limit less than 50	None t	to low	Quick to slow	None		ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with low plasticity. Silts of low to medium Liquid Limit.	
solLs an 63 mn m	SILTS AND CLAYS uid limit less than	Medium	to high	None to very slow	Medium		CL, CI	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays.	
FINE GRAINED SOILS material less than 63 0.075 mm	Lic	Li.	Low to	medium	Slow	Low		OL	Organic silts and organic silt-clays of low to medium plasticity.
oť	AYS er than	Low to	medium	Slow to none	Low to medium		МН	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, silts of high Liquid Limit.	
More than 50%	F More than 50% of n SILTS AND CLAYS Liquid limit greater than 50	High to v	very high	None	High		СН	Inorganic clays of high plasticity.	
M	Medium		to high	None to very slow	Low to medium		он	Organic clays of high plasticity	
HIGHLY OR	GANIC SOILS	Readily ide	entified by colo	ur, odour, spongy feel and fre	quently by fibrous texture	Pt	Pe	at and other highly organic soils	

PLASTICITY CHART



For laboratory classification of fine grained soils



PLASTICITY

DESCRIPTIVE TERM	OF LOW PLASTICITY	OF MEDIUM PLASTICITY	OF HIGH PLASTICITY
Range Of Liquid Limit (%)	≤ 35	> 35 ≤ 50	> 50

DESCRIPTION OF ORGANIC OR ARTIFICIAL MATERIALS

PREFERRED TERMS	SECONDARY DESCRIPTION
Organic Matter	Fibrous Peat/ Charcoal/ Wood Fragments/ Roots (greater than approximately 2mm diameter)/ Root Fibres (less than approximately 2mm diameter)
Waste Fill	Domestic Refuse/ Oil/ Bitumen/ Brickbats/ Concrete Rubble/ Fibrous Plaster/ Wood Pieces/ Wood Shavings/ Sawdust/ Iron Filings/ Drums/ Steel Bars/ Steel Scrap/ Bottles/ Broken Glass/ Leather

CONSISTENCY - Cohesive soils

TERM	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD
Symbol	VS	S	F	St	VSt	н
Undrained Shear Strength (kPa)	< 12	12 - 25	25 - 50	50 - 100	100 - 200	> 200
SPT (N) Blowcount	0 - 2	2 - 4	4 - 8	8 - 15	15 - 30	> 30
Field Guide	Exudes between the fingers when squeezed	Can be moulded by light finger pressure	Can be moulded by strong finger pressure	Cannot be moulded by fingers. Can be indented by thumb nail	Can be indented by thumb nail	Can be indented with difficulty with thumb nail

CONSISTENCY - Non-cohesive soils

TERM	VERY LOOSE	LOOSE	MEDIUM DENSE	DENSE	VERY DENSE	COMPACT
Symbol	VL	L	MD	D	VD	со
SPT (N) Blowcount	0 - 4	4 - 10	10 - 30	30 - 50	50 - 100	> 50/150 mm
Density Index (%)	< 15	15 - 35	35 - 65	65 - 85	85 - 95	> 95
Field Guide	Ravels	Shovels easily	Shovelling very difficult	Pick required	Pick difficult	Cannot be picked

MINOR COMPONENTS

TERM	TRACE	WITH
% Minor Component	Coarse grained soils: < 5%	Coarse grained soils: 5 - 12%
	Fine grained soils: <15%	Fine grained soils: 15 - 30%
Field Guide	Presence just detectable by feel or eye, but soil properties little	Presence easily detectable by feel or eye, soil properties
	or no different to general properties of primary components	little different to general properties of primary component



GEOLOGICAL ORIGIN

	TYPE	DETAILS
TRANSPORTED SOILS	Aeolian Soils	Deposited by wind
	Alluvial Soils	Deposited by streams and rivers
	Colluvial Soils	Deposited on slopes
	Lacustrine Soils	Deposited by lakes
	Marine Soils	Deposited in ocean, bays, beaches and estuaries
FILL MATERIALS	Soil Fill	Describe soil type, UCS symbol and add 'FILL'
	Rock Fill	Rock type, degree of weathering, and word 'FILL'.
	Domestic Fill	Percent soil or rock, whether pretrucible or not.
	Industrial Fill	Percent soil, whether contaminated, particle size & type of waste product, ie brick, concrete, metal

STRENGTH OF ROCK MATERIAL

TERM	SYMBOL	IS (50)	(MPA)	FIELD GUIDE TO STRENGTH
Extremely Low	EL	≤0.03		Easily remoulded by hand to a material with soil properties.
Very Low	VL	>0.03	≤0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxle sample by hand. Pieces up to 3 cm thick can be broken by finger pressure.
Low	L	>0.1	≤0.3	Easily scored with a knife; indentations 1 mm to 3 mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150 mm long by 50 mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.
Medium	Μ	>0.3	≤1.0	Readily scored with a knife; a piece of core 150 mm long by 50 mm diameter can be broken by hand with difficulty.
High	н	>1	≤3	A piece of core 150 mm long by 50 mm diameter cannot be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.
Very High	VH	>3	≤10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.
Extremely High	EH	>10		Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.

ROCK MATERIAL WEATHERING CLASSIFICATION

TERM	SYMBOL	DEFINITION
Residual Soil	RS	Soil developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported
Extremely Weathered Rock	XW	Rock is weathered to such an extent that it has 'soil' properties, i.e. it either disintegrates or can be remoulded, in water.
Distinctly Weathered Rock	DW	Rock strength usually changed by weathering. Rock may be highly discoloured, usually be iron staining. Porosity may be increased by leaching or may be decreased due to deposition of weathering products in pores.
Slightly Weathered Rock	SW	Rock is slightly discoloured but shows little or no change of strength from fresh rock.
Fresh Rock	FR	Rock shows no sign of decomposition or staining.

Appendix E

Laboratory results



CERTIFICATE OF ANALYSIS

Work Order	EP2107544	Page	: 1 of 4	
Client	: GHD PTY LTD	Laboratory	Environmental Division Perth	
Contact	: MS VICKI DAVIES	Contact	: Nick Courts	
Address	: 999 HAY STREET	Address	: 26 Rigali Way Wangara WA Australia 6065	
	PERTH WA, AUSTRALIA 6000			
Telephone	:	Telephone	: +61-8-9406 1301	
Project	: 12546218 Albany Motorsports Park DA	Date Samples Received	: 01-Jul-2021 13:30	
Order number	: 12546218	Date Analysis Commenced	: 02-Jul-2021	
C-O-C number	:	Issue Date	: 13-Jul-2021 13:47	NATA
Sampler	:		Hac-MRA	NATA
Site	:			
Quote number	: EP/444/21		The Column	Assessment and the same
No. of samples received	: 15		Accredi	Accreditation No. 825 ted for compliance with
No. of samples analysed	: 6			ISO/IEC 17025 - Testing

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with Quality Review and Sample Receipt Notification.

Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories	Position	Accreditation Category
Ankit Joshi	Inorganic Chemist	Sydney Inorganics, Smithfield, NSW
Chris Lemaitre	Laboratory Manager (Perth)	Perth Inorganics, Wangara, WA



General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contact for details.

Key: CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society. LOR = Limit of reporting

* = This result is computed from individual analyte detections at or above the level of reporting

ø = ALS is not NATA accredited for these tests.

 \sim = Indicates an estimated value.

- Phosphorus Sorption Index + Capacity conducted by ALS Sydney, NATA accreditation no. 825, site no 10911.
- ED007 and ED008: When Exchangeable AI is reported from these methods, it should be noted that Rayment & Lyons (2011) suggests Exchange Acidity by 1M KCI Method 15G1 (ED005) is a more suitable method for the determination of exchange acidity (H+ + AI3+).



Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)			Sample ID	TP1 - 900mm to 1100mm	TP2 - 500mm to 900mm	TP3 - 300mm to 600mm	TP4 - 400mm to 800mm	TP5 - 400mm to 800mm
	Sampling date / time			25-Jun-2021 00:00	25-Jun-2021 00:00	25-Jun-2021 00:00	25-Jun-2021 00:00	25-Jun-2021 00:00
Compound	CAS Number	LOR	Unit	EP2107544-002	EP2107544-003	EP2107544-005	EP2107544-008	EP2107544-011
				Result	Result	Result	Result	Result
EA002: pH 1:5 (Soils)								
pH Value		0.1	pH Unit	6.1	6.1	5.7	5.8	5.4
EA010: Conductivity (1:5)								
Electrical Conductivity @ 25°C		1	µS/cm	22	25	28	24	4
ED007: Exchangeable Cations								
Exchangeable Calcium		0.1	meq/100g	0.8	0.8	1.6	0.8	<0.1
Exchangeable Magnesium		0.1	meq/100g	0.5	1.0	0.2	0.2	<0.1
Exchangeable Potassium		0.1	meq/100g	<0.1	<0.1	<0.1	<0.1	<0.1
Exchangeable Sodium		0.1	meq/100g	<0.1	<0.1	0.1	<0.1	<0.1
Cation Exchange Capacity		0.1	meq/100g	1.4	1.9	2.0	1.1	0.1
Exchangeable Sodium Percent		0.1	%	5.8	4.8	5.7	6.2	<0.1
EK072: Phosphate Sorption Capacity								
Phosphate Sorption Capacity		250	mg P	688	1650	3660	3000	<250
			sorbed/kg					
Phosphate Sorption Index		1	mgkg-1/log10	60	157	289	244	<1
			ugL-1					



Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)					 	
(800mm		
		Sampli	ng date / time	25-Jun-2021 00:00	 	
Compound	CAS Number	LOR	Unit	EP2107544-013	 	
				Result	 	
EA002: pH 1:5 (Soils)						
pH Value		0.1	pH Unit	5.9	 	
EA010: Conductivity (1:5)						
Electrical Conductivity @ 25°C		1	μS/cm	20	 	
ED007: Exchangeable Cations						
Exchangeable Calcium		0.1	meq/100g	1.0	 	
Exchangeable Magnesium		0.1	meq/100g	0.2	 	
Exchangeable Potassium		0.1	meq/100g	<0.1	 	
Exchangeable Sodium		0.1	meq/100g	<0.1	 	
Cation Exchange Capacity		0.1	meq/100g	1.3	 	
Exchangeable Sodium Percent		0.1	%	1.4	 	
EK072: Phosphate Sorption Capacity						
Phosphate Sorption Capacity		250	mg P	966	 	
			sorbed/kg			
Phosphate Sorption Index		1	mgkg-1/log10	62	 	
			ugL-1			

Inter-Laboratory Testing Analysis conducted by ALS Sydney, NATA accreditation no. 825, site no. 10911 (Chemistry) 14913 (Biology).

(SOIL) EK072: Phosphate Sorption Capacity



QUALITY CONTROL REPORT

Work Order	: EP2107544	Page	: 1 of 3	
Client		Laboratory	: Environmental Division Pe	erth
Contact	: MS VICKI DAVIES	Contact	: Nick Courts	
Address	: 999 HAY STREET PERTH WA, AUSTRALIA 6000	Address	: 26 Rigali Way Wangara W	/A Australia 6065
Telephone	:	Telephone	: +61-8-9406 1301	
Project	: 12546218 Albany Motorsports Park DA	Date Samples Received	: 01-Jul-2021	
Order number	12546218	Date Analysis Commenced	: 02-Jul-2021	
C-O-C number	:	Issue Date	: 13-Jul-2021	NATA
Sampler	:			HAC-MRA NATA
Site	:			
Quote number	: EP/444/21			Accreditation No. 825
No. of samples received	: 15			Accredited for compliance with
No. of samples analysed	: 6			ISO/IEC 17025 - Testing

This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full.

This Quality Control Report contains the following information:

- Laboratory Duplicate (DUP) Report; Relative Percentage Difference (RPD) and Acceptance Limits
- Method Blank (MB) and Laboratory Control Spike (LCS) Report; Recovery and Acceptance Limits
- Matrix Spike (MS) Report; Recovery and Acceptance Limits

Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

Signatories	Position	Accreditation Category
Ankit Joshi	Inorganic Chemist	Sydney Inorganics, Smithfield, NSW
Chris Lemaitre	Laboratory Manager (Perth)	Perth Inorganics, Wangara, WA



General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis. Where the LOR of a reported result differs from standard LOR, this may be due to high

Key: Anonymous = Refers to samples which are not specifically part of this work order but formed part of the QC process lot

CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.

LOR = Limit of reporting

RPD = Relative Percentage Difference

= Indicates failed QC

Laboratory Duplicate (DUP) Report

The quality control term Laboratory Duplicate refers to a randomly selected intralaboratory split. Laboratory duplicates provide information regarding method precision and sample heterogeneity. The permitted ranges for the Relative Percent Deviation (RPD) of Laboratory Duplicates are specified in ALS Method QWI-EN/38 and are dependent on the magnitude of results in comparison to the level of reporting: Result < 10 times LOR: No Limit; Result between 10 and 20 times LOR: 0% - 50%; Result > 20 times LOR: 0% - 20%.

Sub-Matrix: SOIL						Laboratory	Duplicate (DUP) Report		
Laboratory sample ID	Sample ID	Method: Compound	CAS Number	LOR	Unit	Original Result	Duplicate Result	RPD (%)	Acceptable RPD (%)
EA002: pH 1:5 (Soils	s) (QC Lot: 3770355)								
EP2107544-002	TP1 - 900mm to 1100mm	EA002: pH Value		0.1	pH Unit	6.1	6.1	0.0	0% - 20%
EA010: Conductivity	y (1:5) (QC Lot: 3770356)								
EP2107544-002	TP1 - 900mm to 1100mm	EA010: Electrical Conductivity @ 25°C		1	µS/cm	22	22	0.0	0% - 20%
ED007: Exchangeat	le Cations (QC Lot: 378043	5)							
EP2107521-057	Anonymous	ED007: Exchangeable Sodium Percent		0.1	%	2.9	3.0	3.6	0% - 20%
		ED007: Exchangeable Calcium		0.1	meq/100g	16.8	14.7	13.3	0% - 20%
		ED007: Exchangeable Magnesium		0.1	meq/100g	0.4	0.4	0.0	No Limit
		ED007: Exchangeable Potassium		0.1	meq/100g	<0.1	<0.1	0.0	No Limit
		ED007: Exchangeable Sodium		0.1	meq/100g	0.5	0.5	0.0	No Limit
		ED007: Cation Exchange Capacity		0.1	meq/100g	17.8	15.6	13.1	0% - 20%
EK072: Phosphate	Sorption Capacity (QC Lot: 3	3776718)							
EP2107544-002	TP1 - 900mm to 1100mm	EK072: Phosphate Sorption Capacity		250	mg P sorbed/kg	688	409	50.9	No Limit
		EK072: Phosphate Sorption Index		1	mgkg-1/log10ug	60	60	0.0	0% - 20%
					L-1				



Method Blank (MB) and Laboratory Control Sample (LCS) Report

The quality control term Method / Laboratory Blank refers to an analyte free matrix to which all reagents are added in the same volumes or proportions as used in standard sample preparation. The purpose of this QC parameter is to monitor potential laboratory contamination. The quality control term Laboratory Control Sample (LCS) refers to a certified reference material, or a known interference free matrix spiked with target analytes. The purpose of this QC parameter is to monitor method precision and accuracy independent of sample matrix. Dynamic Recovery Limits are based on statistical evaluation of processed LCS.

Sub-Matrix: SOIL				Method Blank (MB)	Laboratory Control Spike (LCS) Report							
				Report	Spike	Spike Recovery (%)	Acceptable	e Limits (%)				
Method: Compound	CAS Number	LOR	Unit	Result	Concentration	LCS	Low	High				
EA002: pH 1:5 (Soils) (QCLot: 3770355)												
EA002: pH Value			pH Unit		4 pH Unit	100	70.0	130				
					7 pH Unit	100	70.0	130				
EA010: Conductivity (1:5) (QCLot: 3770356)												
EA010: Electrical Conductivity @ 25°C		1	μS/cm	<1	1412 µS/cm	99.6	93.6	106				
ED007: Exchangeable Cations (QCLot: 3780436)												
ED007: Exchangeable Calcium		0.1	meq/100g	<0.1	21.6 meq/100g	91.0	82.9	117				
ED007: Exchangeable Magnesium		0.1	meq/100g	<0.1	1.76 meq/100g	91.3	78.4	119				
ED007: Exchangeable Potassium		0.1	meq/100g	<0.1	1 meq/100g	107	87.9	129				
ED007: Exchangeable Sodium		0.1	meq/100g	<0.1	0.9 meq/100g	103	92.9	132				
ED007: Cation Exchange Capacity		0.1	meq/100g	<0.1	25.3 meq/100g	92.0	84.7	117				
ED007: Exchangeable Sodium Percent		0.1	%	<0.1								

Matrix Spike (MS) Report

The quality control term Matrix Spike (MS) refers to an intralaboratory split sample spiked with a representative set of target analytes. The purpose of this QC parameter is to monitor potential matrix effects on analyte recoveries. Static Recovery Limits as per laboratory Data Quality Objectives (DQOs). Ideal recovery ranges stated may be waived in the event of sample matrix interference.

• No Matrix Spike (MS) or Matrix Spike Duplicate (MSD) Results are required to be reported.



QA/QC Compliance Assessment to assist with Quality Review										
Work Order	: EP2107544	Page	: 1 of 4							
Client		Laboratory	: Environmental Division Perth							
Contact	: MS VICKI DAVIES	Telephone	: +61-8-9406 1301							
Project	: 12546218 Albany Motorsports Park DA	Date Samples Received	: 01-Jul-2021							
Site	·	Issue Date	: 13-Jul-2021							
Sampler	:	No. of samples received	: 15							
Order number	: 12546218	No. of samples analysed	: 6							

This report is automatically generated by the ALS LIMS through interpretation of the ALS Quality Control Report and several Quality Assurance parameters measured by ALS. This automated reporting highlights any non-conformances, facilitates faster and more accurate data validation and is designed to assist internal expert and external Auditor review. Many components of this report contribute to the overall DQO assessment and reporting for guideline compliance.

Brief method summaries and references are also provided to assist in traceability.

Summary of Outliers

Outliers : Quality Control Samples

This report highlights outliers flagged in the Quality Control (QC) Report.

- <u>NO</u> Method Blank value outliers occur.
- <u>NO</u> Duplicate outliers occur.
- <u>NO</u> Laboratory Control outliers occur.
- <u>NO</u> Matrix Spike outliers occur.
- For all regular sample matrices, <u>NO</u> surrogate recovery outliers occur.

Outliers : Analysis Holding Time Compliance

• <u>NO</u> Analysis Holding Time Outliers exist.

Outliers : Frequency of Quality Control Samples

• <u>NO</u> Quality Control Sample Frequency Outliers exist.



Analysis Holding Time Compliance

If samples are identified below as having been analysed or extracted outside of recommended holding times, this should be taken into consideration when interpreting results.

This report summarizes extraction / preparation and analysis times and compares each with ALS recommended holding times (referencing USEPA SW 846, APHA, AS and NEPM) based on the sample container provided. Dates reported represent first date of extraction or analysis and preclude subsequent dilutions and reruns. A listing of breaches (if any) is provided herein.

Holding time for leachate methods (e.g. TCLP) vary according to the analytes reported. Assessment compares the leach date with the shortest analyte holding time for the equivalent soil method. These are: organics 14 days, mercury 28 days & other metals 180 days. A recorded breach does not guarantee a breach for all non-volatile parameters.

Holding times for VOC in soils vary according to analytes of interest. Vinyl Chloride and Styrene holding time is 7 days; others 14 days. A recorded breach does not guarantee a breach for all VOC analytes and should be verified in case the reported breach is a false positive or Vinyl Chloride and Styrene are not key analytes of interest/concern.

Evaluation: × = Holding time breach ; <	<pre>(= V</pre>	Vithin holdin	g time.
---	------------------	---------------	---------

Matrix: SOIL					Evaluation	: × = Holding time	e breach ; ✓ = Withi	n holding tim
Method		Sample Date	Ex	traction / Preparation			Analysis	
Container / Client Sample ID(s)			Date extracted	Due for extraction	Evaluation	Date analysed	Due for analysis	Evaluation
EA002: pH 1:5 (Soils)								
Snap Lock Bag (EA002)								
TP3 - 300mm to 600mm,	TP4 - 400mm to 800mm,	25-Jun-2021	02-Jul-2021	02-Jul-2021	1	02-Jul-2021	02-Jul-2021	✓
TP5 - 400mm to 800mm,	TP6 - 500mm to 800mm							
Soil Glass Jar - Unpreserved (EA002)								
TP1 - 900mm to 1100mm,	TP2 - 500mm to 900mm	25-Jun-2021	02-Jul-2021	02-Jul-2021	✓	02-Jul-2021	02-Jul-2021	✓
EA010: Conductivity (1:5)								
Snap Lock Bag (EA010)								
TP3 - 300mm to 600mm,	TP4 - 400mm to 800mm,	25-Jun-2021	02-Jul-2021	02-Jul-2021	1	02-Jul-2021	30-Jul-2021	✓
TP5 - 400mm to 800mm,	TP6 - 500mm to 800mm							
Soil Glass Jar - Unpreserved (EA010)								
TP1 - 900mm to 1100mm,	TP2 - 500mm to 900mm	25-Jun-2021	02-Jul-2021	02-Jul-2021	1	02-Jul-2021	30-Jul-2021	✓
ED007: Exchangeable Cations								
Snap Lock Bag (ED007)								
TP3 - 300mm to 600mm,	TP4 - 400mm to 800mm,	25-Jun-2021	08-Jul-2021	23-Jul-2021	1	08-Jul-2021	23-Jul-2021	✓
TP5 - 400mm to 800mm,	TP6 - 500mm to 800mm							
Soil Glass Jar - Unpreserved (ED007)								
TP1 - 900mm to 1100mm,	TP2 - 500mm to 900mm	25-Jun-2021	08-Jul-2021	23-Jul-2021	✓	08-Jul-2021	23-Jul-2021	✓
EK072: Phosphate Sorption Capacity								
Soil Glass Jar - Unpreserved (EK072)								
TP1 - 900mm to 1100mm,	TP2 - 500mm to 900mm,	25-Jun-2021				06-Jul-2021	22-Dec-2021	✓
TP3 - 300mm to 600mm,	TP4 - 400mm to 800mm,							
TP5 - 400mm to 800mm,	TP6 - 500mm to 800mm							



Quality Control Parameter Frequency Compliance

The following report summarises the frequency of laboratory QC samples analysed within the analytical lot(s) in which the submitted sample(s) was(were) processed. Actual rate should be greater than or equal to the expected rate. A listing of breaches is provided in the Summary of Outliers.

trix: SOIL Evaluation: × = Quality Control frequency not within specification ; ✓ = Quality Control frequency within specification										
Quality Control Sample Type			ount		Rate (%)		Quality Control Specification			
Analytical Methods	Method	OC	Reaular	Actual	Expected	Evaluation				
Laboratory Duplicates (DUP)										
Electrical Conductivity (1:5)	EA010	1	6	16.67	10.00	✓	NEPM 2013 B3 & ALS QC Standard			
Exchangeable Cations	ED007	1	8	12.50	10.00	✓	NEPM 2013 B3 & ALS QC Standard			
P Sorption Index & P Sorption Capacity	EK072	1	6	16.67	10.00	✓	NEPM 2013 B3 & ALS QC Standard			
pH (1:5)	EA002	1	6	16.67	10.00	1	NEPM 2013 B3 & ALS QC Standard			
Laboratory Control Samples (LCS)										
Electrical Conductivity (1:5)	EA010	1	6	16.67	5.00	✓	NEPM 2013 B3 & ALS QC Standard			
Exchangeable Cations	ED007	1	8	12.50	5.00	✓	NEPM 2013 B3 & ALS QC Standard			
pH (1:5)	EA002	2	6	33.33	10.00	✓	NEPM 2013 B3 & ALS QC Standard			
Method Blanks (MB)										
Electrical Conductivity (1:5)	EA010	1	6	16.67	5.00	✓	NEPM 2013 B3 & ALS QC Standard			
Exchangeable Cations	ED007	1	8	12.50	5.00	✓	NEPM 2013 B3 & ALS QC Standard			



Brief Method Summaries

The analytical procedures used by the Environmental Division have been developed from established internationally recognized procedures such as those published by the US EPA, APHA, AS and NEPM. In house developed procedures are employed in the absence of documented standards or by client request. The following report provides brief descriptions of the analytical procedures employed for results reported in the Certificate of Analysis. Sources from which ALS methods have been developed are provided within the Method Descriptions.

Analytical Methods	Method	Matrix	Method Descriptions
рН (1:5)	EA002	SOIL	In house: Referenced to Rayment and Lyons 4A1 and APHA 4500H+. pH is determined on soil samples after a 1:5 soil/water leach. This method is compliant with NEPM Schedule B(3).
Electrical Conductivity (1:5)	EA010	SOIL	In house: Referenced to Rayment and Lyons 3A1 and APHA 2510. Conductivity is determined on soil samples using a 1:5 soil/water leach. This method is compliant with NEPM Schedule B(3).
Exchangeable Cations	ED007	SOIL	In house: Referenced to Rayment & Lyons Method 15A1. Cations are exchanged from the sample by contact with Ammonium Chloride. They are then quantitated in the final solution by ICPAES and reported as meq/100g of original soil. This method is compliant with NEPM Schedule B(3).
P Sorption Index & P Sorption Capacity	EK072	SOIL	In house: Referenced to Rayment & Lyons Method 9H1 & 9I1 Soil is bought to equilibrium with a solution of P at known concentration. P absorbed, released is determined by FIA analysis of the final solution.
Preparation Methods	Method	Matrix	Method Descriptions
Exchangeable Cations Preparation Method	ED007PR	SOIL	In house: Referenced to Rayment & Lyons method 15A1. A 1M NH4Cl extraction by end over end tumbling at a ratio of 1:20. There is no pretreatment for soluble salts. Extracts can be run by ICP for cations.
1:5 solid / water leach for soluble analytes	EN34	SOIL	10 g of soil is mixed with 50 mL of reagent grade water and tumbled end over end for 1 hour. Water soluble salts are leached from the soil by the continuous suspension. Samples are settled and the water filtered off for analysis.

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ob Manager (Invoice) /icki.Davies@ghd.com & GHD accounts		Email Address (Res Vicki.Davies@ghd.c		Sample Matrix 5-Soil/ Sludge/ W-Water/ A-Air	Type B-Bottle/J-Jar/V- Mal/Bag/G-Glass/P-Mastic	NO3/Other		fotal Volume (mL)	(1:5)	CEC/ Exchangeabe Cations (ED007) - Default Parameters	Index & P apacity		E								
Sample ID L	aboratory Sample ID	Date	Time	Sample N sludge/ w-w	Type B-Bottle/J-Jar/V- Vlai/Bag/G-Glass/P-Plas	Preservative Unpre HCI/ H2SO4/HNO3/Othe	No	Total Vol	pH plus EC (1:5)	CEC/ Exchi (ED007) - I Parameter	P Sorption Index & P Sorption Capacity								НОГВ		
P1 - 180mm to 490mm	Í	25/06/2021		s															~		
P1 - 900mm to 1100mm	2	25/06/2021		s					~	~	~										
P2 - 500mm to 900mm	3	25/06/2021		s					~	~	•								_	 	
P2 - 1700mm to 2000mm	4	25/06/2021		s															~		
P3 - 300mm to 600mm	5	25/06/2021		s					~	~	~										
P3- 900mm to 1200mm	6	25/06/2021		s															-		
P3 - 1600mm to 2000mm	7	25/06/2021		s													_		~		
P4 - 400mm to 800mm	8	25/06/2021		s					~	~	~		_								
P4 - 1350mm to 1650mm	9	25/06/2021		\$													_		~		
P4 - 1800mm to 2200mm	10	25/06/2021		s															~		_
P5 - 400mm to 800mm	11	25/06/2021		s					•	•	~										
P5 - 1200mm to 1500mm	12	25/06/2021		° S						-									~		_
P6 - 500mm to 800mm	13	25/06/2021	-	ŝ					~	~	~										
P6 - 1300mm to 1600mm	14	25/06/2021		S															-	,	En
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Environmental Division Perth Work Order Reference EP2107544



Telephone : -- 61-8-9406 1301

Appendix F

Aquarius Wastewater Systems Pty Ltd

AQUARIUS[®] Systems

1 – 5 Bedrooms	O-3 ATU	O-2 NR ATU	O-2 ATU								
6 – 9 Bedrooms	O-3 3KL ATU	O-2 NR 3KL ATU	O-2 3KL ATU								
Commercial	AQUARIUS [®] Standa	rd or Custom Designed	Commercial Systems								
Commercial	Please speak to our Sales Consultant										

Specifications

	0-3	O-2 NR	0-2
System Features			
Poly/Duralen Plastic or Concrete Tank Construction	\checkmark	\checkmark	\checkmark
Nutrient Retentive (Phosphorous removal)	\checkmark	\checkmark	
Ozone Disinfection	\checkmark		
Recycles all wastewater through irrigation into gardens, orchards, etc.	\checkmark	~	\checkmark
Supplied complete with irrigation components, electrical components and pumps	\checkmark	~	\checkmark
Footprint required approx 6m x 2.5m x 2m**	\checkmark	\checkmark	\checkmark
Low Energy use	\checkmark	\checkmark	\checkmark
Irrigation Area Above Ground Dripper Irrigation	√		
Sub-Surface Dripper Irrigation	\checkmark	\checkmark	\checkmark
Irrigation area in sandy soil conditions – $*150m^2$	\checkmark	\checkmark	\checkmark
Other Disposal options			
Leach Drains / Soakwells / Aquasafe Drains	\checkmark	\checkmark	\checkmark
Maintenance			
Service calls per year as per DoH WA requirements	2	2	2
Manufacturers Warranties			
Poly/Duralen Plastic Tanks 15 years	\checkmark	\checkmark	\checkmark
Orange Pumps 1 year	\checkmark	\checkmark	\checkmark
Irrigation and Electrical components 1 year	\checkmark	\checkmark	\checkmark
Approvals			
Fully approved by the WA Department of Health	\checkmark	\checkmark	\checkmark
Australian Standards approved AS/NZS 1546.3	\checkmark	\checkmark	\checkmark
Why choose Aquarius			
Wholly owned West Australian Company	\checkmark	\checkmark	\checkmark
Manufactured in Western Australia	\checkmark	\checkmark	\checkmark
Extensive Support Network covering all of WA	\checkmark	\checkmark	\checkmark
Local Agents fully trained and registered with Department of Health WA	\checkmark	✓	\checkmark
*Subject to local authority approval		<u> </u>	

*Subject to local authority approval

**Subject to configuration of ATU

Treatment Process

	0-3	O-2 NR	0-2
Primary Tank			
Retains the solids and uses aerobic and anaerobic			
bacteria to breakdown the BOD_5 levels in the	\checkmark	\checkmark	\checkmark
sewage.			
Alum Tank			
Doses the Clarifying chamber of the Treatment tank			
with Alum. Alum acts as a flocculent to remove the	.(
nutrients and suspended solids and settle them to	v	v	
the bottom of the tank for further aerobic bacteria			
breakdown.			
Treatment Tank			
Secondary / Aeration Chamber			
Incorporates aeration to further break down BOD_5	\checkmark	\checkmark	\checkmark
and nitrates.			
Clarifying Chamber			
The Clarifying Chamber provides a settling and			
clarifying period for the water prior to discharge.	\checkmark	\checkmark	\checkmark
Discharge Chamber			
The Discharge chamber contains the Discharge			
Pump to pump the treated water out to irrigation or	,		,
other disposal methods.	\checkmark	\checkmark	\checkmark
Ozonation Pump			
Ozone is a powerful disinfectant, many times more	\checkmark		
effective than chlorine and kills all bacteria.	V		
DoH WA ATU Water Quality Criteria			
<20mg/L BOD ₅	\checkmark	\checkmark	\checkmark
<30mg/L suspended solids	√	\checkmark	\checkmark
<10 E.coli/100ml	\checkmark		
>3mg/L Ozone concentration	\checkmark		
<1mg/L (98.5%) TP (% removal)	\checkmark	\checkmark	
<10mg/L (97.8%) TN (% removal)	✓	\checkmark	\checkmark



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