



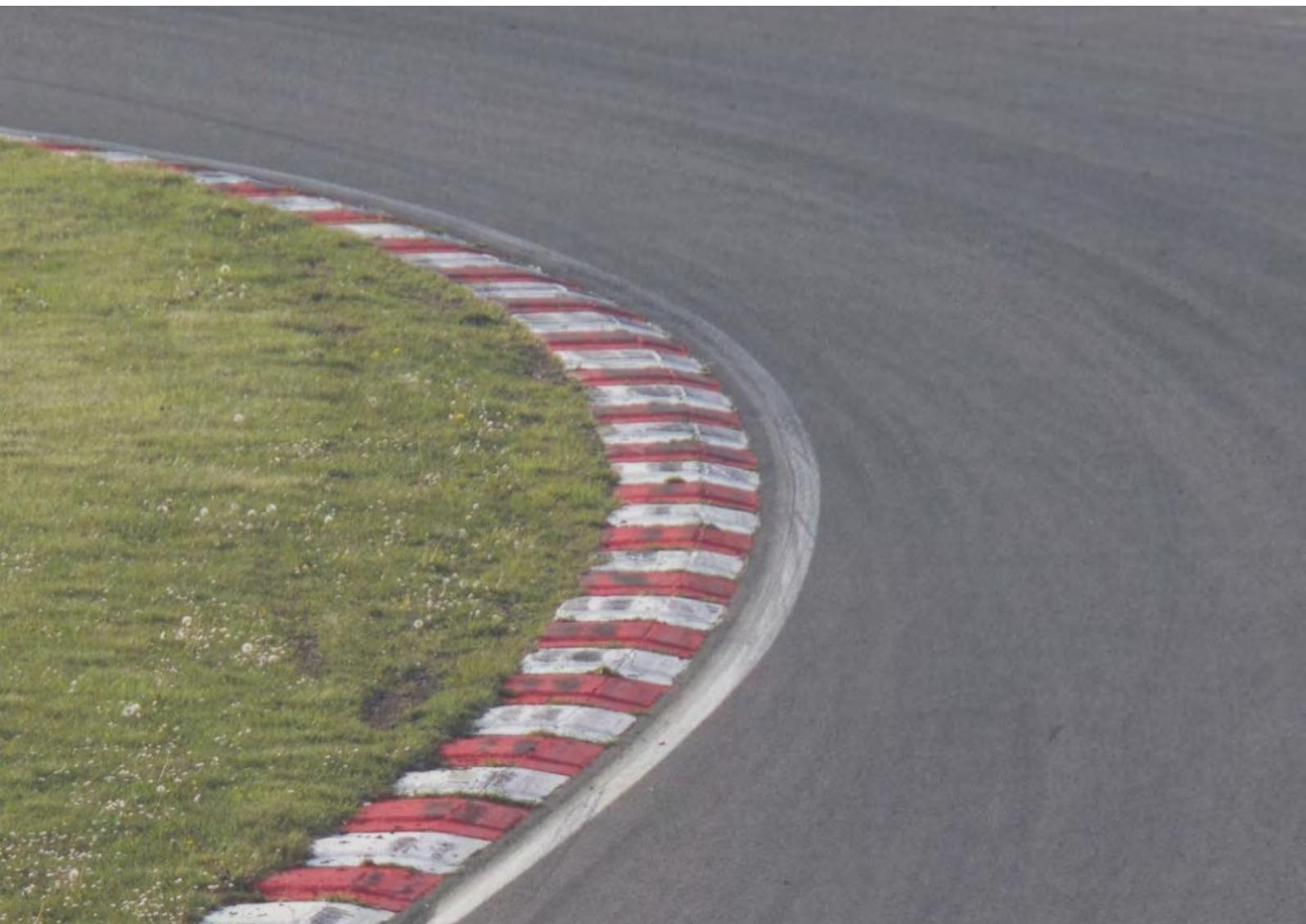
# Albany Motorsport Park – Development Application

## Water Management Plan

City of Albany

16 August 2021

→ **The Power of Commitment**



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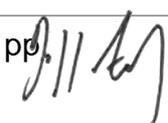
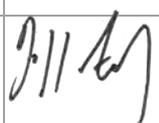
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# Abbreviations

Term	Definition
AHD	Australian Height Datum
AMP	Albany Motorsport Park
AMV Inc.	Albany Motorsport Venue Incorporated
ASS	Acid Sulfate Soil
ATV	All-terrain vehicle
BGL	Below ground level
BMP	Best management practices
BoM	Bureau of Meteorology
CAMS	Confederation of Australian Motor Sport Limited
CEMP	Construction Environmental Management Plan
CEO	Chief Executive Officer
CoA	City of Albany
DPIRD	Department of Primary Industries and Regional Development
DPLH	Department of Planning, Lands and Heritage
DWER	Department of Water and Environmental Regulation
EMP	Environmental Management Plan
ESA	Environmentally Sensitive Areas
FIA	Federation Internationale de l'Automobile
FIM	Federation Internationale Motocyclisme
GIS	Geographic information system
GoWA	Government of Western Australia
GSMG	Great Southern Motorplex Group Inc.
JDAP	Joint Development Assessment Panel
LGA	Local Government Area
LWMS	Local Water Management Strategy
LGSTWSS	Lower Great Southern Towns Water Supply Scheme
MA	Motorcycling Australia
PDWSA	Public drinking water source area
RIWI Act	<i>Rights in Water and Irrigation Act 1914</i>
SMP	Stormwater Management Plan
TN	Total Nitrogen
TP	Total Phosphorus
WQPN	Water quality protection note
WSUD	Water sensitive urban design
4WD	Four-wheel drive

# 1. Introduction

## 1.1 Project description

The City of Albany (CoA) has engaged GHD Pty Ltd (GHD) to prepare an Application for Planning Approval for the staged construction of the Albany Motorsport Park (AMP) at Lot 5780 (No. 54) Down Road South, Drome (the Site) (Figure 1, Appendix A). The project Proponent is the Great Southern Motorplex Group Inc. (GSMG).

At full development, the proposed AMP will consist of:

- Sealed, configurable multi-use track (3.5 km long × 12 m wide) for motor car racing, motorcycle racing, drifting, driver training and cycling:
  - Designed to comply with Motorsport Australia *Track Operator's Safety Guide*<sup>1</sup> and Motorcycling Australia (MA) *Track Guidelines*<sup>2</sup>.
  - To be licensed by Motorsport Australia for Fédération Internationalé de l'Automobile (FIA) Grade 2 and Fédération Internationalé Motocyclisme (FIM) Grade B (i.e. up to second-tier international motor racing).
- A motocross circuit designed and constructed in association with MA guidelines.
- An off-road four wheel drive (4WD) and all-terrain vehicle (ATV) training area.
- Associated buildings and infrastructure.

Due to the scale and nature of the complex, the works have been broken down into two key stages which comprise of the following:

- Stage 1 (this Development Application):
  - Stage 1A: Construction of motocross track, 4WD driver training area, all-terrain vehicle (ATV) area and associated infrastructure.
  - Stage 1B: Construction of racetrack and associated infrastructure (subject to funding).
- Future Development: Construction and replacement of final permanent structures to support the function of the motorsports complex (subject to funding). Stage 2 will be addressed as a separate Development Application.

A Master Plan, which illustrates the various aspects of the Site and staging areas, has been developed by the GSMG and CoA to support the Development Application for the AMP (Figure 2, Appendix A).

Once operational the AMP will be operated by Albany Motorsport Venue Incorporated (AMV Inc.).

## 1.2 Site location

Lot 5780 Down Road South, Drome is located approximately 20 km to the north of the Albany CBD and is 192.34 ha in size. The AMP comprises 141.7 ha (including 0.2 ha for crossovers) in the eastern portion of the Site. Two areas within Lot 5780 are excluded from the AMP development and include 49.47 ha at the western end of the Site which is covered with native vegetation and a dam area (1.37 ha) on the northern boundary which is subleased to Plantation Energy.

The site is zoned 'Special Use – SU26' under City of Albany Local Planning Scheme No. 1.

The Site is bounded by Down Road West to the north, Down Road South to the east, Lot 5781 Down Road South to the south (privately owned) and a local road reserve and the Avon-Albany rail reserve to the west. The Site is located adjacent to the Mirambeena Timber Processing Precinct and sits within the industrial buffer area.

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<sup>1</sup> CAMS. (2012). *Track Operator's Safety Guide*. Malvern East: Confederation of Australian Motor Sports.

<sup>2</sup> MA. (2011). *Track Guidelines*. South Melbourne: Motorcycling Australia.

## 1.3 Purpose of this report

This Water Management Plan (WMP) has been prepared to support the Application for Planning Approval. The WMP identifies the principles, criteria and water management strategies to manage water across the Site during construction and operational phases.

## 1.4 Albany Motorsport Park design

### 1.4.1 Events and usage

For the purposes of sizing facilities and infrastructure GSMG have provided conceptual usage of the AMP, with an assumed typical /frequent site attendance of 300 persons for the Motocross Precinct and 500 persons for the Race Track Precinct (i.e. competitors + officials + spectators). This was determined through discussion with the GSMG on the nature and size of expected typical events. For special events that anticipate a greater number of site attendees, additional water servicing management measures will need to be implemented (e.g. drinking water carts, port-a-loos).

### 1.4.2 Elements of AMP design

Key elements of the track design and consideration for Water Sensitive Urban Design (WSUD) are summarised in Table 1.

Table 1 Key AMP design elements and WSUD considerations

Track element	Description	WSUD considerations
AMP facilities	Includes the following: <ul style="list-style-type: none"> <li>– Facility buildings (clubrooms, first aid, toilets, storage sheds)</li> <li>– Carpark (competitor and spectator)</li> <li>– Pit and garage areas</li> <li>– Refueling area</li> </ul>	Considered impervious areas contributing surface runoff. To be protected from flood events. Pit and garage areas and refueling areas are key water quality treatment areas.
Access roads	Entry and exit roads consisting of 7 m wide gravel road, with 2 m wide grassed verges either side.	Road and verge have limited permeability.
Overflow parking	Grassed overflow parking	Considered pervious.
Race Track pavement	The Race Track pavement consists of 12 m wide track.	Considered impervious areas contributing surface runoff.
Race Track verge	The Race Track verge is predominantly grass and gravel with limited asphalt on T11.(recovery area)	Gravel verge is considered permeable.
Run-off areas	Run-off areas occur around the Race Track to enable drivers to dissipate speed during a race. Run-off areas are composed of loose gravel underlain by compacted pavement material.	Pavement layer underneath is considered impervious.
Motocross Track	Compacted clay and sand Motocross track.	Limited permeability.
4WD Driver Training and ATV Precinct	4WD and ATV area comprises finished natural surface after removal of some gravel, sand and clay to build the Motocross track.	Limited permeability.

## 1.5 Previous studies

Numerous studies and investigations have been undertaken to support development planning for the Albany Motorsports Complex. A summary of key documents of relevance to integrated water management of the Site is provided below:

- **Pavement Investigation Report 4212/1 Albany Motorsport Park Development** (Great Southern Geotechnics , 2021)
  - A geotechnical investigation was completed for the proposed Albany Motorsport Park Development including assessment of soil types and profiles, characteristics of selected soil samples and completion of in-situ permeability testing at selected locations.
- **Albany Motorsport Park Local Water Management Strategy** (GHD, 2021)
  - A Local Water Management Strategy (LWMS) was prepared (as part of the Scheme Amendment) that identified the key water management principles, design criteria, and strategies for the proposed development of the Albany Motorsport Park. The water management strategies in the LWMS were developed with reference to the concept track design and with regard to the site characteristics.
- **Albany Motorsport Park Site Feasibility Study – Lot 5780 Down Road South, Drome** (GHD, 2018)
  - A site feasibility assessment was completed as part of preliminary planning investigations for the proposed Albany Motorsport Park. The feasibility assessment included a range of desktop technical investigations including review of servicing requirements and traffic impact assessment, and desktop geotechnical, hydrogeological, noise and water management planning. The feasibility assessment further included a preliminary risk assessment of the key issues identified and identified a suite of recommended remedial actions based on a hierarchy of controls. A number of recommended remedial and control actions were outlined to provide guidance for the various stages of the development.
- **Albany hinterland prospective groundwater resources map; Explanatory notes** (DWER, 2017)
  - Hydrogeological report and map for the Albany hinterland developed by the Department of Water and Environmental Regulation (DWER) as part of the Royalties for Regions South Coast Groundwater Investigation project. The Albany hinterland area in the South Coast is known as an important resource for water supply in the Great Southern region. In 2013, DWER undertook some hydrogeological (surface water and groundwater) investigations (as part of South Coast groundwater investigation by Western Australian Government on groundwater availability) and mapped prospective groundwater resources in the Albany hinterland region in order to support regional developments.
  - The report and map were used to develop a conceptual hydrogeological model for the Site as part of the LWMS, in order to understand the groundwater and surface water sources and pathways.
- **Motorplex Development, Down Road Surface and Groundwater Monitoring 2018 Summary Report** (Bio Diverse Solutions, 2018)
  - Summary reporting of shallow groundwater monitoring bore monitoring program. Monitoring of shallow groundwater bores installed across the Site commenced in February 2018. The 2018 report summarises preliminary results for the 2018 monitoring period, with additional monitoring completed up to November 2019 which were included in the LWMS.
- **Proposed Motorsport Park, Lot 5780 Down Road, Drome Reconnaissance Flora and Level 1 Fauna Survey Report** (Bio Diverse Solutions, 2019)
  - Bio Diverse Solutions completed a desktop assessment and reconnaissance flora survey and Level 1 Fauna survey of the Project Site in Spring 2018. The survey included identification of habitat trees and threatened fauna dependent hollows, and mapping of vegetation communities (GIS mapping, vegetation condition mapping, fauna habitat types and condition).

## **1.6 Scope and limitations**

This report: has been prepared by GHD for City of Albany and may only be used and relied on by City of Albany for the purpose agreed between GHD and City of Albany as set out in section 1.3 of this report. GHD otherwise disclaims responsibility to any person other than City of Albany arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

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## 2. Existing environment

This section summarises key information relating to catchment characteristics for the Site. The LWMS (GHD, 2021) provides a comprehensive overview of environmental characteristics.

### 2.1 Existing activities

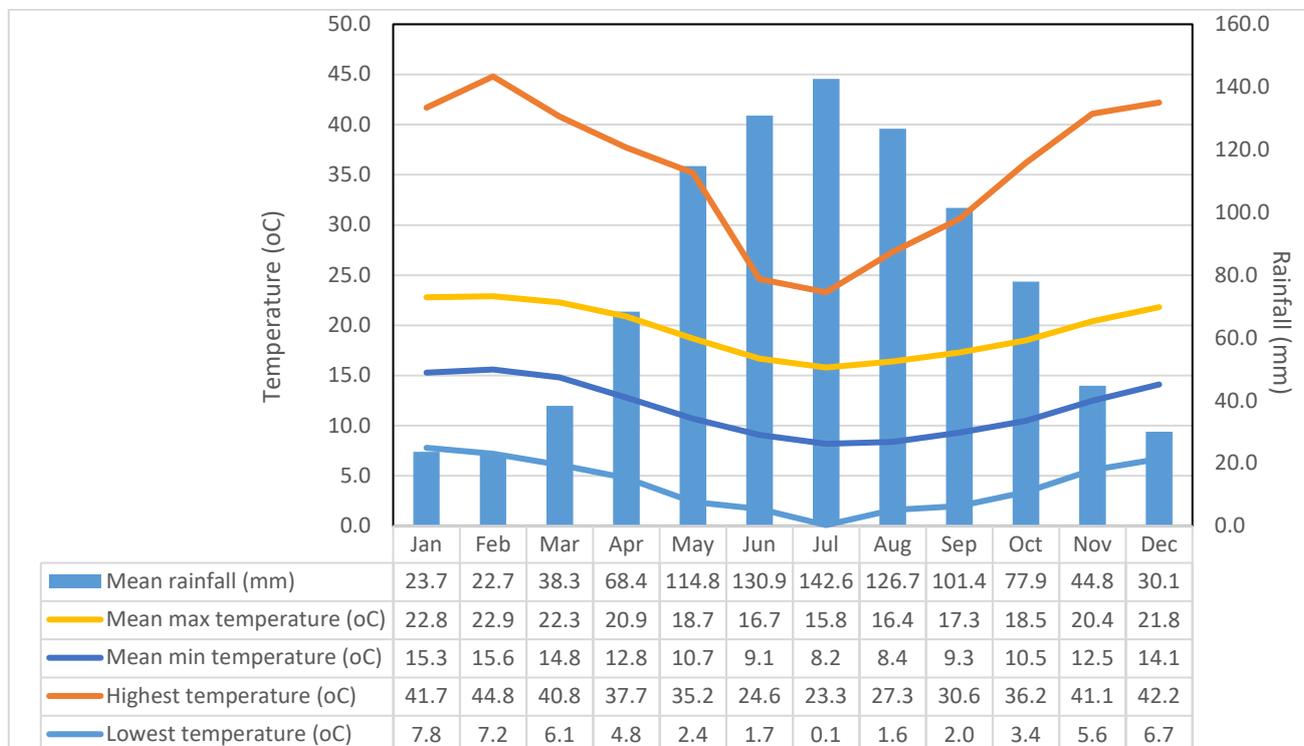
The perimeter of the site is entirely fenced and is currently used for the primary purpose of cattle grazing. Historically the site is likely to also have been used mainly for the purpose of agriculture, as well as some limited resource extraction (sand and gravel). The western end of the site consists of 52 ha of native vegetation that will be retained. A number of small dams are located across the site for stock watering. These will be retained and maintained for the AMP.

### 2.2 Climate

Albany is located on the south coast of Western Australia and the climate is broadly described as Mediterranean, with warm dry summers and mild wet winters. The nearest Bureau of Meteorology (BoM) official recording station is Albany Airport (Station No. 9500). This station records temperature, rainfall, relative humidity, wind speed and direction and has data available dating back to 1877. Table 2 illustrates recorded average monthly meteorological data for the Bunbury AWS BoM station for years 1877 to 2020 (BoM, 2020).

Temperatures range from a mean maximum of 22.9 °C in summer and drop to a mean maximum of 15.8 °C in winter. Mean minimum temperatures follow a similar trend, reaching 15.6 °C in summer and 8.2 °C in winter. Rainfall is low throughout the summer months and peaks in July, with a monthly average of 142.6 mm. The mean annual rainfall is 925.2 mm, with approximately 103.1 rain days a year. Relative humidity at Albany reflects the Mediterranean climate, demonstrating drier summers and a comparatively high relative humidity of 82 % in the morning in winter (BoM, 2020).

**Table 2** Mean rainfall and temperatures in the Albany region (Site No. 9500) (BoM, 2020)



## 2.3 Topography, landform and soils

### 2.3.1 Topography

The surface elevation of the site ranges from approximately 41 m AHD to 73 m AHD (GoWA, 2021). The lowest elevation is on the southern boundary and extends through the center of the site within a gully (a tributary to Marbelup Brook) that lies in a north-easterly direction. The highest elevation occurs on the eastern boundary of the site.

### 2.3.2 Surface soils and geology

Regional geology is described with reference to the 1:50,000 Environmental Geology series map (Albany sheet) and the 1:250,000 Geological Series map (Mt Barker – Albany sheet). These indicate the site is underlain by Cainozoic sand of colluvial origin – “Qc: *Colluvium – Sand, silt and clay*” on the slopes and within the low-lying areas of the Marbelup Brook “QA – *Clay, silt, sand and gravel in watercourses*” (Allen & Sofoulis, 1984). The sand is described as pale grey, fine to coarse, angular to sub-rounded quartz that is loose and moderately sorted and contains occasional pebbles of laterite. The thickness of the sand unit is not indicated on the maps, however the 1:250,000 map sheet indicates sand unit generally overlays laterite.

Local soils and geology are further delineated by Department of Primary Industries and Regional Development (DPIRD) Soil Landscape Mapping as summarized in Table 3 and presented in Figure 3 (Appendix A).

Site investigations were completed by Great Southern Geotechnics across the site in March 2021 to assess soil types and profiles and in-situ permeability. Eight test pits were completed, with soil types typically in agreement with DPIRD Soil Landscape Mapping. Gravels were identified on the western slope in the vicinity of the 4WD Driver Training and ATV Area, and deep sands present on the valley slopes and duplex soils in the valley floors.

In-situ soil permeability testing was completed for test pit locations TP4 to TP8, with saturated hydraulic conductivity ranging between 0.41 m/day (TP8) and 3.29 m/day (TP6 and TP7).

The locations of the test pits, soil logs and soil permeability results provided in Appendix B.

**Table 3** Soil map units within the Project Site (GoWA, 2021)

Map unit symbol	Name	Landform	Geology	Soil
242KgDMc	Dempster Crest phase	Broad convex crests of sandy and lateritic spurs and ridges	Deeply weathered siltstone	Duplex sandy gravels; Grey deep sandy duplexes; Pale deep sand; Shallow gravels
242KgS7f	Minor Valleys S7 floor phase	Foot slopes and swampy valley floors of minor valleys	Colluvial and alluvial deposits over weathered sedimentary rocks	Wet and semi-wet soils; Pale deep sands; Grey deep sandy duplexes
242KgS7h	Minor Valleys S7 slope phase	Side slopes of minor valleys	Colluvium sedimentary rocks	Pale deep sands; Grey deep sandy duplexes
242ReDMc	Dempster Crest phase	Elongate crests	No information recorded	Sands and laterite

### 2.3.3 Acid sulfate soils risk mapping

An overlay of the site onto the DWER ASS risk mapping for the Albany-Torbay region (GoWA, 2021) is presented as Figure 4 (Appendix A), which identifies that the site is located outside of the boundary extent of the mapped areas.

Given that tributaries of Marbelup Brook located approximately 750 m to the south of the site are mapped as “Moderate to Low Risk” of ASS occurring, GHD has inferred that where these tributaries of Marbelup Brook extend into the site that they would also be considered to represent the same level of ASS risk. This is also consistent with the more broadly mapped risk areas where there are obvious low lying drainage lines, creeks and tributaries.

To more accurately inform the ASS risk onsite, a preliminary ASS investigation was completed as part of the onsite geotechnical investigation undertaken by Great Southern Geotechnics on 25 March 2021. Based on the ASS assessments to date, inorganic sulfidic sources capable of rapid acid release upon disturbance were not observed. Other, more slow releasing acidity sources were observed in the ASS assessment and will require management if disturbed in volumes greater than 100 m<sup>3</sup>.

Any impacts associated with dewatering (if required) during construction will need to be considered in the ASS management plan. Further detail is captured in the associated AMP Environmental Management Plan.

## 2.4 Hydrology

A summary of desktop searches related to hydrology datasets is provided in Table 4. Further detail is provided in the following sections where relevant.

Table 4 Summary of hydrology dataset queries within the Project Site

Dataset	Details	Result
Public Drinking Water Source Areas (PDWSA)	PDWSA is a collective term used for the description of Water Reserves, Catchment Areas and Underground Pollution Control Areas declared (gazetted) under the provisions of the <i>Metropolitan Water Supply, Sewage and Drainage Act 1909</i> or the <i>Country Area Water Supply Act 1947</i> .	Site lies within the Priority 2 Marbelup Brook Catchment Area (Section 2.4.1).
Groundwater Areas	Groundwater areas proclaimed under the <i>Rights in Water and Irrigation Act 1914</i> (RIWI).	Site lies within Albany Groundwater Area (Section 2.4.2, Figure 5).
Surface Water Areas	Surface water areas proclaimed under the RIWI Act 1914.	None present.
Irrigation District	Irrigation Districts proclaimed under the RIWI Act 1914.	None present.
Rivers	Rivers proclaimed under the RIWI Act 1914.	None present.
Waterways Management Areas	Areas proclaimed under the <i>Waterway Conservation Act 1976</i> .	None present within the Site; however, the Albany Waterways Management Area is located approx. 800 m to the north.
Clearing Control Catchments	Country Area Water Supply Act 1947 Part 2A.	None present.
South Coast Significant Wetlands	Represents the regionally significant wetlands of the South Coast.	Site contains the Marbelup Flats, a conservation class wetland (Section 2.4.3).

## 2.4.1 Public drinking water source area

The site is located within a Priority 2 (P2) area of the Marbelup Brook public drinking water source area (PDWSA) (GoWA, 2021). This PDWSA is gazetted under the *Country Areas Water Supply Act 1947*, however is currently not used. It has been identified as a potential future water source option in the *Great Southern Regional Water Supply Strategy 2014* (DoW, 2014).

The Minister for Water has formally provided advice to the City of Albany (Kelly, 2018) that while a motorsport facility is incompatible with a P2 PDWSA (DoW, 2016), “*there are measures that can be put in place to protect water quality should the City proceed to approve the development*”. These measures are further discussed in Section 4.2 (Wastewater servicing), Section 5.2 (Stormwater quantity management), Section 5.3 (Stormwater quality management) and Section 6 (Construction management) and Section 7 (Monitoring).

## 2.4.2 Groundwater conditions

On a regional scale, the 250K Map Series – Hydrogeology identifies a “*sedimentary aquifer within intergranular porosity – extensive aquifers, major groundwater resources*” underlying the Site (DoW, 2002). Groundwater salinity in the local area is in the range of 500 – 1000 mg/L, which is considered to be marginal for productive uses (GoWA, 2021).

A review of the DWER Water Information Reporting database identified no publicly available groundwater level or groundwater quality data within 2 km from the Site.

## 2.4.3 Wetlands and groundwater dependent ecosystems

Desktop searches identified no internationally important (Ramsar) or Nationally Important listed wetlands within 5 km of the Site (GoWA, 2021).

The South Coast Significant Wetlands dataset (DBCA-018) identifies the unnamed water course located within the Site as the Marbelup Flats, part of the King River Suite, and a Conservation Class wetland (Figure 4, Appendix A) (GoWA, 2021).

## 2.4.4 Surface water features

An unnamed creek line runs from the north-east corner of the site through to the south-west corner, from where it joins into Marbelup Brook located approximately 800 m west of the site boundary.

During a site visit (June 2018) the watercourse was observed to be in a modified state, with cattle currently having access to the watercourse. Erosion was evident, particularly in the eastern extent of the watercourse. This area was also mostly devoid of native vegetation, with the exception of some sedges (*Juncus* spp) (GHD, 2018). The western section of the watercourse contains native shrubs / sedges and had a defined bed / banks.



*Plate 1 Eastern extent of the watercourse showing evidence of erosion and cattle access*

## 2.4.5 Summary of pre-development monitoring (Bio Diverse Solutions)

Bio Diverse Solutions completed quarterly monitoring of surface water and groundwater at the Project Site for the period February 2018 to November 2019. An overview of the key results is provided in the following sections with sampling locations, the 2018 summary report and baseline water quality results for surface water and groundwater provided in Appendix C.

### 2.4.5.1 Surface water

Field records indicate two surface water sample locations within the unnamed watercourse were flowing for all monitoring dates in 2018 (Feb, May, Sep, Nov 2018), with flow at the downstream site (CS01) on all dates in 2019 (Feb, May, Aug, Nov).

An overview of key surface water quality data include:

- Surface water pH is moderately acidic, ranging from 4.46 to 6.85.
- Total nitrogen (TN) concentrations were typically higher at the upstream surface water location CS02 (TN range of 2 mg/L to 6.5 mg/L) compared to the downstream location CS01 (TN range from 0.5 mg/L to 2 mg/L)
- Total phosphorus (TP) concentrations were higher at the upstream surface water location CS02 (TP range from 0.22 mg/L to 0.55 mg/L) reflecting the TP concentration of bores in proximity to CS02. TP concentrations were typically below detection levels at the downstream surface water location CS01.
- Dissolved metals parameters including aluminium, iron and zinc were elevated in several samples at downstream surface water location CS01. Site CS02 reported isolated elevated aluminium, iron and zinc.
- MBTEXN parameters reported below detection in all surface water samples.
- TRH fractions were detected in some surface water samples.
- PAH parameters reported below detection in all surface water samples.
- Microbial testing detected microbial parameters in the majority of surface water samples.

## 2.4.5.2 Ground water

A summary of groundwater level records is provided in Table 5.

Table 5 Groundwater levels

Bore ID	Easting (m)	Northing (m)	Ground level – est. RL (mAHD)	Depth to Groundwater (mBGL)							
				Feb 2018	May 2018	Sep 2018	Nov 2018	Feb 2019	May 2019	Aug 2019	Nov 2019
SB01	567179	6133615	58.4	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB02	567404	6133889	49.6	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB03	567519	6134401	56.8	> 2.0	> 2.0	1.21	1.93	> 2.0	> 2.0	1.45	> 2.0
SB04	567700	6134179	48.2	> 2.0	0.91	0.30	1.07	1.66	1.11	0.37	1.48
SB05	568056	6134636	60.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB06	568131	6134478	53.6	0.87	0.70	0.00	0.59	1.03	0.73	0.06	0.73
SB07	567939	6134264	51.6	0.64	0.54	0.44	0.64	0.95	0.58	0.52	0.64
SB08	568308	6134637	56.5	> 2.0	1.55	0.18	1.27	1.58	1.42	0.38	1.29
SB09	568032	6134141	50.3	0.66	0.57	0.44	0.78	0.98	0.87	0.61	0.99
SB10	567886	6133756	62.7	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB11	568314	6134267	68.6	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0	> 2.0
SB12	568474	6134781	60.2	> 2.0	> 2.0	1.04	> 2.0	> 2.0	> 2.0	1.1	> 2.0
DB01	-	-	-	-	-	-	-	-	7.10	6.95	6.97
Notes	BGL – below ground level - Where results shown as “> 2.0”, this means the groundwater table was not intersected by the shallow groundwater monitoring bore (being only 2 m deep)										
	Results shown in red font - groundwater table was intersected by the groundwater monitoring bore.										
	Deep bore (DB01) monitoring only commenced from May 2019.										

An overview of key groundwater quality data include:

- Groundwater pH is moderately acidic, typically ranging from 3.82 to 7.52. pH at SB06 and SB07 (2.5 and 2.8) were significantly lower in February 2018 sampling event.
- Total nitrogen (TN) concentrations were typically elevated across the Site (range from 2 mg/L to 28 mg/L), which may be attributed to the historic and current farming practices. Significantly elevated TN at some bores (SB06, SB07 and SB08) coincided with sampling following peak groundwater levels. Exceptionally elevated TN concentrations reported in bore SB08 in February and May 2019 (110 and 79 mg/L), and additional sampling is recommended to confirm concentrations.
- Total phosphorus (TP) concentrations were typically elevated in some bores (SB06, SB07 and SB08).
- Dissolved metals parameters including aluminium, iron and zinc were elevated in the majority of samples in all bores, suggesting background concentrations of these metals are elevated due to the local soil and geological profile. Dissolved chromium was also elevated above the default trigger value in some bores.
- With the exception of toluene MBTEXN parameters reported below detection in the majority of groundwater samples. Toluene was detected in bore SB04 on all sampling occasions, and in bores SB06, SB07, SB08, SB09 in some sampling occasions. Toluene was elevated above the ANZG (2018) default toxicant guideline value in samples from SB07 (770 ug/L) and SB08 (210 ug/L, 310 ug/L, 980 ug/L).
- TRH fractions were detected in some groundwater samples. Particularly elevated TRH fractions were reported for bore SB07 and SB08 in February 2019. It is recommended that additional TRH samples are collected, with silica gel cleanup requested from the laboratory where elevated samples are identified.
- With the exception of a single detection for Naphthalene (SB06, Sept 2019) PAH parameters reported below detection in all groundwater samples.
- Microbial testing detected microbial parameters in some groundwater samples at all bores

## 2.4.6 Conceptual hydrogeological model

A conceptual hydrogeological model was developed for the site to gain an initial understanding of surface and groundwater water flows and potential linkages. Soil landscape mapping and regional geology mapping were used to infer geological units and soil types in the absence of deeper borehole data. The outcomes of the model (see Appendix D) noted:

- The groundwater levels observed in the shallow bores indicate that groundwater is present in the lower lying areas nearer the creek and will be most likely be supplying the creek with groundwater inflow.
- The groundwater levels and gradient, inferred from topography, supports that groundwater discharges into the creek.
- Shallow/perched groundwater may discharge and resurface via sandier layers that sit on top of more impermeable lateritic, coffee rock or clay layers; especially when there is significant slope.
- The discharging groundwater either expresses as surface water, or migrates within the deeper more permeable deposits.

## 2.4.7 Existing hydrological regime

### 2.4.7.1 Pre-development hydrology

A catchment analysis was completed using CatchmentSIM to delineate pre-development catchments for the entire site, including upstream areas. Refer to Figure 6 in Appendix A.

A one-dimensional DRAINS model with ILSAX hydrology was used for calculation of runoff. Model parameters included:

- Paved (impervious) area depression storage = 1 mm
- Supplementary area depression storage = 1 mm
- Grassed (pervious) area depression storage = 5 mm
- Soil Type 3 (slow infiltration rates).

The assessment was determined in accordance with Australian Rainfall and Runoff (ARR) 2016 (Geoscience Australia, 2016), with design rainfall data from the ARR 2016 data hub and the Bureau of Meteorology (BoM, 2018). The estimated peak flows for pre-development from various catchments are shown below in Table 6. Further assessment of specific areas impacted by the project works are further detailed in section 5.2.5. These focus on predevelopment areas surrounding the western motocross development and the eastern race track development, where the majority of the changes to the site occur.

**Table 6** Estimates of peak flows pre-development

Catchment	Area (ha)	Impervious fraction (%)	Peak flows (m <sup>3</sup> /s)			
			1EY (1 yr ARI)	0.5 EY (2 yr ARI)	10% AEP (10 yr ARI)	1% AEP (100 yr ARI)
E1	19.8	3	0.06	0.08	0.43	2.44
E2	17.4	3	0.08	0.10	0.39	2.24
E3	15.3	3	0.01	0.02	0.36	1.97
E4	13.9	0	0.00	0.00	0.45	2.27
E5	36.4	60	0.00	0.00	0.00	0.67
E6	17.4	0	0.00	0.00	0.33	1.81
S1	14.1	0	0.00	0.00	0.31	1.64
S2	23.4	0	0.00	0.00	0.57	3.30
S3	41.6	0	0.00	0.00	1.02	6.07
S4	33.6	0	0.00	0.00	0.65	3.64

Catchment	Area (ha)	Impervious fraction (%)	Peak flows (m <sup>3</sup> /s)			
			1EY (1 yr ARI)	0.5 EY (2 yr ARI)	10% AEP (10 yr ARI)	1% AEP (100 yr ARI)
S5	25.1	0	0.00	0.00	0.90	4.18
TOTAL	262.7	-	0.03	0.03	1.82	17.0
<i>Note:</i>	<i>E denotes an external catchment, S denotes a catchment within the site or with a significant portion of the catchment within the site.</i>					
	<i>TOTAL denotes the flows leaving the site via the creek/wetland which may be different to the individual catchments due to routing and storage within the site/model.</i>					

## 2.4.7.2 Flood modelling

To inform the design of site infrastructure, a site-wide modelling of the existing (or pre-development) flood conditions was undertaken. This entailed simulating the 1% AEP storm event over the site using TUFLOW (Build 2020-10-AA), which is a program for simulating depth-averaged, one and two-dimensional free surface flows (such as occurs from floods and tides). Calibration of the model was not performed, as there are no operational streamflow gauges in vicinity and/or relevant to the site.

### 2.4.7.2.1 Model setup and assumptions

Modelling was done using a ‘rainfall-on-grid’ approach, in which the design rainfall hyetograph is applied directly to a Digital Elevation Model (DEM) that describes the site topography. The DEM was generated with a 5 m cell resolution using 1 m surface contours from Landgate, which is the finest available topography data that is publicly available for the site.

Routing of surface runoff over the DEM is influenced by the surface roughness, which is characterised by assigning Manning’s roughness values to each DEM cell. Characterisation of the surface roughness was done through manual interpretation of the latest aerial imagery, with each identified surface type assuming the roughness values listed in Table 7.

Table 7 Adopted surface roughness values in flood modelling

Surface type	Manning’s roughness n*
Cleared and grassed	0.050
Forested	0.070
Bare earth	0.040
Paved/roof areas	0.020

\* Note: Values determined based on Table 6.2.2 in Book 6 of ARR 2019.

Catchment hydrological losses were simulated using an initial and continuing loss approach. With the exception of existing impervious areas, an initial and continuing loss values of 27 mm and 3.4 mm/hour were globally applied to the model domain. For paved and roofed areas, the initial loss was set to 1 mm and no continuing loss was applied. The effects of rainfall pre-burst are also accounted for in modelling by subtracting the median pre-burst depths (extracted from the ARR Data Hub) from the initial loss value.

Culverts across Down Road West were simulated as one-dimensional elements within the greater two-dimensional model. In the absence of detailed survey information, the culvert sizes were determined based on manual measurements taken by the Great Southern Motorplex Group on 17 June 2021; whilst culvert levels were set the same as the topographical low spots. Only two of the three culverts identified along the road were modelled. The culvert near the northeast corner of the site (i.e., Culvert E on Figure 7) could not be modelled due to the coarse resolution of the topography dataset, which did not accurately reflect the road geometry and adjacent table drains.

An open flow boundary is assumed along the perimeter of the model domain. This effectively simulates free discharge of flood waters out of the model and towards low lying areas external to the domain.

#### 2.4.7.2.2 Modelling outcomes

The simulated maximum flood depths and flow velocities for the 1% AEP storm event are provided in Figure 7 and Figure 8 in Appendix A. The results demonstrate that majority of the site drains to the central creek line via overland sheet flow and has very shallow or negligible flood depths; other than in obvious gullies or valleys.

Elevated floodwaters are simulated along the main creek that traverses the site, with localised spots where the flood depth and flow velocities exceed 1 m or 1 m/s in the 1% AEP storm event. Nevertheless, the simulated creek flood extents are largely contained within the proposed Protected Exclusion Area (which will be fenced off) and not expected to interfere with future site operations.

Concentrated flows are expected to occur across the centre of the motocross track, as well as the northern and southern portions of the multi-use racetrack. The simulated flood depths at these areas are generally less than 200 mm but will require provisioning of culverts and/or floodways to mitigate standing water on tracks.

Some flooding is simulated at two low spots north of Down Road West, with flood depths of up to 0.6 m at the western low spot and as high as 0.9 m at the eastern one in the 1% AEP storm event. Both low spots are drained via cross-carriageway culverts that discharge directly to the northern boundary of the site. In particular, the western culvert (i.e., Culvert W) discharges directly towards the proposed motocross track and diversion of these flows will need to be considered as part of this site’s stormwater management. This is further discussed in Section 5.

Table 8 summarises the simulated flows and velocities through each culvert.

Table 8 Simulated 1% AEP culvert flows and velocities

Culvert details	Culvert W	Culvert C	Culvert E
Diameter (mm)	750	900	1050
Flow (m <sup>3</sup> /s)	0.48	1.07	3.54*
Velocity (m/s)	2.04	2.61	NA

\* Note: Culvert not modelled. Overland surface flow used as proxy for culvert flow.

Some external catchment runoff from the CBH Mirambeena grain receival site is also expected to flow across Down Road and into the site from the north-east corner, partially through Culvert E. The natural flow path of this external flow cuts across the northern tip of the multi-use track and will need to be diverted accordingly.

## 2.5 Water users

### 2.5.1 Surface water

Review of aerial photography identifies numerous small dams located within Marbelup Brook and riparian zone (as demarcated by the DWER South Coast Significant Wetlands coverage), and one potential surface water abstraction (pumping) site downstream of the Site. These locations are summarised in Appendix E.

### 2.5.2 Groundwater

Groundwater allocation in Western Australia is regulated by DWER. The DWER Water Register notes one groundwater license for the Site and five groundwater licenses downgradient / downstream of the Site along the Marbelup Brook. The groundwater licences are summarised in Appendix E.

## 2.6 Environmentally sensitive areas

### 2.6.1 DWER Environmentally sensitive areas

The DWER maintains a dataset of Environmentally Sensitive Areas (ESA). ESAs are areas of land deemed to support conservation, heritage or ecological value, or an area protected through existing State Policy. There are no mapped Environmentally Sensitive Areas (ESA) within 5 km of the Project Site (DWER-046).

As per DWER guidance (DER 2014) a conservation category wetland is “a defined wetland and the area within 50 m of the wetland” and is declared to be an ESA under the *Environmental Protection Act 1986*. The Conservation Class wetland within the Project Site (Section 2.4.3, Figure 4) is identified as an ESA.

### 2.6.2 Groundwater dependent ecosystems

A search of the online *Groundwater Dependent Ecosystems (GDE) Atlas* (BoM 2020) does not identify any terrestrial or aquatic groundwater dependent ecosystems within the Project Site boundary.

### 2.6.3 Flora and fauna

Bio Diverse Solutions (2019) completed a Level 1 Fauna Survey and a reconnaissance level flora survey in spring 2018. The reconnaissance level flora survey did not identify any EPBC Act, BC Act or State Priority listed flora species within the Project Site.

The Level 1 fauna survey observed four conservation significant fauna species directly and indirectly within the broader survey area including:

- Baudin’s Cockatoo (*Calyptohynchus baudinii*) (Vulnerable, Schedule 2)
- Forest Red-tailed Black Cockatoo (*Calyptohynchus banksia naso*) (Vulnerable, Schedule 3)
- Western Brush Wallaby (*Notamacropus irma*) (Priority 4)
- Southern Brown Bandicoot, Quenda (*Isodon fusciventer*) (Priority 4).

Marbelup Brook was identified to have high aquatic fauna species richness from monitoring for the study *Ecological values of waterways in the south coast region, Western Australia* (Cook, Janicke, & Maughan, 2008). The high aquatic fauna species richness was partly attributed to the high number of samples collected, comprising 28 sites including three sites (MAR07, MAR08 and MAR09) located within and immediately downstream of the Site.

## 2.7 Sewage sensitive areas

The Department of Planning Lands and Heritage Map of Sewage Sensitive Areas identifies that the majority of the site is located within a sewage sensitive area (within 1 km of significant wetlands).

### 3. Design criteria and objectives

This section outlines the design criteria and objectives that the Water Management Plan (WMP) for the site must achieve. The design criteria have been developed with reference to the principles and objectives and guidance in the following:

- AMP Feasibility Study (GHD, 2018)
- *Stormwater Management Manual for Western Australia* (DoW, 2007)
- *Decision process for stormwater management in Western Australia* (DWER 2017)
- *Subdivision and Development Guidelines 2018* (CoA, 2018)
- *WQPN 100: Motor sport facilities near sensitive waters* (DoW, 2007)
- *WQPN 28: Mechanical servicing and workshops* (DoW, 2013)
- *WQPN 52: Stormwater management at industrial sites* (DoW, 2006).

#### **Water and wastewater supply and servicing**

This WMP proposes the following water supply design criteria for the site:

- Criteria WS1: Potable water will be supplied through collection and treatment of rainwater to potable standard. Non-potable water will be supplied via bore, site dam and rainwater tanks.
- Criteria WS2: Shortfalls in potable water supply will be imported to the site.

Further detail is provided in Section 4.1.

The wastewater management strategy proposes the following design criteria for the site:

- Criteria WW1 (Stage 1A): Domestic wastewater will be serviced using a combination of transportable toilets (with waste disposal managed by a waste management contractor) and a permanent on-site treatment and disposal system, in accordance with the *Government Sewerage Policy* (DoH, DPLH, DWER, 2019) for a PDWSA and Sewage Sensitive Area.
- Criteria WW1 (Stage 1B): Domestic wastewater will be serviced using transportable toilets (with waste disposal managed by a waste management contractor)
- Criteria WW2: Wastewater from vehicle maintenance, refuelling and washdown areas will be managed in accordance with WQPN 28.

Further detail of domestic wastewater servicing is provided in Section 4.2.1, with detail of vehicular maintenance servicing areas provided in Section 4.2.2.

#### **Stormwater management**

This WMP proposes the following stormwater design criteria for the site:

- Criteria SW1: Maintain the hydrological regime of the site and surrounds.
- Criteria SW2: Maintain serviceability of motorsport tracks for the 10% AEP event.
- Criteria SW3: Provide adequate drainage to achieve 300 mm separation from the 1% AEP event for key infrastructure (e.g. vehicle maintenance areas, buildings, wastewater facilities).

#### **Water quality management**

This WMP proposes the following water quality design criteria for the site:

- Criteria WQ1: Manage stormwater from the Site to ensure no deterioration in surface and groundwater quality.
- Criteria WQ2: Retain and treat stormwater runoff from constructed impervious surfaces generated by the first 15 mm of rainfall at source, prior to discharge or disposal to groundwater.
- Criteria WQ3: Manage stormwater quality from the Site in accordance with WQPN 100, WQPN 28 and WQPN 52.

## 4. Water supply and servicing

### 4.1 Water supply

#### 4.1.1 Potable water

The Water Corporation's Lower Great Southern Towns Water Supply Scheme (LGSTWSS) runs along Albany Highway, with the nearest connection point approximately 4 km to the east at 66 Down Road (fertiliser distribution warehouse) (Water Corporation, 2018). Hence, it is proposed to service Site drinking water needs through a combination of collected rainwater and water carts.

Uncontaminated rainwater from the Site roof runoff (AMP buildings) will be collected in standard 110,000 litre rainwater tanks. At source treatment by household-scale filtration and ultraviolet disinfection will be undertaken. This will allow a safe drinking water supply to the AMP facilities (i.e. clubrooms, canteen, etc.) and ablutions.

A preliminary water balance for the site suggests that rainfall alone will be insufficient to meet expected demand for regular attendance of 500 people. Where there is a shortfall, the venue operator will purchase and cart water to the Site. Similarly for large-scale events, additional potable water will need to be carted to site.

#### 4.1.2 Non-potable

Water demands for other external, non-potable uses (i.e. garden irrigation, toilet flushing, vehicle washdown, dust suppression, etc.) will be met from Site bore, dams and rainwater tanks (where possible). The GSMG is negotiating with Plantation Energy for access to their 4,000 kL Bremer West superficial groundwater allocation (licence number 168308).

#### 4.1.3 Fire water

Fire water supply will be through on-site resources via bore extraction to tank storage and pumped to facilities around the site. Storage of water dedicated for firefighting will be located in the north and the eastern precincts and tanks are to be a minimum of 110,000 L (as shown on Masterplan).

### 4.2 Wastewater servicing

#### 4.2.1 Domestic wastewater

The Water Corporation's Albany sewerage scheme is not in close proximity to the Site, with the nearest connection point being at Lancaster Road, McKail (being some 10 km distant).

Stage 1A of the development will be serviced by a combination of transportable toilet units (Plate 2) and permanent toilets in the multi-purpose building (sized for 300 patrons). The permanent toilets are connected to an on-site treatment and disposal system, designed in accordance with the *Government Sewerage Policy* (DoH, DPLH, DWER, 2019) for a PDWSA and Sewage Sensitive Area. A full site and soil evaluation report is attached in Appendix H. The transportable toilet units will be maintained and regularly serviced by a local waste disposal contractor. For large-scale events additional portable hire toilet units will be used to accommodate peaks in wastewater production.

Stage 1B of the development will be serviced by transportable toilet units only (Plate 2). The transportable toilet units will be maintained and regularly serviced by a local waste disposal contractor. For large-scale events additional portable hire toilet units will be used to accommodate peaks in wastewater production.



Plate 2 Example portable toilet unit

## 4.2.2 Vehicular maintenance wastewater

The Site is proposed to be used for motor sport activities. All vehicle maintenance and servicing including vehicle washdown and refueling, will be undertaken in dedicated refueling and pit areas.

To minimise the risk of contamination to sensitive receptors the refueling and pit areas will be designed and constructed in accordance with WQPN 100 and WQPN 28, including the following attributes:

- Have a low permeability sealed concrete pad to minimise seepage and assist cleanup of spills.
- Will be covered and weatherproofed to prevent stormwater intrusion.
- Designed with floors graded to a pit and pipe network that will be serviced by a sediment trap and oil water separator, to ensure stormwater and wastewater are managed separately from other parts of the Site.
- Be double bunded to contain water and spills within the internal drainage network.
- No fuel or combustible chemicals will be stored on-site.

On-site personnel will complete regular inspection and maintenance of the vehicle maintenance areas wastewater infrastructure to ensure they are operating as required.

Sediment from the sediment trap will be removed as required and disposed of at a registered waste facility. Any hydrocarbons removed from the oil water separator will be collected and stored within appropriate sealed containers for disposal at a registered waste facility.

Spill kits will be held at the vehicle maintenance areas in the event of any hydrocarbon spill. When spill kits are used the material will be disposed of at a registered waste facility.

On-site personnel will be trained in the use and disposal of spill kits.

A separate Hydrocarbon Management Plan is included as part of the Environmental Management Plan.

# 5. Stormwater management plan

## 5.1 Overview

Stormwater management across the Site has been developed based on an understanding of the key site risks. The design of the Site and stormwater management elements has been iterative and developed with regard to key site characteristics including nature of the proposed activities, external catchment flows, steep terrain over parts of the Site, shallow groundwater conditions over parts of the Site, high surface/groundwater connectivity and downstream receptors and water users.

The key components of the Stormwater Management Plan for the site include:

- Flows that originate upstream of the site will be diverted around motorsport park infrastructure to maintain pre-development hydrology, and to keep externally generated flows separated from stormwater runoff from the motorsport park infrastructure.
- The Site has been designed to ensure key infrastructure (vehicle maintenance areas, buildings, bioretention basins) are sited outside of the modelled 1% AEP flood area (Section 2.4.7.2).
- Key stormwater management controls and best management practices have been considered for various parts of the Site infrastructure to reduce or minimise risk to surface and groundwater quality.
- Stormwater generated from areas considered to have a higher risk of discharging potential contaminants of concern (vehicle maintenance areas) will be managed separate to stormwater runoff from the remainder of the site.
- The first 15 mm of runoff generated from car parking, hardstand areas, motocross track and race track will be treated in bioretention areas.
- Runoff generated from Site buildings will be directed to rainwater tanks, with overflow infiltrated close to source or diverted to swales.

The following sections provide a further detail of the design of the stormwater management system for Stage 1A and 1B of the proposal, with Section 5.2 detailing the management of stormwater quantity and Section 5.3 detailing the management of stormwater quality.

## 5.2 Stormwater quantity

### 5.2.1 Principles and objectives

The management of stormwater quantity is proposed in accordance with the principles and objectives of the technical feasibility study (GHD, 2018), the *Stormwater Management Manual for Western Australia* (DoW, 2007); the *Decision Process for Stormwater Management in Western Australia* (DoW 2017), WQPN and the *Subdivision and Development Guidelines 2018* (CoA, 2018).

For vehicle maintenance areas (refueling, washdown and pit areas) stormwater and wastewater generated in these areas for all events up to the 1% AEP will be managed internally as detailed in Section 4.2.2. The stormwater system within this area is further described in Section 5.2.3.2. Vehicle maintenance areas will not be used during events exceeding the 10 year ARI event (10% AEP).

For all other parts of the Site the following principles apply with detail provided for Stage 1A in Section 5.2.2 and Stage 1B in 5.2.3.

#### **1-year ARI event and smaller (1EY)**

To retain and treat the 1-year ARI (1EY) event:

- Runoff from impervious areas will be managed via a range of measures including:
  - Small event runoff from impervious areas will be directed to bioretention basins for treatment, prior to infiltration where there is sufficient separation to groundwater.

- Targeted rainwater (roof water only) capture for potable (i.e. drinking) and non-potable water supply (refer Section 4.1). Overflow from rainwater tanks will be infiltrated close to source using soakage pits or infiltration galleries, or directed to swales.
- Drainage swales will be sited downstream of the tracks, conveying stormwater to bioretention basins and allowing stormwater infiltration as close to source as practical, in accordance with WSUD principles. Vegetation, rock weirs and/or check dams (in steep sloped areas) will slow flows and contribute to achieving WSUD objectives. Culverts will be installed to allow crossings of access tracks, carparking (where required) and racetrack pavement, with some piped sections where site topography doesn't allow overland flow.
- Direction of runoff to bioretention basins targeting peak flow management to pre-development levels, where possible.
- Where possible, bioretention basins are positioned to ensure 2 m vertical clearance from the maximum groundwater level. Where bioretention basins are located within 2 m vertical clearance from maximum groundwater level the base of the basin will be lined with local clay to reduce permeability, with subsoil drains installed to provide drainage function.

### **10-year ARI event (10% AEP)**

To maintain site serviceability in the 10-year ARI (10% AEP) event:

- Drainage swales will convey stormwater to bioretention basins and will allow stormwater to be infiltrated as close to source as practical in accordance with WSUD principles. Vegetation and check dams (in steep sloped areas) will slow flows and contribute to achieving WSUD objectives. Culverts will be installed to allow crossings of access tracks and raceway pavements.
- The bioretention basins are designed to compensate peak flows to pre-development levels, and maximise opportunities for infiltration prior to discharge from the site.
- Appropriate erosion control and energy dissipation will be implemented at the outlet of piped drainage structures.

### **100-year ARI event (1% AEP)**

To protect from flooding in the 100-year ARI (1% AEP) event:

- Key site infrastructure (vehicle maintenance areas, habitable buildings) are sited outside the 1% AEP flood area (Section 2.4.7.2). A minimum freeboard of 300 mm is provided to prevent ingress of water.
- Stormwater flows will exceed the capacity of the internal drainage swales, but will be contained within the swale freeboard, or via overload flow along roadways or grassed flow paths.
- The bioretention basins will compensate peak flows to levels that will not adversely impact the downstream receiving areas, and maximise opportunities for infiltration prior to discharge from the site.
- Overland flow paths are provided to minimise the potential for exposure of publicly accessible areas to flood waters.
- Basins will be designed with appropriate emergency overflow weirs and structures to ensure controlled discharge wherever possible.

## **5.2.2 Stage 1A**

Stage 1A of the Albany Motorsport Park comprises the motocross track and 4WD driver training, ATV area and associated infrastructure. Figure 9 in Appendix A presents the proposed stormwater management plan for Stage 1A. An overview of key stormwater management infrastructure is described in the following sections. Details of the hydraulic and hydrologic modelling, including sizing of key stormwater infrastructure are provided in Section 5.2.4.

### **5.2.2.1 Diversion of external flows**

Flood modelling of the site (Section 2.4.7.2) has identified external flows generated from the catchment of the Albany Plantation Export Company (APEC) site to the north of the Stage 1A area. Under current conditions it is assumed that stormwater runoff passes through existing culverts along Down Road West (refer Table 8), with occasional overtopping of the road in larger events and sheeting across the road verge and down into the existing valley.

It is proposed to divert flow from this external catchment via a vegetated diversion drain that traverses around the western edge of the motocross track. Culverts will be located to convey flows under the carpark area and under the motocross track where required.

A second diversion drain is sited along the central hillslope, on the eastern side of the motocross track, as a cut off drain to divert any flows from the hillslope area away from the track.

It is proposed to direct flows from the diversion drains to the central creekline along gently sloping areas. A level spreader weir is proposed to dissipate flows as sheetflow over a vegetated overland pathway. Where slopes are steep or level spreader weirs are not used, the base of swales will be rock protected and feature regular rock weirs and/or check dams to reduce velocity.

Diversion drains have been sized to manage all runoff from the external catchments in accordance with pre-development discharge.

### **5.2.2.2 Refuelling and washdown area**

All servicing, washdown and refuelling associated with the motocross track will be completed within the designated refuelling and washdown area. This area will be a covered concrete area with double perimeter bund and internally draining pit and pipe network. The pit and pipes will direct all water to a sediment trap and an oil water separator, as described in Section 4.2.2.

Treated water from the oil water separator will be directed into the stormwater drainage system.

### **5.2.2.3 Access road and carpark**

In small runoff events stormwater runoff generated from the access roads and carparks will be directed towards distributed bioretention basins to treat stormwater, and infiltrate where possible. Flow in excess of the capacity of the bioretention basins will connect to surface drainage (e.g. diversion drain, swale drainage).

### **5.2.2.4 Motocross track**

The motocross track is sited across the northern valley of the Site. Fill sourced from the Site is used to provide adequate separation ( $\geq 2.0$  m) of the track from the maximum groundwater level. The track is constructed using locally sourced sandy/clay. Refer to the motocross track drawings (plan and longitudinal sections in Appendix F).

Stormwater runoff from the motocross track is directed to a series of vegetated drainage swales that capture and convey stormwater flows to distributed bioretention basins.

Swale dimensions are summarised in Section 5.2.4.

### **5.2.2.5 4WD driver training and ATV area**

The location of the 4WD driver training and ATV area has been identified as a local source of sand/clay and gravel, which will be used for the construction of the motocross track, access road, carparking areas and race track at the Site.

Following removal of sand/clay and gravel the 4WD driver training and ATV area will comprise the natural surface. No formal stormwater management is proposed in this area. Stormwater runoff from this area will be directed to a bioretention basin at the natural low point to aid settling of sediment, with flow in excess of the bioretention basin volume directed via a vegetated overland flowpath towards the central creekline.

## 5.2.3 Stage 1B

Stage 1B of the Albany Motorsport Park comprises the race track and associated infrastructure. Figure 10 in Appendix A presents the proposed stormwater management plan for Stage 1B. An overview of key stormwater management infrastructure is described in the following sections. Details of the hydraulic and hydrologic modelling, including sizing of key stormwater infrastructure are provided in Section 5.2.4.

### 5.2.3.1 Diversion of external flows

Flood modelling of the site (Section 2.4.7.2) has identified external flows generated from the north-east catchment, with flows crossing Down Road West from the APEC site to the north, the CBH Mirambeena site to the north-east, and agricultural land to the east of the Stage 1B area.

Flows from part of the northern part of this external catchment accumulate in a roadside drain on the north side of Down Road West, and flow via a culvert (1050 mm dia.) under Down Road West to the Site. External flows originating along the northern boundary of Stage 1B will follow their natural flowpaths with minor culvert crossings (300 mm culvert) provided under access roads where required. A culvert crossing of the Down Road West roadside drain will be provided at the entry to the Site.

External flow originating from the eastern agricultural land will follow its natural flowpath, with minor culvert crossings provided under the access road and race track where required. This diversion drain will also receive some race track stormwater runoff, and flows will be directed to a bioretention basin prior to discharge from the Site.

The flows originating from the north-east (CBH site) will be diverted around the race track using a cut off drain, with minor culvert crossings provided under the access road and race track where required.

Where slopes are steep or level spreader weirs are not used, the base of swales shall be rock protected and feature regular rock weirs and/or check dams to reduce velocity and provide water treatment.

Diversion drains are sized to manage all runoff from the external catchments in accordance with pre-development discharge.

### 5.2.3.2 Pit area

All servicing, washdown and refuelling associated with the race track will be completed within the designated pit area. The pit area will be covered and weatherproofed to prevent stormwater intrusion, with an impervious perimeter bund and floors graded to an internally draining pit and pipe network. The pit and pipe drainage network in this area may comprise perimeter trench drains with trafficable covers located within the perimeter bund to prevent egress of any surface water drainage or spills generated within this area.

The pit and pipe drainage network will direct all water to a sediment trap and an oil water separator, as described in Section 4.2.2. Treated water from the oil water separator will be directed into the stormwater drainage system.

### 5.2.3.3 Access road, spectator carpark, competitor carpark and emergency muster area

Runoff from these areas will be managed as follows:

- Access roads and tracks – stormwater runoff generated from the access roads will drain to vegetated areas alongside the roads. Where this cannot occur, roadside drains will be implemented which will feature regularly spaced rock weirs/check dams to slow flows and promote sedimentation. Where required, suitable culvert pipes or overflow points either under the roadway or over the roadway will be provided to target controlled discharge to the surrounding environment.
- Spectator carpark – small event stormwater runoff generated from carpark area will be directed towards the bioretention swales distributed throughout the carpark. These will be connected via minor culverts under the carpark to the adjacent drainage swales.
- Competitor parking and marshalling area – it is proposed that the emergency muster area will feature a crest to direct stormwater runoff to vegetated swale drains located around the perimeter of the competitor carpark and marshalling area. The southern and eastern portions of the carpark and emergency muster area will be

designed to direct flows to a bioretention basin in the south-east corner of the Site. The north-western portion of the carpark and emergency muster area will divert flows to drainage swales and bioretention basins located to the north and south of the Pit area.

#### 5.2.3.4 Race track

Runoff from the race track is designed to capture and convey stormwater flows in a series of shallow vegetated swales (1V:6H) sited downstream of race track cross-fall (assumed on inside of corners). The shallow vegetated swales will feature regularly spaced interceptor traps, and will convey flows to bioretention basins.

### 5.2.4 Hydrologic and hydraulic assessment

Sizing of key stormwater infrastructure for Stage 1A and Stage 1B including diversion drains, swales and bioretention basins was completed through development of a post-development hydrologic and hydraulic model, using inputs from the existing site hydrology (Section 2.4.7) and the Site infrastructure plans (Figure 2 in Appendix A).

#### 5.2.4.1 Diversion drains

Design of the diversion drains is based on the following:

- Where space and topography permit the drainage swales will be broad and shallow. Side slopes of 1V:6H are proposed to ensure safe vehicle run-off in proximity to the motocross track and race track, as well as ease of maintenance.
- Maximum side slopes of 1V:3H may be required in areas restricted by space or topography.
- Diversion drains will have a freeboard of 0.3 m (over the 10% AEP design event level) to allow additional storage and conveyance to distributed bioretention basins.
- Drains with typical slopes that are greater than 3% longitudinal grade will require erosion protection surfacing either in the form of rock lining or other similar measures.

Typical diversion drain dimensions are summarised in Table 9. Further information on drains with similar requirements are detailed on Figure 9 and Figure 10.

Table 9 *Diversion drain dimensions*

Swale example	Shape and side slope (V/H)	Average slope (%)	Max depth* (m)	Length (m)	10% AEP flow (m <sup>3</sup> /s)
Stage 1A					
W-EXT02	1:6 swale	0.38	0.542	140	0.172
W-EXT04	1:6 swale	1.56	1.423	100	0.186
Stage 1B					
E-B9-07	1:4 swale	1.64	0.781	350	0.072
E-B9-08	1:4 swale	0.94	0.781	120	0.024

\* The max. depth is driven by providing adequate freeboard for the 10% AEP event while also considering the depths in the 1% AEP event. The depth varies along the drain and would generally increase from a minimum depth of 300 mm at the upstream end, unless receiving water from upstream drains or culverts.

#### 5.2.4.2 Drainage swales

Design of the drainage swales is based on the following:

- Where space and topography permit the drainage swales will be broad and shallow. Side slopes of 1V:6H are proposed to ensure safe vehicle run-off in proximity to the motocross track and race track, as well as ease of maintenance.

- Maximum side slopes of 1V:3H may be required in areas restricted by space or topography.
- Drainage swales will have a freeboard of 0.3 m (over the 10% AEP design event level) to allow additional storage and conveyance to distributed bioretention basins.
- Drains with typical slopes that are greater than 3% longitudinal grade will require erosion protection surfacing either in the form of rock lining or other similar measures.

Key swale dimensions are summarised in Table 10, while the modelling results for each swale drain are contained in Appendix G.

Table 10 Swale dimensions

Swale example	Shape and side slope (V/H)	Average slope (%)	Max depth*** (m)	Length (m)	10% AEP flow (m <sup>3</sup> /s)
Stage 1A					
W-B4-01	1:6 swale	1.80	0.909	170	0.088
W-B4-02	1:6 swale	4.81	0.909	200	0.110
W-B5-04	1:6 swale	3.00	0.811	40	0.188
W-B5-05	1:6 swale	4.89	0.798	45	0.018
W-S1	1:6 swale	5.07	0.478	300	0.265
Stage 1B					
E-B4-01*	K300**, 0.4 m deep	0.50	0.57	150	0.090
E-B4-02	1:4 swale	0.90	0.586	220	0.248
E-B6-01	1:6 swale	3.87	0.699	150	0.094
E-B9-01	1:6 swale	3.60	0.447	160	0.129

\* Further development in detail design will likely require a pit and pipe system to be installed in combination with this trench drain.

\*\* K300 is an assumed 300 mm wide with varying depth Class D Covered Trench Drain

\*\*\* The max. depth is driven by providing adequate freeboard for the 10% AEP event while also considering the depths in the 1% AEP event. The depth varies along the drain and would generally increase from a minimum depth of 300 mm at the upstream end, unless receiving water from upstream drains or culverts.

### 5.2.4.3 Culverts

Different crossing locations were determined to manage discharge to the surrounding environment. Preliminary sizing of proposed culverts was done using DRAINS software and results are shown in Table 11. Further assessment of these culverts are suggested in future design stages to determine structural suitability, should there be reduced cover as limited by resulting earthworks.

Table 11 Culvert dimensions

Culverts	Length (m)	Slope (%)	No. of barrels	Diam (mm)
Stage 1A				
W-B1-CULV1	30	1.17	1	450
W-B5-CULV1	13	2.00	1	450
W-B5-CULV2	12.5	3.00	1	450
W-B5-CULV3	19.2	1.56	2	450
W-B5-CULV4	14.5	2.76	1	450

Culverts	Length (m)	Slope (%)	No. of barrels	Diam (mm)
W-B5-CULV5	12.6	7.06	1	450
W-B5-CULV6	20	1.00	1	450
W-EXT-CULV	150	2.13	1	450
W-EXT-CULV1	20	0.50	1	450
Stage 1B				
E-B5-CULV1	15	6.07	1	450
E-B7-CULV1	55.2	2.55	1	450
E-B7-CULV2	13.4	3.06	1	450
E-B7-CULV3	97.1	0.50	1	450
E-B9-CULV1	13.7	7.30	1	450
E-B9-CULV2	28.3	3.22	1	450
E-B9-CULV3	49	1.86	1	450

#### 5.2.4.4 Bioretention basins

A series of shallow distributed bioretention basins are sited to provide both water quality treatment as well as stormwater compensation/detention/infiltration throughout the Site.

The bioretention basins are sized such that the total post-development flow off the site was equal to or less than the pre-development flow for the minor (10% AEP) design event and targeted appropriate compensation and management of major storms (i.e. the 1% AEP or 100 year ARI). Bioretention basin parameters included:

- Sited outside the 1% AEP event from the major creek through the site.
- Construction should use the natural topography of the Site where possible.
- Basin base levels set to be 2 m above the assumed groundwater level when used for infiltration. If within 2 m of the groundwater the base of the basin is to be lined to prevent infiltration; these basins will require the implementation of a subsoil drainage system.
- Basins equipped with low flow outlet/s (pipe/orifice), high flow bypass pit and a mortared/rock protected overflow spillway that has sufficient capacity to handle 1% AEP flow, where possible.
- Nominal depths ranging from 0.35 m to 1.2 m to spillway levels; and 0.5 m to 1.5 m to top of wall.
- 1V:6H side slopes where space permits to allow for vegetation to stabilise side slopes and reduce erosion risk. Where geotechnical conditions permit, basin side slopes may be increased a max. of 1V:3H to facilitate increased base infiltration surface (may require fencing and/or signage for safety where fencing is not appropriate).
- An average 2 m/day infiltration rate has assumed, noting that testing has found varying rates of between 0.41 and 3.29 m/day across the site. Detailed design of each basin should be informed by the site-specific permeability test results in Appendix B.
- Bioretention basins feature a low flow piped discharge, designed to be:
  - Set above the peak 1EY basin water level, such that no discharge occurs for water quality management, where possible (basins requiring lining will need to discharge the 1EY event).
  - Set and sized so as to ensure that the basin overflow spillway does not activate in events up to and including the 10% AEP.
  - Contributing catchments would be directed into each of the basins as detailed in Section 5.2.2 and Section 5.2.3.
- Post development flows are those of the combined catchment areas that contribute to the basin location and are shown in Appendix G.
- The results of the bioretention basin sizing for Stage 1A and Stage 1B are summarised in Table 12.

Table 12 Bioretention basin sizing \*

Basin	Slope (1V:_H)	Base Elevation (m)	Base Area (m <sup>2</sup> )	Top Elevation (m)	Top Surface Area (m <sup>2</sup> )	Depth (m)	Max Volume (m <sup>3</sup> )	By-pass level (m)	Low Flow Outlet	Overflow weir level (m)
Stage 1A										
West-B1	3	66.0	90	67.0	265	1.0	170	66.60	N/A	66.75
West-B2	6	62.0	150	62.5	640	0.5	180	62.35	3 x 70	62.35
West-B3	3	62.5	160	64.0	475	1.5	450	63.20	N/A	63.70
West-B4	6	59.0	100	60.5	450	1.5	400	59.50	2 x 70, 1 x 100	59.60
West-B5	3	53.5	105	54.5	260	1.0	175	54.00	3 x 90	54.25
West-B6	6	58.0	100	59.0	500	1.0	275	58.50	N/A	58.75
West-B7	3	51.5	430	52.5	980	1.0	700	52.20	3 x 70	52.50
Stage 1B										
East-B1	6	58.0	145	59.5	950	1.5	750	58.75	1 x 90	59.50
East-B2	6	57.0	500	58.0	1150	1.0	800	57.50	1 x 90	57.75
East-B3	6	70.0	350	71	950	1.0	625	70.60	3 x 100	71.00
East-B4	6	71.0	250	71.5	550	0.5	200	71.25	N/A	71.38
East-B5	6	66.0	300	67.5	1300	1.5	1100	67.00	2 x 80, 1 x 100	67.20
East-B6	6	61.0	600	61.5	1000	0.5	400	61.20	3 x 90	61.50
East-B7	6	65.0	300	66.0	850	1.0	550	65.50	180, 1 x 90, 1 x 90	65.75
East-B8	6	70.5	250	71.5	750	1.0	475	71.00	N/A	71.25
East-B9	6	63.0	950	64.0	1800	1.0	1350	63.50	N/A	64.00
East-B10	6	62.0	430	62.5	800	0.5	300	62.25	3 x 110	62.50

\* The levels detailed in the above table are subject to change during detailed design however base areas and volumes will need to be generally achieved.

## 5.2.5 Pre- and post-development discharge

The outlet locations to the downstream watercourse were determined, and the contributing catchments from Stage 1 works assessed for the treatment and management of stormwater runoff within the site. Due to the proposed layout of the tracks, minor changes in catchment areas were present when comparing both pre-development and post-development scenarios. A summary of this comparison is shown in Table 13.

All outlet locations on Stage 1B are shown discharging on a 1EY event and must be treated within the basin prior to discharge, to mitigate any adverse water quality outcomes. The modelling determined it is impractical to manage some flows to below pre-development discharge (i.e. East-3 and East 4) for the 10% AEP. However overall the post-development discharge from all eastern catchments is below pre-development discharge. For the western catchments, the total post-development discharge is only 0.007 m<sup>3</sup>/s above pre-development, which is only 1.5% and considered insignificant.

Table 13 Combined site discharge

Discharge location	Pre-development flows (m3/s)				Post Development flows (m3/s)			
	Area (ha)	1EY	10% AEP	1% AEP	Area (ha)	1EY	10% AEP	1% AEP
<b>Stage 1A</b>								
West-1	14.10	0	0.270	1.64	14.10	0	0.263	1.600
West-2	11.17	0	0.214	1.36	6.86	0	0.132	0.286
*West-3	*	*	*	*	4.31	0.013	0.096	0.498
<b>TOTAL</b>	<b>25.27</b>	<b>0</b>	<b>0.484</b>	<b>3.00</b>	<b>25.27</b>	<b>0.013</b>	<b>0.491</b>	<b>2.384</b>
<b>Stage 1B</b>								
East-1	12.13	0	0.244	1.58	11.04	0.020	0.158	0.450
East-2	13.30	0	0.296	1.83	15.53	0.016	0.290	1.080
East-3	9.76	0	0.177	1.06	10.28	0.031	0.193	0.919
East-4	7.35	0	0.118	0.65	5.72	0.021	0.174	0.494
<b>TOTAL</b>	<b>42.54</b>	<b>0</b>	<b>0.835</b>	<b>5.12</b>	<b>42.57</b>	<b>0.088</b>	<b>0.815</b>	<b>2.943</b>

\*additional outlet location taken from West-2

## 5.3 Stormwater quality

### 5.3.1 Overview

The hydrogeological conceptual model (Appendix D) indicates high surface/ groundwater connectivity within the Site, with potential for impacted groundwater to migrate towards the creekline and off-site towards the major drainage in the area, the Marbelup Brook. If not responsibly managed, the development has the potential to negatively affect stormwater quality discharging from the catchment and impact on the potential receptors and water users.

Based on the proposed site activities the key stormwater quality issues requiring management include:

- **Sediment load:** Erosion caused by high flow velocity can result in a loss of soil, damage to drainage swales, and increased sediment load to the receiving water body.
- **Nutrient load:** Increased nutrient loading to the receiving water body may result from over- application of fertilisers to landscaped areas.
- **Gross pollutants:** Suspended and dissolved pollutants, and rubbish.
- **Toxicants:** Key pollutants associated with motor sport facilities include leaks and spills of chemical or petroleum hydrocarbons from vehicle maintenance areas, hydrocarbon storage areas and racetracks. Other potential toxicants of concern include dissolved metals and pesticides.

## 5.3.2 Best management practices

Management of stormwater quality is focused on providing appropriate treatment of stormwater runoff generated by the various parts of the Site based on an understanding of the key site risks. A range of key controls and best management practice WSUD elements will be utilised to manage stormwater quality across the site.

Best management practices (BMPs) are design strategies targeted to manage total suspended solids, gross pollutants, nutrients (TP and TN) within stormwater discharged from urban catchments (DoW, 2007). Frequently occurring rainfall events are targeted, using source, in-transit and end-of-pipe controls to improve water quality. BMPs considered appropriate for the Site include:

- The Site stormwater drainage system has been designed to separate good quality stormwater from potentially contaminated stormwater.
- Flows generated from external catchments will be diverted around the Site infrastructure, with external drainage separated from Site drainage where possible.
- Stormwater runoff from hydrocarbon-impacted areas including the refuelling and washdown area (Stage 1A) and pit (Stage 1B) will be isolated from stormwater generated for other parts of the Site. These areas are covered, double bunded, with internal stormwater pit and pipe network connected to sediment trap and oil water separator.
- Maximising infiltration by adopting a stormwater retention system to contain, and as a minimum, treat the first 15 mm of rainfall on site.
- Flows generated from Site buildings are considered to be uncontaminated and will be diverted to rainwater tanks for reuse as discussed in Section 4.1.1, or infiltrated at source.
- Use of suitable soils within swales and compensation basins that target the uptake of nutrients.
- Construction of combined bioretention and compensation basins to allow water quality treatment of small events (including metals and hydrocarbons), encourage infiltration and reduce peak flow rates.
- Swale drains shall be planted with grass for filtering of particulates and uptake of dissolved nutrients. Grass will be mowed with clippings removed from site.
- Additional sediment management measures include regularly spaced interceptor traps on swale drains, with check dams and rock protection used on steeper slopes where required.
- First-flush diversion will be installed for the pit area as well as the adjacent extensive hardstand area of the competitor parking and marshalling area, to capture initial stormwater run-off after an extended dry period.

## 5.3.3 Spill control and pollution management

To achieve spill control and pollution management in the high risk areas of the AMP, the following practices from *WQPN 28: Mechanical workshops and servicing* (DoW, 2013), *WQPN 52: Stormwater management at industrial sites* (DoW, 2006) and *WQPN 100: Motor sport facilities near sensitive waters* (DoW, 2007) will be implemented:

- Separation of uncontaminated stormwater from potentially contaminated stormwater (particularly roof water from other trafficked hardstands).
- Fuel / chemical handling areas (i.e. pits and maintenance areas) shall be located within secondary containment areas that allow maximum recovery of any spilt materials.
- Paved areas exposed to rainfall where dust, litter or spilt substances accumulate will be regularly cleaned by AMV Inc. personnel with methods that prevent fluid drainage or leaching into the surrounding environment.
- Oil and sediment traps (as appropriate to the site) will be installed at vehicle maintenance areas, and managed by AMV Inc. personnel (Section 4.2.2). First-flush water diversion to be installed for the pit area as well as the adjacent extensive hardstand area of the competitor parking and marshalling area to capture initial stormwater run-off after any extended dry period.
- Wash down of vehicles to occur in vehicle maintenance areas only. These areas feature a bunded impervious pad that is weatherproof to minimise stormwater access. Chemical solvents and non-degradable detergents used to clean equipment or pavements should not be released into stormwater systems. High pressure, steam cleaning, scrubbing or quick break detergents are the preferred methods of cleaning vehicles.

- Spill kits (permanent and mobile) will be located throughout the Site, comprising absorbent materials. AMV Inc. personnel will have necessary training on the handling of, and disposal of, hydrocarbons and spill kits. Any fuel/ chemical spills will be contained and remediated in accordance with the management strategies and actions outlined in the Hydrocarbon Management Plan prepared for the Site (GHD, 2021).

### **Water contamination barriers**

The following water contamination barriers are proposed, to prevent any loss of hydrocarbons and chemicals from the site:

- A 50 m grassed buffer (Development Exclusion Buffer) from the unnamed watercourse and Conservation Class wetland.
- A 200 m buffer from the unnamed water course and Conservation Class wetland to vehicle maintenance areas (as per DoW *WQPN 100*).

No permanent fuel, oil or chemical storage will occur on the Site. Temporary storage of fuel, oil and chemical solvents within the Site will occur within the bunded vehicle maintenance areas / pits.

- Covered, double bunded impervious vehicle maintenance areas with spill controls in place for hydrocarbon management. Runoff from these areas will be internally draining to a pit and pipe network connected to treatment devices including a sediment trap and pol water separator. Treated water shall outlet to the Site drainage network of swales and bioretention basins. Wastes and oily residue will be disposed to an approved off-site location (Section 4.2.2).
- Interceptor traps shall be installed and maintained throughout the swale network for treatment of track stormwater runoff.

It is noted that a swale exists within 200 m of the vehicle pits in the south-east of the site. Whilst water conveyance through the swale will improve water quality when compared to piped conveyance, it can also be considered a direct connection to the watercourse. It is proposed that all runoff from the pits and maintenance areas in this location should pass through an oil/water separator to remove contaminants before they enter the watercourse. Furthermore, the runoff from this area will pass through a compensating basin before entering the watercourse. This retarding effect on the runoff will allow a chance for the contaminants to settle and/or break down.

## **5.3.4 Emergency response plan**

In the event of a vehicle crash and/or fire, first response extinguishment will be via standard, portable dry chemical fire extinguishers (ABE type). The multipurpose ABE powder is a versatile extinguishant, which is used to extinguish Class A (carbonaceous), Class B (flammable liquid) and Class E (electrical) fires. When dry, the powder may be cleaned up with a vacuum cleaner, or similar. No larger firefighting apparatus are proposed for the AMP, and no firefighting foams are proposed.

As part of Motorsports Australia Regulations, each flag point (attended by a trained marshal) on a racetrack is required to have 2 × 9 kg fire extinguishers available. The AMP racetrack will likely have 5-6 flag points.

In the case of an emergency in the high risk areas of the AMP, the following actions from *WQPN 100: Motor sport facilities near sensitive waters* (DoW, 2007) will be implemented:

- A contingency plan shall be developed before the operational phase and be available on the Site in order to address emergency situations such as accidents, fires and chemical spills that could put local water resources including surface water and groundwater at risk. Relevant AMV Inc. personnel and contractors shall be familiar with the Site emergency response procedures.
- During larger events (potentially up to 20,000 for national race events), adequate emergency response services (e.g. firefighting, security, communications, medical personnel and emergency vehicle access) shall be provided.
- Portable spill kits and containment booms (land socks or similar) shall be kept at various locations, including flag points within the Site with absorbent material to soak up spilt oil, chemicals and/or fuel. Additionally, sand bags or coir logs will be used in the case of a vehicle accident to block flow to drains.

- The plan should be submitted to Water Corporation, City of Albany and Department of Fire and Emergency Services for advice before implementing.

### 5.3.5 Non-structural measures

There are a number of temporary and non-structural measures are also key management measures for the development and operation of the Site.

#### **Construction**

Construction sites can be a major source of silt and other pollutants. Proponents and builders shall be encouraged to undertake good practice on building sites through preparation of a site-specific Construction Environmental Management Plan (Section 6).

A separate Construction Management Plan is also included the in the AMP Environmental Management Plan.

#### **Maintenance**

Regular maintenance of the Site drainage system shall be undertaken prior to the start of the wet season. Cleaning of the drainage system, including base of swale drains, interceptor traps in swale drains and bioretention basins will provide an opportunity to remove gross pollutants and silt build up that may enter the receiving water bodies after heavy rainfall. Any vegetation disturbed in the swales and bioretention basins will be re-established to ensure water quality treatment.

In addition to transporting pollutants, drains with accumulated pollutants may also overflow, leading to localised flooding and erosion, and risks to human safety and constructed assets. Maintenance may also include erosion control measures such as rock pitching if required.

#### **Revegetation and landscape management**

- Revegetation of the Protected Exclusion Area (Figure 2), which encompasses the Conservation Class wetland and creek line, shall be undertaken as part of the development. Revegetation shall comprise suitable wetland species identified by Bio Diverse Solutions (2019), including Unit 13, Unit 47 and Unit 49 from the *Albany Regional Vegetation Survey Extent* (Sandiford & Barrett, 2010). The proposed native wetland revegetation species will assist in uptake of nutrients and trap sediment in surface runoff and shallow groundwater discharging to the wetland area. These native species include *Baumea juncea* and *Baumea rubiginosa* which are frequently used in bioretention areas for their nutrient uptake abilities.
- A 50 m wide, low fuel 'Development Exclusion Buffer' comprising a managed grass area will provide a further buffer for stormwater runoff from the development, and any overflow from bioretention basins. The managed grass buffer will assist to filter and trap sediments and nutrients in overland flow discharged to the unnamed creek line / wetland.
- Use of pesticides and fertilisers shall be limited, and completely excluded within the Protected Exclusion Area and Development Exclusion Buffer. Refer to the Protected Exclusion Area Management Plan in the AMP Environmental Management Plan. Use of herbicides shall be in accordance with the *Use of herbicides in water catchment areas* (Circular No: PSCBB, Department of Health).

#### **Erosion and sediment control**

A range of measures will be implemented throughout the Site to minimise erosion and prevent sediment loss from the Site impacting on downstream receptors. Erosion and sediment control measures during construction are detailed in Section 6.

During operation of the Site the erosion and sediment control measures include:

- Sediment traps installed in vehicle maintenance areas.
- Drainage swales that convey stormwater runoff will be vegetated with grass to promote sedimentation and feature regularly spaced interceptor traps.
- The base of drainage swales and diversion drains in higher slope areas will be rock protected and feature regular rock weirs and/or check dams to reduce flow velocity.

## 6. Construction management

Potential impacts to water resources during construction activities include:

- Soil erosion – construction would result in the exposure of the natural ground surface and subsurface through the removal of vegetation, and excavation and landforming works within the Site which may increase the potential for soil erosion to occur. There is further potential for mobilisation of dust associated with the construction works.
- Surface water quality – construction of the project has the potential to impact surface water quality through the pollution of runoff with sediments, fuel and other hazardous materials from the construction site.
- Disturbance of acid sulfate soils – potential for construction activities to disturb acid sulfate soils.

### 6.1 Construction Environmental Management Plan

The AMP Environmental Management Plan includes a specific Construction Management Plan, which outlines objectives, broad strategies and actions required to minimise environmental impacts associated with construction of the AMP. The Construction Management Plan applies to the GSMG and all appointed contractors during the construction of the AMP.

It is recommended that a site-specific Construction Environmental Management Plan (CEMP) be prepared for the Site that addresses the management of construction works to ensure no detrimental impacts to the receptors. The CEMP should be referred to DWER for approval. The CEMP shall be maintained during the construction period and Site establishment period and include:

- Temporary bunds, coir logs and silt fences to prevent silt runoff into the drainage system
- Litter and waste storage bins to prevent litter to be blown by wind or washed by rainfall
- Establishing a washing-down area behind the bund or silt fence
- Provide a stabilised entry and exit point to prevent vehicle tracking of soil from the building site onto roads
- Position stockpiles of sand and soil stockpiles to prevent material being tracked, washed, or blown into roads, and then into existing surface drainage or constructed stormwater systems.

### 6.2 Acid Sulfate Soil Management Plan

Surface and/ or groundwater may also become contaminated through the exposure of ASS during construction (excavation). ASS disturbance may have a range of impacts including enhanced phosphorus leaching, death of vegetation irrigated with affected water, the smothering of benthic aquatic animals by the precipitation of iron, and metal bioaccumulation in aquatic plants and animals. However, based on the ASS assessments to date (refer to Section 2.3.3), inorganic sulfidic sources capable of rapid acid release upon disturbance were not observed. Other, more slow releasing acidity sources were observed in the ASS assessment and will require management if disturbed in volumes greater than 100 m<sup>3</sup>.

The following ASS management recommendations are made with regards to the proposed redevelopment:

- Topsoil (0-300 mm) appears acceptable to be stripped and stockpiled for reuse without treatment (pH on average above 4 across the site).
- Neutralisation treatment and validation of soils *will be required* for silty sand soil units disturbed in the proximity of the watercourse area given that there are exceedances of the DWER action criteria (coarse textured soils) *and* if the proposed disturbance of greater than 100 m<sup>3</sup> of soil.
- An ASS management plan will be required (in accordance with DWER guidelines) to enable to the effective excavation, treatment and disposal/reuse of the materials during construction works.
- Soil excavations should only occur during the periods of the year where groundwater is at its lowest point (i.e. outside of winter and post-winter periods) to eliminate the need for temporarily lowering the groundwater table (dewatering). If dewatering is determined to be required, then site specific dewatering risk assessment, management strategies and criteria are required to be developed, approved and implemented.

# 7. Monitoring

## 7.1 Monitoring requirements

The objective of the surface water and groundwater monitoring is to assess the operation of the Site against the design criteria (Section 3) and baseline water quality (Section 2.4.5).

Monthly monitoring of surface and groundwater conditions will be completed during the construction and operational period. The monitoring data will be compared to baseline data (Section 2.4.5) to ensure no adverse impacts from construction and operation of the Site on the surface water and groundwater quality and levels.

Event based monitoring will be completed at key locations of drainage infrastructure (bioretention basins) to assess stormwater drainage performance in improving stormwater quality. It is assumed the first flush events will have the highest level of nutrients and chemicals, therefore sampling should occur at the time/after the first significant rainfall event of each wet season, and after extended dry periods. Field notes should include details of the rainfall events, site conditions, time of sampling and time of sample testing.

Additional sampling should also be undertaken in response to any spill events.

A summary of the proposed surface water monitoring program is provided in Table 14. The proposed groundwater monitoring program is provided in Table 15, and the groundwater monitoring sites are shown on Figure 6.

Table 14: Summary of surface water monitoring

Site	Frequency	Duration	Parameters
<b>Surface water</b> - Upstream of the site (TBC) - Mid-stream (CS02) - Downstream of the site (CS01)	Monthly	On-going, with annual reporting	In-situ: pH, EC, temperature  Unfiltered sample: pH, EC, TN, FRP, TKN, ammonia, TP, TRH, PAH, BTEXN, surfactants, microbial analysis
<b>Compensating basin</b> - Inlet (6 No.) and Outlet (6 No.) West-B1 West-B7 East-B3 East-B5 East-B6 East-B10 <b>Sub-catchment Inlets and Outlets</b> West 1 Outlet Only (4WD training area) West 3 (DS Culvert W-EXT-CULV & DS Culvert W-CULV1) East 3 Outlet East 1 Outlet (DS of East-E9)	3-4 events per year following 1EY rainfall events or greater		Filtered sample: Filtered total nitrogen and filtered total phosphorus (to quantify organic component), NO <sub>2</sub> /NO <sub>3</sub> , PO <sub>4</sub> , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)

Table 15: Summary of groundwater monitoring program

Site	Frequency	Duration	Parameters
Monitoring bores (up to 6 bores across the site locations to be confirmed) To include SB04, SB03, SB08, SB09 and 2 others Production bore/s (location to be confirmed)	Monthly	On-going, with annual reporting	Water level  In-situ: pH, EC, temperature  Unfiltered sample: pH, EC, TN, FRP, TKN, ammonia, TP, TRH, PAH, BTEXN, surfactants, microbial analysis  Filtered sample: Filtered total nitrogen and filtered total phosphorus (to quantify organic component), NO <sub>2</sub> /NO <sub>3</sub> , PO <sub>4</sub> , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)

## 7.2 Quality assurance and quality control

A surface and groundwater monitoring plan will be prepared to support ongoing monitoring of the Site for submission and approval by DWER and Water Corporation.

Monitoring will be completed in accordance with the requirements of the *Australian and New Zealand guidelines for fresh and marine water quality* (ANZECC, 2018). Sample collection, processing, transportation, storage, preservation and labelling of water samples will be conducted in accordance with the appropriate industry standards and general water sampling guidance (AS/NZS 5667.1:1998), with collected samples analysed in a NATA accredited laboratory.

Post-development, permanent groundwater monitoring bore locations and sites should be identified and constructed in accordance with industry standards (ASTM D5092/ D5092-16, *Standard practice for design and installation of groundwater monitoring bores*).

## 7.3 Contingency plan

Should monitoring of groundwater and/ or surface water identify that water quality objectives are not being met the following contingency measures will be implemented:

- Investigate the source or cause of elevated contaminants through site investigation and/or additional monitoring if required.
- Review installation of stormwater management BMPs to ensure they are designed, installed and maintained as required.
- Review implementation of Site procedures for incident management to ensure appropriate measures are undertaken to respond to incidents such as spills and accidents.
- Should further monitoring identify that water quality objectives are not being met, AMV Inc. will notify DWER and the City of Albany to determine requirements further site investigation or remediation actions.

A water quality response and contingency plan will be developed in consultation with the Water Corporation, City of Albany and DWER. The water quality response and contingency plan shall be included in the surface and groundwater monitoring plan.

## 7.4 Reporting

The AMV Inc. will prepare an annual water quality monitoring report for submission to the DWER and Water Corporation. The annual water monitoring report will summarise surface water and groundwater monitoring results for the calendar year, including comparison to baseline data and previous years of monitoring. The annual report will include summary reporting of any water quality exceedance, including parameters exceeding water quality objectives, measures taken to investigate exceedances, results of additional monitoring and any further actions undertaken.

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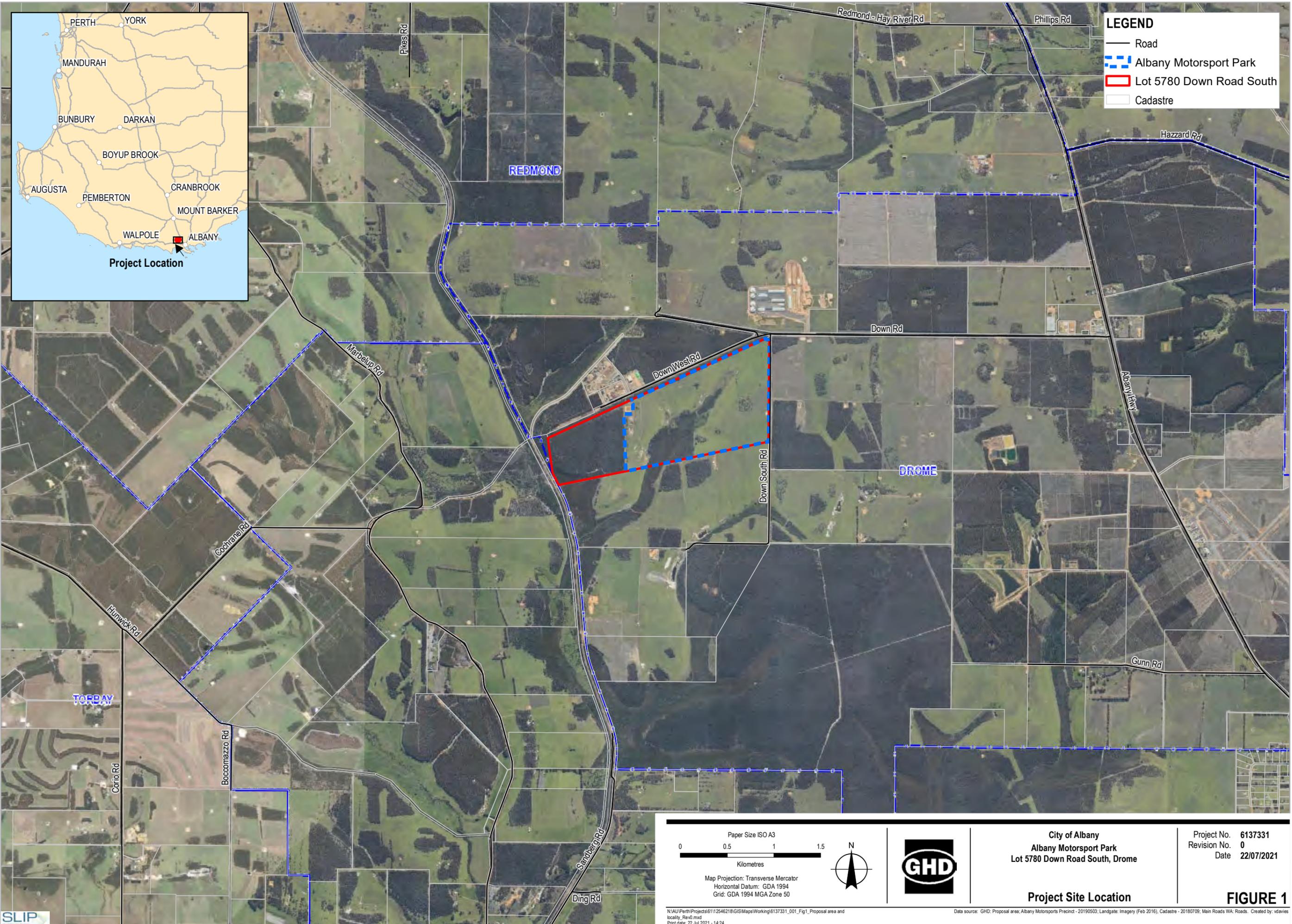
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# Appendices

# Appendix A

## Figures

- Figure 1*      *Project site location*
- Figure 2*      *Master Plan*
- Figure 3*      *DPIRD soil landscape mapping*
- Figure 4*      *South Coast Significant Wetlands and extrapolated ASS risk mapping*
- Figure 5*      *PDWSA and Water Management Areas*
- Figure 6*      *Pre-development catchment plan*
- Figure 7*      *1% AEP pre-development maximum flood depths*
- Figure 8*      *1% AEP pre-development maximum flow velocities*
- Figure 9*      *Stormwater Management Plan – Stage 1A*
- Figure 10*     *Stormwater Management Plan – Stage 1B*



**LEGEND**

- Road
- ▬▬▬ Albany Motorsport Park
- ▭ Lot 5780 Down Road South
- ▭ Cadastre



Paper Size ISO A3

0 0.5 1 1.5

Kilometres

Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50



City of Albany  
 Albany Motorsport Park  
 Lot 5780 Down Road South, Drome

Project No. 6137331  
 Revision No. 0  
 Date 22/07/2021

**Project Site Location**

**FIGURE 1**

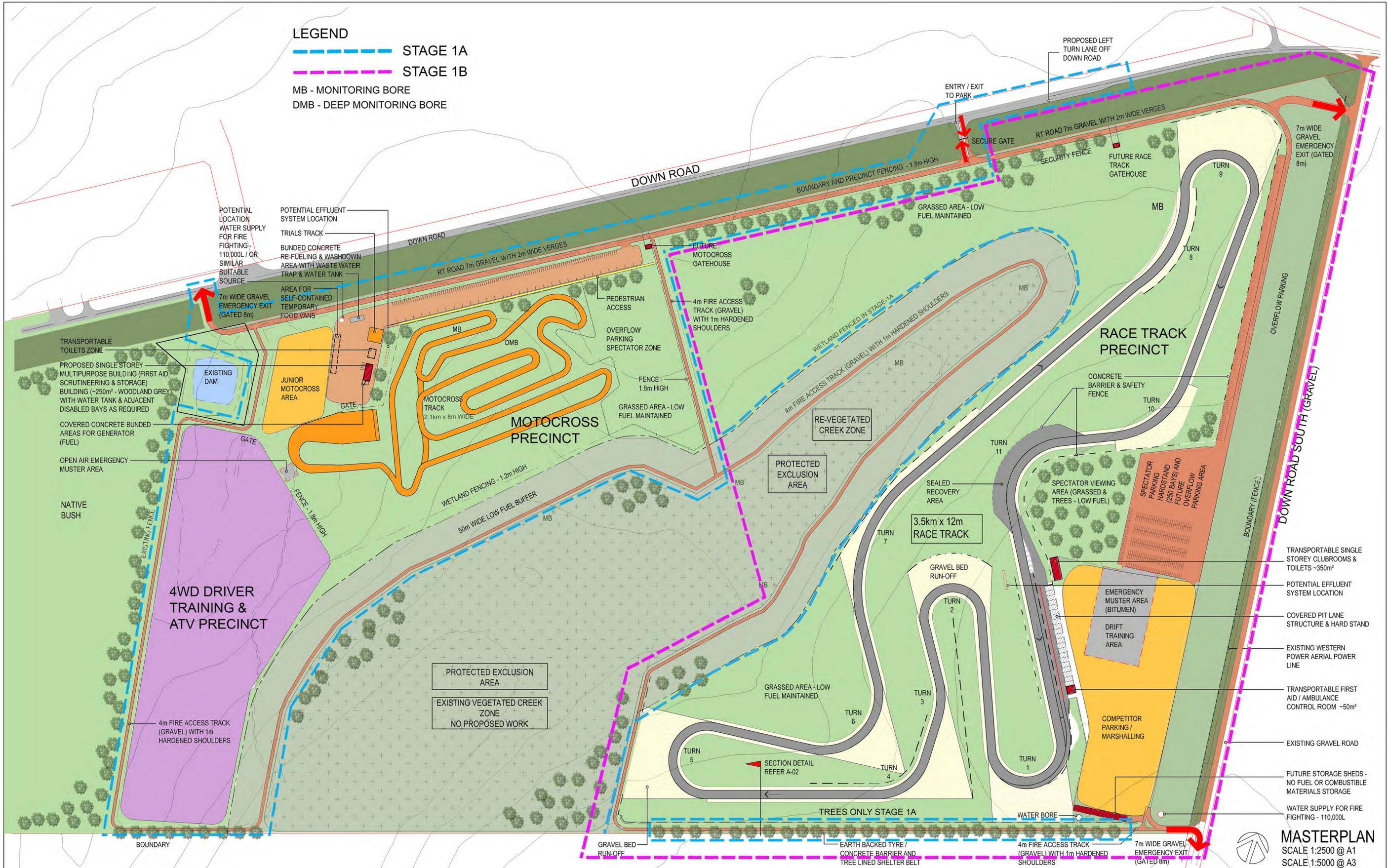
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Data source: GHD: Proposal area; Albany Motorsports Precinct - 20190503; Landgate: Imagery (Feb 2016); Cadastre - 20180709; Main Roads WA: Roads. Created by: vdvavies



**LEGEND**

- STAGE 1A
- STAGE 1B
- MB - MONITORING BORE
- DMB - DEEP MONITORING BORE



**MASTERPLAN**  
 SCALE 1:2500 @ A1  
 SCALE 1:5000 @ A3

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rev	date	description
A	15-04-2021	ISSUED FOR CLIENT REVIEW
B	27-04-2021	ISSUED FOR CLIENT REVIEW
C	12-05-2021	ISSUED FOR CLIENT REVIEW
D	26-05-2021	ISSUED FOR CLIENT REVIEW
E	05-07-2021	ISSUED FOR DA

p.o. box 1502, albany, western australia 6331  
 telephone: (08) 9841 5455  
 email: admin@rgarchitects.com.au



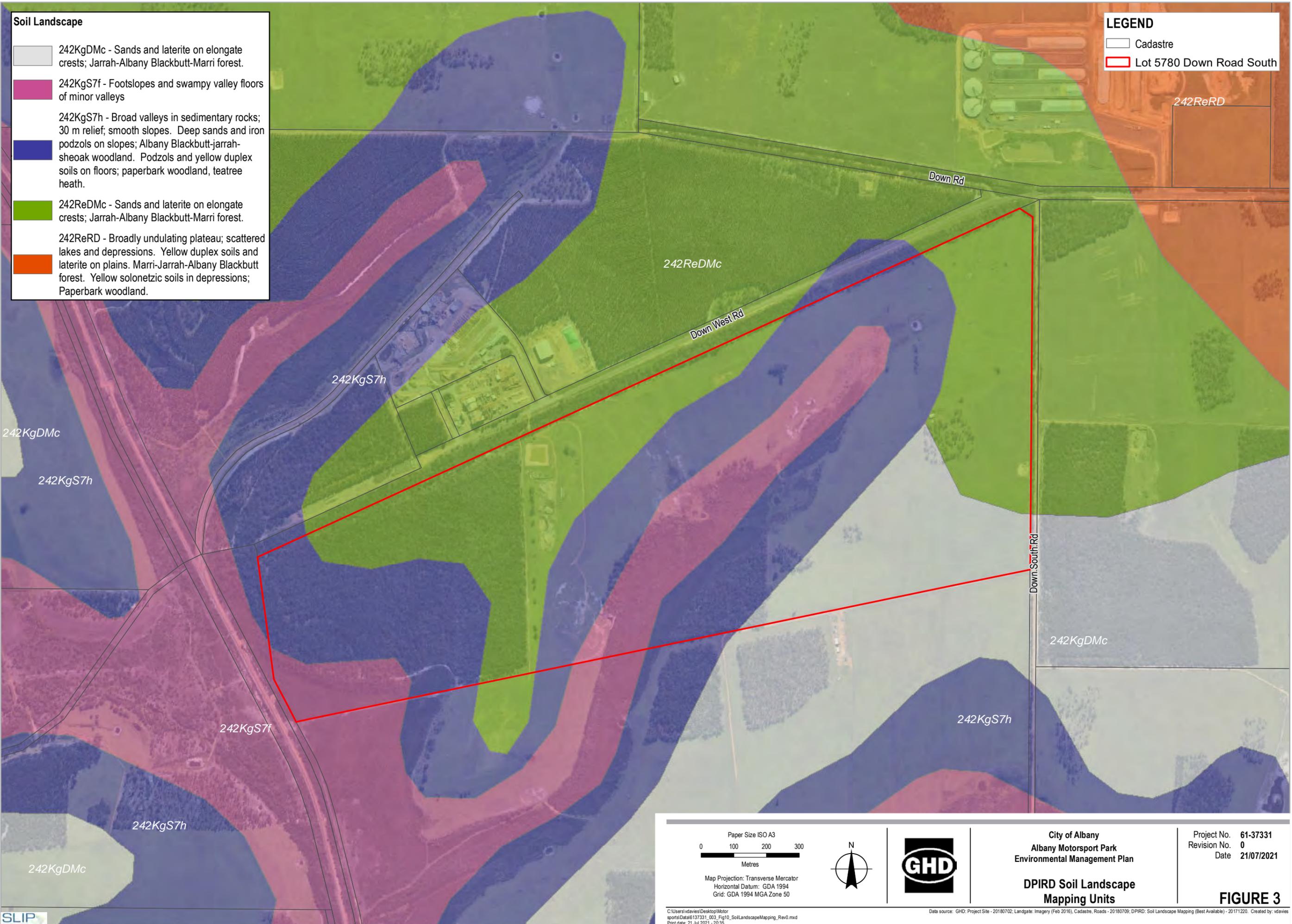
project  
**Albany Motorsport Park**  
 Lot 5780 Down Rd, Drome, WA 6330  
 client  
 City of Albany

Masterplan - Stage 1

cad file

drawn CB project number 21-002

scale	date	dwg no.	rev.
1:2500 @ A1	JULY 2021	A-01	E



**Soil Landscape**

- 242KgDMc - Sands and laterite on elongate crests; Jarrah-Albany Blackbutt-Marri forest.
- 242KgS7f - Footslopes and swampy valley floors of minor valleys
- 242KgS7h - Broad valleys in sedimentary rocks; 30 m relief; smooth slopes. Deep sands and iron podzols on slopes; Albany Blackbutt-jarrah-sheoak woodland. Podzols and yellow duplex soils on floors; paperbark woodland, teatree heath.
- 242ReDMc - Sands and laterite on elongate crests; Jarrah-Albany Blackbutt-Marri forest.
- 242ReRD - Broadly undulating plateau; scattered lakes and depressions. Yellow duplex soils and laterite on plains. Marri-Jarrah-Albany Blackbutt forest. Yellow solonetzic soils in depressions; Paperbark woodland.

**LEGEND**

- Cadastre
- Lot 5780 Down Road South

242KgDMc  
242KgS7h  
242KgS7f  
242KgS7h  
242KgDMc

242KgS7h

242ReDMc

242KgDMc

242KgS7h

242KgS7h

Paper Size ISO A3  
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Metres

Map Projection: Transverse Mercator  
Horizontal Datum: GDA 1994  
Grid: GDA 1994 MGA Zone 50

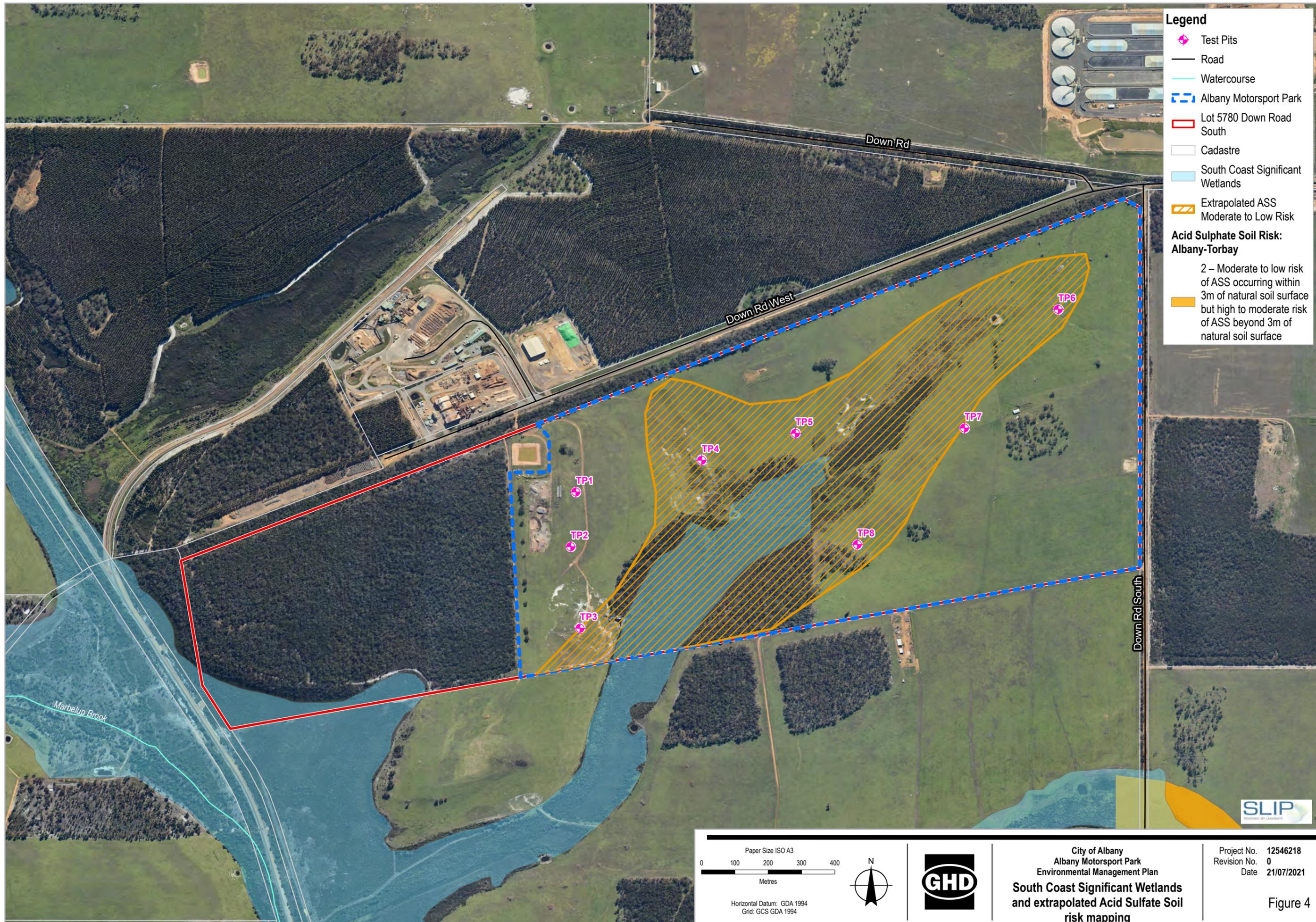


City of Albany  
Albany Motorsport Park  
Environmental Management Plan

**DPIRD Soil Landscape  
Mapping Units**

Project No. 61-37331  
Revision No. 0  
Date 21/07/2021

**FIGURE 3**



**Legend**

- Test Pits
- Road
- Watercourse
- Albany Motorsport Park
- Lot 5780 Down Road South
- Cadastre
- South Coast Significant Wetlands
- Extrapolated ASS Moderate to Low Risk

**Acid Sulphate Soil Risk: Albany-Torbay**

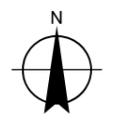
2 – Moderate to low risk of ASS occurring within 3m of natural soil surface but high to moderate risk of ASS beyond 3m of natural soil surface

Paper Size ISO A3

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Metres

Horizontal Datum: GDA 1994  
Grid: GCS GDA 1994



City of Albany  
Albany Motorsport Park  
Environmental Management Plan

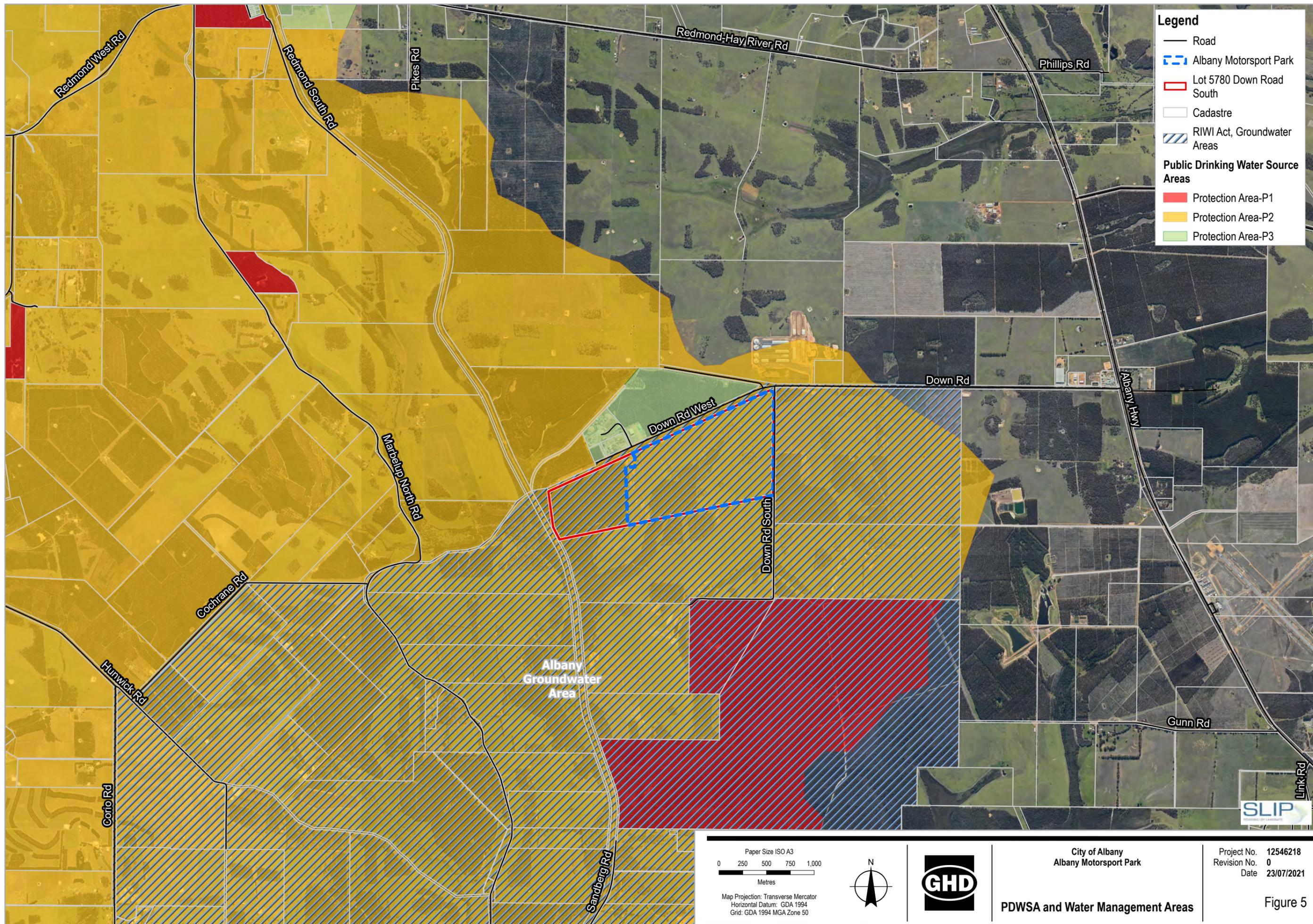
**South Coast Significant Wetlands and extrapolated Acid Sulphate Soil risk mapping**

Project No. 12546218  
Revision No. 0  
Date 21/07/2021

Figure 4

N: \\AU\Perth\Projects\6112546218\GIS\Maps\Working\12546218\12546218\_EnvironmentalManagementPlan\12546218\_EnvironmentalManagementPlan.aprx1254  
Print date: 21 Jul 2021 - 13:43

Data source: Landgate\_Subscription\_Imagery\WAnow: Landgate / SLIP. Created by: v-davies



**Legend**

- Road
- ▭ Albany Motorsport Park
- ▭ Lot 5780 Down Road South
- ▭ Cadastre
- ▨ RIWI Act, Groundwater Areas

**Public Drinking Water Source Areas**

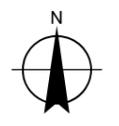
- ▭ Protection Area-P1
- ▭ Protection Area-P2
- ▭ Protection Area-P3

Paper Size ISO A3

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Metres

Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50

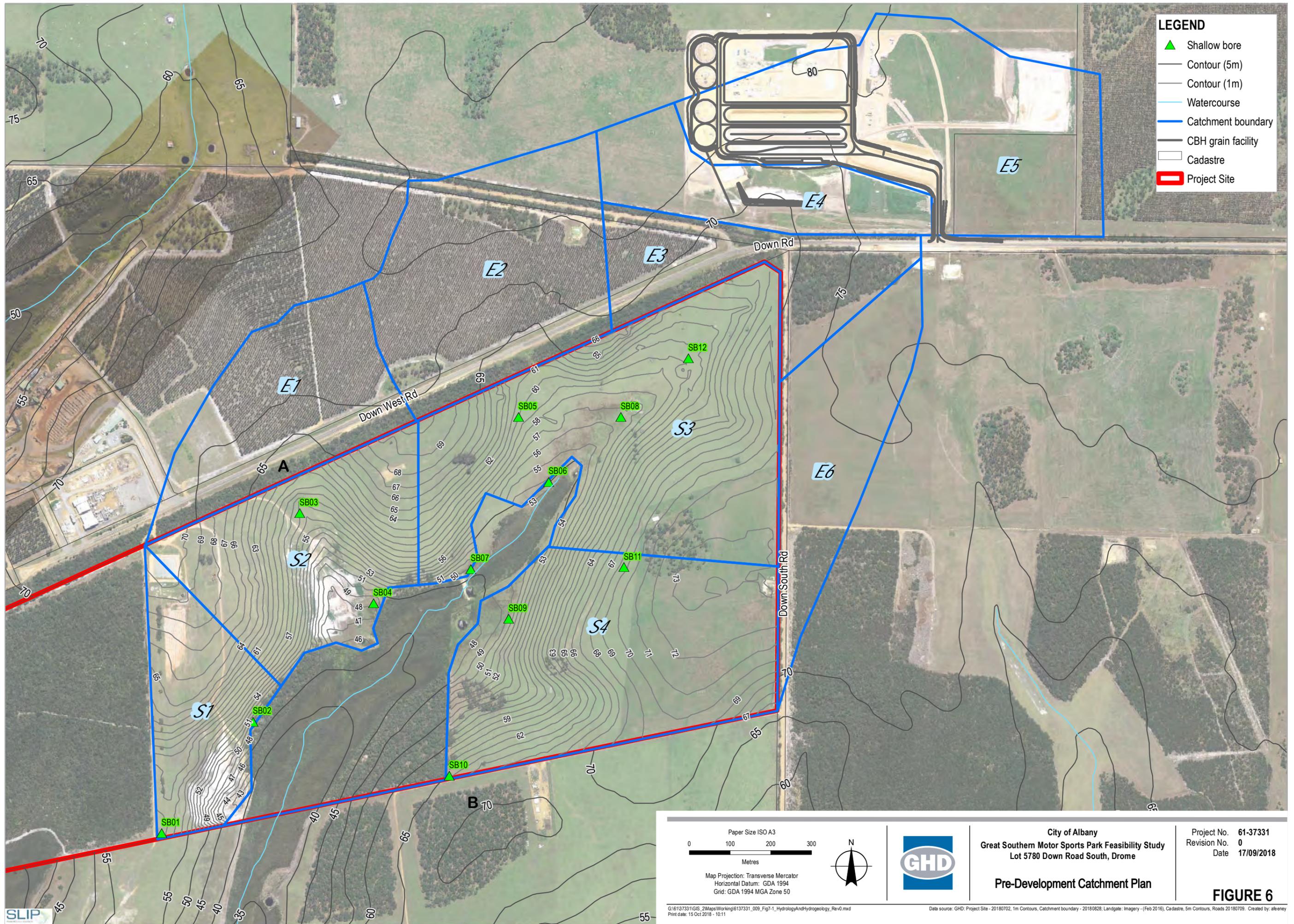


City of Albany  
 Albany Motorsport Park

**PDWSA and Water Management Areas**

Project No. 12546218  
 Revision No. 0  
 Date 23/07/2021

Figure 5



**LEGEND**

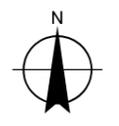
- ▲ Shallow bore
- Contour (5m)
- Contour (1m)
- Watercourse
- Catchment boundary
- CBH grain facility
- ▭ Cadastre
- ▭ Project Site

Paper Size ISO A3

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Metres

Map Projection: Transverse Mercator  
Horizontal Datum: GDA 1994  
Grid: GDA 1994 MGA Zone 50

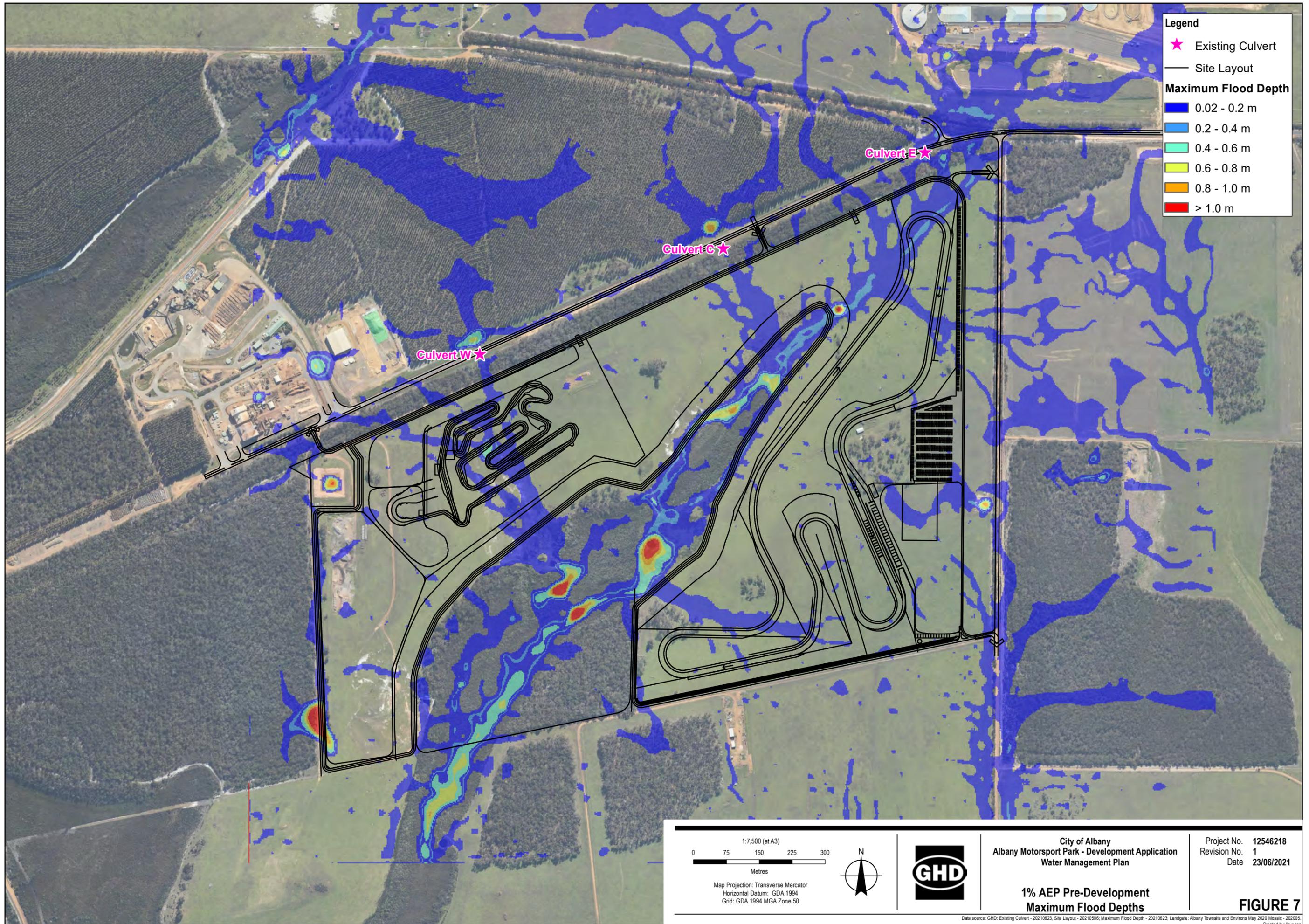


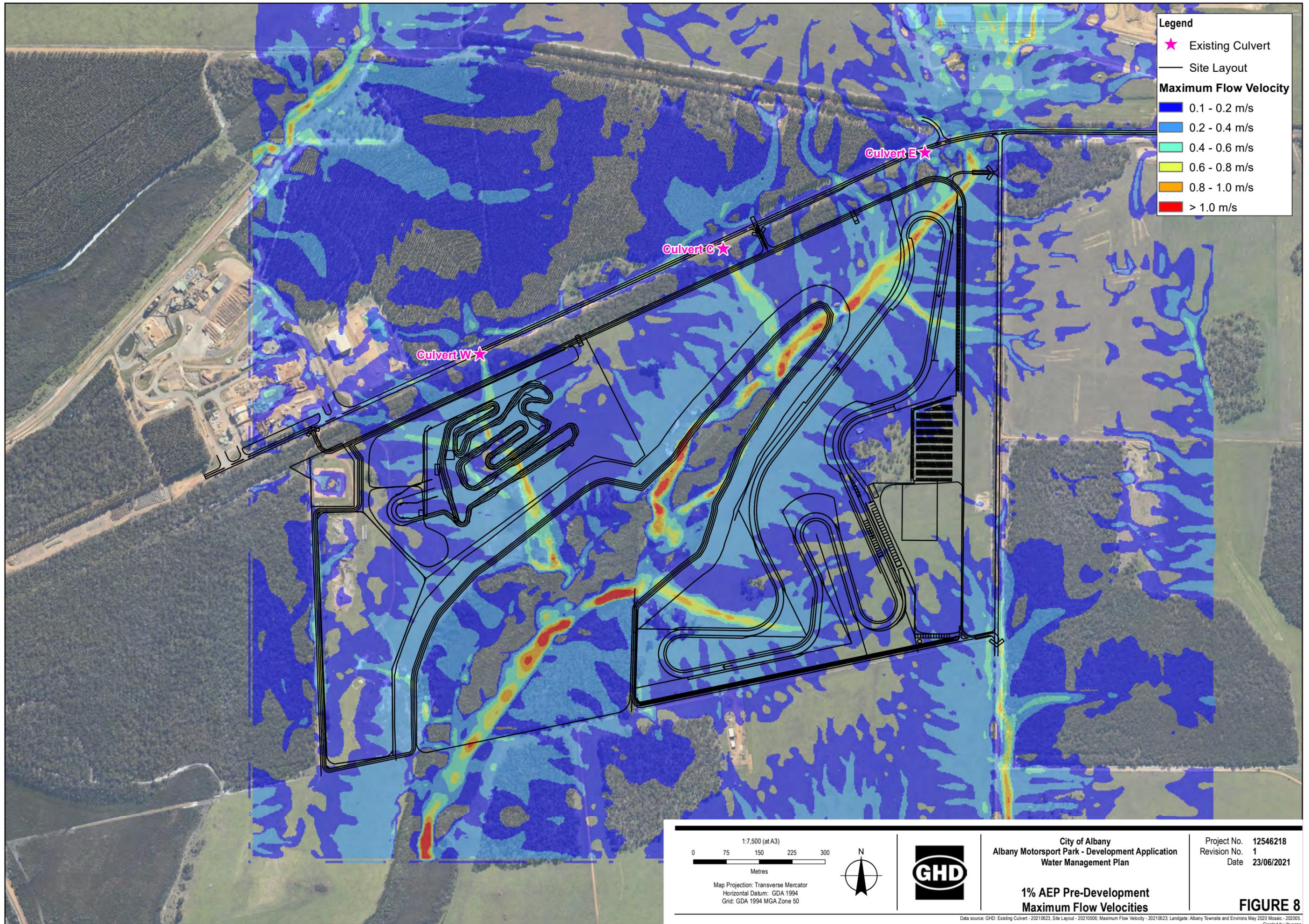
City of Albany  
Great Southern Motor Sports Park Feasibility Study  
Lot 5780 Down Road South, Drome

**Pre-Development Catchment Plan**

Project No. 61-37331  
Revision No. 0  
Date 17/09/2018

**FIGURE 6**



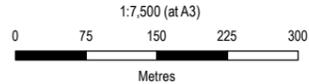


**Legend**

- ★ Existing Culvert
- Site Layout

**Maximum Flow Velocity**

- 0.1 - 0.2 m/s
- 0.2 - 0.4 m/s
- 0.4 - 0.6 m/s
- 0.6 - 0.8 m/s
- 0.8 - 1.0 m/s
- > 1.0 m/s



Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50



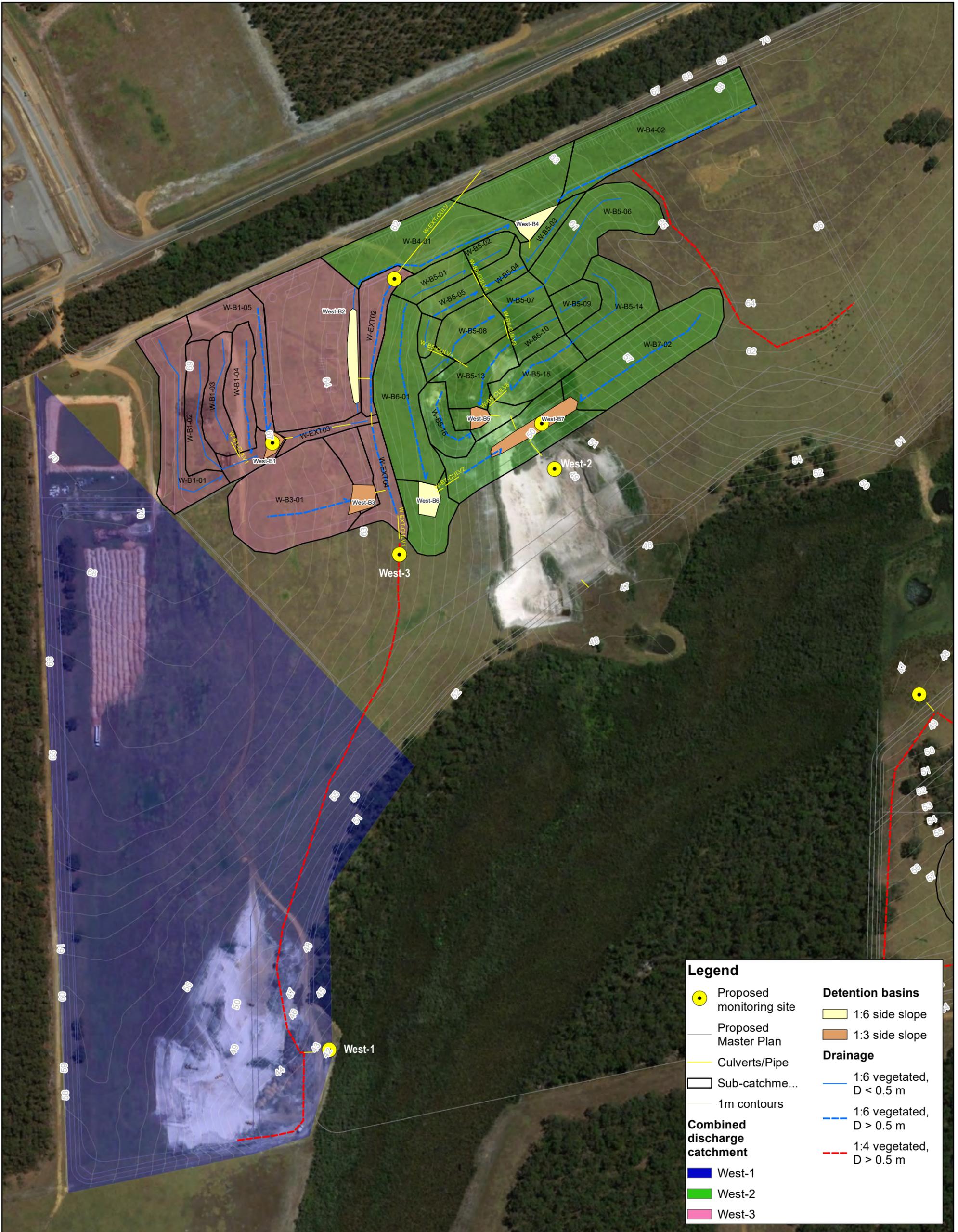
City of Albany  
 Albany Motorsport Park - Development Application  
 Water Management Plan

1% AEP Pre-Development  
 Maximum Flow Velocities

Project No. 12546218  
 Revision No. 1  
 Date 23/06/2021

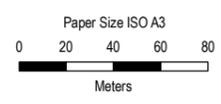
**FIGURE 8**

Data source: GHD; Existing Culvert - 20210623; Site Layout - 20210506; Maximum Flow Velocity - 20210623; Landgate: Albany Townsite and Environs May 2020 Mosaic - 202005. Created by: Ihyoung



**Legend**

- Proposed monitoring site
- Proposed Master Plan
- Culverts/Pipe
- Sub-catchme...
- 1m contours
- Combined discharge catchment
  - West-1
  - West-2
  - West-3
- Detention basins**
  - 1:6 side slope
  - 1:3 side slope
- Drainage**
  - 1:6 vegetated, D < 0.5 m
  - 1:6 vegetated, D > 0.5 m
  - 1:4 vegetated, D > 0.5 m



Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50

City of Albany  
 Albany Motorsport Park

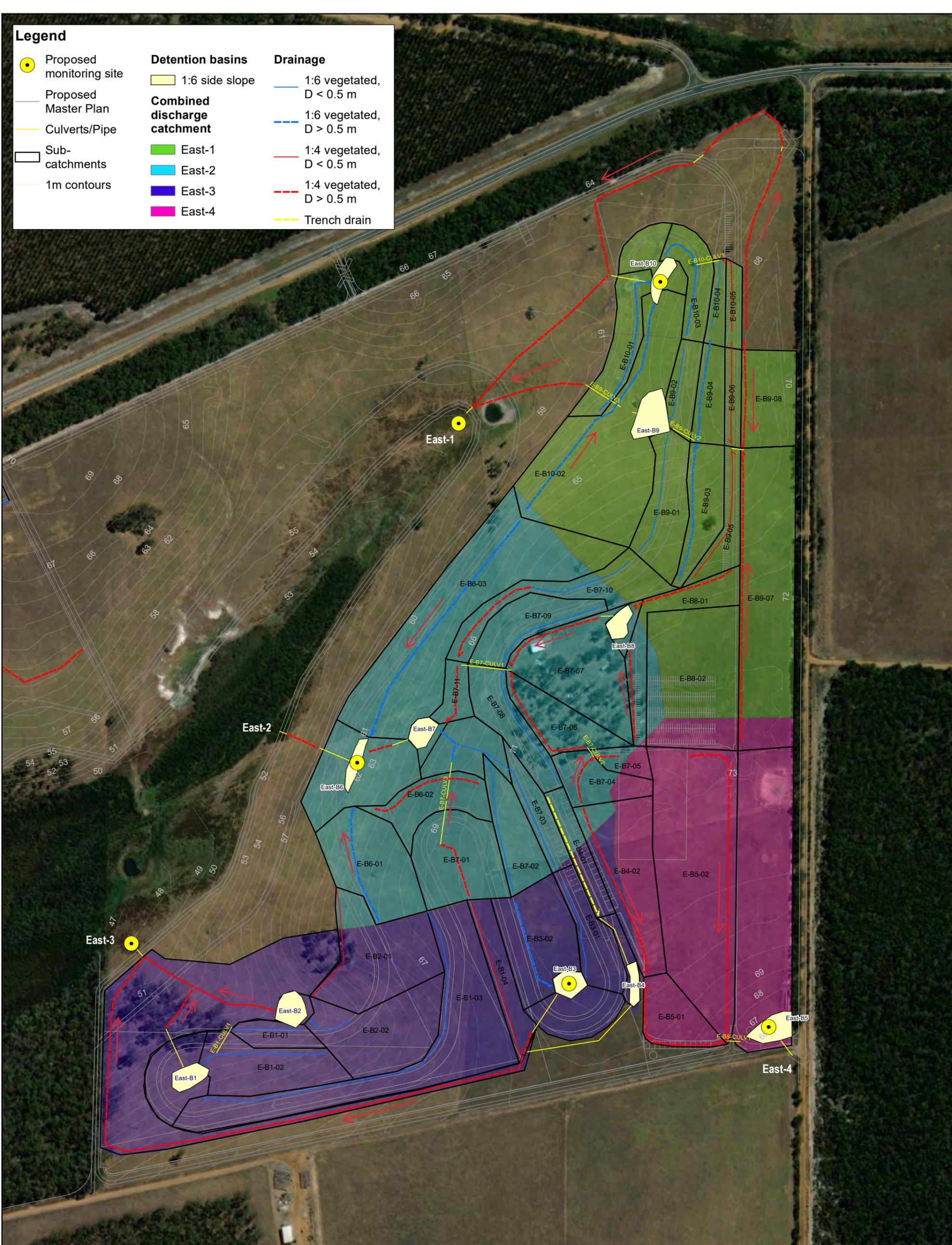
**Stage 1A  
 Drainage Management Plan**

Project No. 12546218  
 Revision No. A  
 Date 16/07/2021

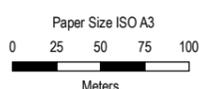
**FIGURE 9**

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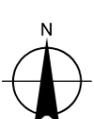
Data source: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community. Created by: bchernandez



Legend		
	Proposed monitoring site	
	Proposed Master Plan	
	Culverts/Pipe	
	Sub-catchments	
	1m contours	
	Detention basins	
	1:6 side slope	
	Combined discharge catchment	
	East-1	
	East-2	
	East-3	
	East-4	
	Drainage	
	1:6 vegetated, D < 0.5 m	
	1:6 vegetated, D > 0.5 m	
	1:4 vegetated, D < 0.5 m	
	1:4 vegetated, D > 0.5 m	
	Trench drain	



Map Projection: Transverse Mercator  
Horizontal Datum: GDA 1994  
Grid: GDA 1994 MGA Zone 50



City of Albany  
Albany Motorsport Park

**Stage 1B  
Drainage Management Plan**

Project No. 12546218  
Revision No. A  
Date 16/07/2021

**FIGURE 10**

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Print date: 22 Jul 2021 - 17:27

Data source: Source: Esri, Maxar, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community. Created by: bohemandez

# Appendix B

**Albany Motorsport Park Development,  
Pavement Investigation (Great Southern  
Geotechics , 2021)**



# GREAT SOUTHERN GEOTECHNICS

CONSTRUCTION MATERIALS TESTING

## Pavement Investigation

**Report 4212/1**

Friday, 9 April 2021

**GHD**

Albany Motorsport Park Development

# GREAT SOUTHERN GEOTECHNICS

## 1.0 INTRODUCTION

As authorised by GHD

an investigation for the proposed Albany Motorsport Park Development adjacent to Down Rd, Mirambeena was performed on the 25/03/2021

## 2.0 GENERAL

The intent of the investigation was to determine the following:

- Soil types and profiles.
- Characteristics of soil properties on select samples including Particle Size and Consistency Limits. ( Liquid Limit, Plastic Limit, Plasticity Index & Linear Shrinkage).
- In Situ permeability rates. ( Where applicable )
- Groundwater levels at time of investigation.

## 3.0 SITE INVESTIGATION

Site conditions and test pit locations were recorded and are displayed in [Appendix A - Maps](#).

Test pits logs various materials types are noted in [Appendix B - Test Pit Logs](#)

The field investigation consisted of 8 Boreholes excavated on-site to depths of up to 2.5 meters using a Kubota KX41-3V mini excavator with a 300mm Auger.

Test pits were spread across the extent of the proposed development and locations were predetermined by GHD.

All soil layers encountered were visually assessed and classified on-site.

Samples gathered from site were the taken back to Great Southern Geotechnics Albany Laboratory For further processing and analysis.

**IMPORTANT NOTE:** The test pits have been spread so that they are representative of the subsurface materials across the intended reconstruction area, however, soil conditions may change dramatically over short distances and our investigations may not locate all soil variations across the site.

## 4.0 LABORATORY TESTING

Results of any relevant Laboratory testing preformed are shown in [Appendix C. \( Test Results Report 4212/2 \)](#)

This report and associated documentation was undertaken for the specific purpose described in the report and shall not be relied on for other purposes.

This report was prepared solely for the use by GHD any reliance assumed by other parties on this report shall be at such parties own risk.



# **Appendix A**

## Maps



# Figure 1

Test Pits 1 to 8

## Test Pit Locations



**GREAT SOUTHERN  
GEOTECHNICS**  
CONSTRUCTION MATERIALS TESTING

Job No: 4212  
Client: GHD  
Project: Albany Motorsport Park Development





# **Appendix B**

Test Pit Logs





**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°55'58.4"S 117°44'13.1"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 200	200	<b>(Topsoil) SAND with silt:</b> Dark grey, fine to medium. Roots and root fibres.	M	MD		No water table encountered.		
200 - 550	350	<b>SANDY gravel:</b> Brown, fine to coarse, sub-rounded to sub-angular. Fine to medium grained sand.	M	MD-D				
550 - 2500	1950	<b>Sandy CLAY:</b> Low to medium plasticity, light brown/orange mottled red. Fine to medium grained sand.	M	F				

				Target Depth	✓	2500
				Cave In		
				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.1



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°56'03.7"S 117°44'12.6"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 100	100	<b>(Topsoil) SAND with silt:</b> Dark grey, fine to medium. Roots and root fibres.	M	MD		No water table encountered.		
100 - 500	400	<b>SANDY gravel:</b> Brown, fine to coarse, sub-rounded to sub-angular. Fine to medium grained sand.	M	MD-D				
500 - 2500	2000	<b>Sandy CLAY:</b> Low to medium plasticity, light brown/orange mottled red. Fine to medium grained sand.	M	F				

				Target Depth	✓	2500
				Cave In		
				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
<b>Cohesive</b>	<b>Non-Cohesive</b>	<b>Rock</b>	<b>Cementation</b>	<b>General</b>		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.2



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°56'11.6"S 117°44'13.5"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 160	160	<b>(Topsoil) Gravelly SAND with silt:</b> Grey/brown, fine to medium. Fine to medium, sub-rounded to sub-angular, gravel.	DM	L-MD		No water table encountered.		
160 - 2100	1940	<b>(FILL) Sandy GRAVEL with clay:</b> Low to medium plasticity, brown/red Fine to coarse, sub-rounded to sub-angular gravel. Fine to medium grained sand.	M	MD				
2100 - 2500	400	<b>SAND with silt:</b> White, fine.	M	L-MD				

				Target Depth	✓	2500
				Cave In		
				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.3



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°55'55.3"S 117°44'25.3"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 50	50	(Topsoil) SAND with silt: Grey, fine to medium. Roots and root fibres.	D	L		No water table encountered.		
50 - 850	800	SAND with silt: Light grey/white, fine to medium.	D-M	L-MD				
850 - 2500	1650	SAND with silt: Brown, fine to medium.	M	D	WC			

				Target Depth	✓	2500
				Cave In		
				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.4



**Excavation**



**Spoil**



**GREAT SOUTHERN  
GEOTECHNICS**  
CONSTRUCTION MATERIALS TESTING

**Job No:** 4212  
**Client:** GHD  
**Project:** Albany Motorsport Park Development

**Sheet** 8 **of** 16



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°55'52.7"S 117°44'34.4"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 240	240	(Topsoil) SAND with silt: Grey, fine to medium. Roots and root fibres.	D	L-MD		No water table encountered.		
240 - 1100	860	SAND with silt: Light grey/white, fine to medium.	M	L-MD				
1100 - 2500	1400	Gravelly SAND with silt: Light brown, fine to medium. Fine to medium, sub-rounded to sub-angular gravel.	M	MD	PC			

				Target Depth	✓	2500
				Cave In		
				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.5



**Excavation**



**Spoil**



**GREAT SOUTHERN  
GEOTECHNICS**  
CONSTRUCTION MATERIALS TESTING

**Job No:** 4212  
**Client:** GHD  
**Project:** Albany Motorsport Park Development

**Sheet** 10 **of** 16



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°55'40.7"S 117°44'59.9"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 180	180	(Topsoil) SAND with silt: Grey, fine to medium. Roots and root fibres.	M	L-MD		No water table encountered.			
180 - 1400	1220	SAND with silt: Light grey/white, fine to medium.	M	L-MD					
1400 - 2500	1100	SAND with silt: Light brown, fine to medium.	M	MD-D	MC				

\*Cobbles noted on outer edge of test pit in shoulder.

Target Depth	✓	2500
Cave In		
Refusal		
Near Refusal		
Flooding		
Lack of Reach		

Cohesive	Non-Cohesive	Rock	Cementation	General
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented	
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented	
St - Stiff	D - Dense	M - Medium		
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented	
H - Hard	CO - Compact	VH - Very High		
		EH - Extremely High		

## Test Pit No.6



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°55'52.2"S 117°44'50.8"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test
0 - 170	170	(Topsoil) SAND with silt: Grey, fine to medium. Roots and root fibres.	D	MD		No water table encountered.		
170 - 450	280	SAND with silt: Light grey, fine to medium.	D	L-MD				
450 - 2100	1650	Sandy GRAVEL: Brown, fine to coarse, sub-rounded to sub-angular. Fine to medium grained sand.	D	MD-D				
2100 - 2500	400	Gravelly SAND with silt: Light brown, fine to medium. Fine to medium, sub-rounded to sub-angular gravel.	D	MD				

				Target Depth	✓	2500
				Cave In		
				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.7



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** 12546218  
**Location:** 34°56'03.5"S 117°44'40.4"E

**Date Commenced**  
25/03/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 200	200	(Topsoil) SAND with silt: Grey, fine to medium. Roots and root fibres.	D	MD		No water table encountered.			
200 - 950	750	SAND with silt: Light grey, fine to medium.	D	MD					
950 - 2500	1550	Sandy GRAVEL: Brown, fine to coarse, sub-rounded to sub-angular. Fine to medium grained sand.	D	MD-D					

				Target Depth	✓	2500
				Cave In		
				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.8



**Excavation**



**Spoil**



**Job No:** 4212  
**Client:** GHD  
**Project:** Albany Motorsport Park Development

**Sheet** 16 **of** 16



# **Appendix C**

## Test Results



Client: GHD  
Project: Albany Motorsport Park Development  
Section: Test Pit 4

Client Number: 12546218  
Date of Test: 25/03/2021

## Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs ( Report 4212/1 )
------------	---------	----------------------	--

Sample No.	4212G9
------------	--------

Saturated Hydraulic Conductivity (cm/min)	0.0913
Saturated Hydraulic Conductivity (m/day)	1.31
Saturated Hydraulic Conductivity (m/sec)	1.52E-05

### Site Location



**Comments:** The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics Scope of Accreditation.

**Disclaimer:** Great Southern Geotechnics does not warrant data produced by use of this spreadsheet or any interpretation based on that data.

Distribution: Laboratory File / Vicki Davies - GHD  
Document ID: WS\_1547\_TalsmaHallam\_Rev2\_Mar2020

Name: M.Coffey  
Function: Quality Manager  
Date: 9/04/2021

Approved  
By:



Client: GHD  
Project: Albany Motorsport Park Development  
Section: Test Pit 5

Client Number: 12546218  
Date of Test: 25/03/2021

## Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs ( Report 4212/1 )
------------	---------	----------------------	--

Sample No.	4212G10
------------	---------

Saturated Hydraulic Conductivity (cm/min)	0.0342
Saturated Hydraulic Conductivity (m/day)	0.49
Saturated Hydraulic Conductivity (m/sec)	5.70E-06

### Site Location



**Comments:** The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics Scope of Accreditation.

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Distribution: Laboratory File / Vicki Davies - GHD  
Document ID: WS\_1547\_TalsmaHallam\_Rev2\_Mar2020

Name: M.Coffey  
Function: Quality Manager  
Date: 9/04/2021

Approved  
By:



Client: GHD  
Project: Albany Motorsport Park Development  
Section: Test Pit 6

Client Number: 12546218  
Date of Test: 25/03/2021

## Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs ( Report 4212/1 )
------------	---------	----------------------	--

Sample No.	4212G11
------------	---------

Saturated Hydraulic Conductivity (cm/min)	0.2282
Saturated Hydraulic Conductivity (m/day)	3.29
Saturated Hydraulic Conductivity (m/sec)	3.80E-05

### Site Location



**Comments:** The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics Scope of Accreditation.

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Distribution: Laboratory File / Vicki Davies - GHD  
Document ID: WS\_1547\_TalsmaHallam\_Rev2\_Mar2020

Name: M.Coffey  
Function: Quality Manager  
Date: 9/04/2021

Approved  
By:



Client: GHD  
Project: Albany Motorsport Park Development  
Section: Test Pit 7

Client Number: 12546218  
Date of Test: 25/03/2021

## Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs ( Report 4212/1 )
------------	---------	----------------------	--

Sample No.	4212G12
------------	---------

Saturated Hydraulic Conductivity (cm/min)	0.2282
Saturated Hydraulic Conductivity (m/day)	3.29
Saturated Hydraulic Conductivity (m/sec)	3.80E-05

### Site Location



**Comments:** The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics Scope of Accreditation.

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Distribution: Laboratory File / Vicki Davies - GHD  
Document ID: WS\_1547\_TalsmaHallam\_Rev2\_Mar2020

Name: M.Coffey  
Function: Quality Manager  
Date: 9/04/2021

Approved  
By:



Client: GHD  
Project: Albany Motorsport Park Development  
Section: Test Pit 8

Client Number: 12546218  
Date of Test: 25/03/2021

## Talsma-Hallam Permeameter Test Report

Layer Type	In Situ	Material Description	Refer to Test Pit Logs ( Report 4212/1 )
------------	---------	----------------------	--

Sample No.	4212G13
------------	---------

Saturated Hydraulic Conductivity (cm/min)	0.0285
Saturated Hydraulic Conductivity (m/day)	0.41
Saturated Hydraulic Conductivity (m/sec)	4.75E-06

### Site Location



**Comments:** The Talsma-Hallam Permeameter is not a method covered by Great Southern Geotechnics Scope of Accreditation.

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Distribution: Laboratory File / Vicki Davies - GHD  
Document ID: WS\_1547\_TalsmaHallam\_Rev2\_Mar2020

Name: M.Coffey  
Function: Quality Manager  
Date: 9/04/2021

Approved  
By:

## COLOURS

	BLACK - BROWN (bk)		BLUE (bl)		ORANGE (or)
	BROWN (br)		BLUE - GREEN (bl/gr)		RED (rd)
	GREY - BROWN (gy/br)		GREEN (gr)		RED - BROWN (rd/br)
	GREY (gy)		YELLOW (yl)		PINK (pk)
	BLUE - GREY (bl/gy)		YELLOW - BROWN (yl/br)		PURPLE (pr)

## MOISTURE CONDITION OF SOIL

TERM	DESCRIPTION
Dry	Cohesive soils; hard and friable or powdery, well dry of plastic limit. Granular soils; cohesionless and free-running.
Moist	Soil feels cool, darkened in colour. Cohesive soils can be moulded. Granular soils tend to cohere.
Wet	Soil feels cool, darkened in colour. Cohesive soils usually weakened and free water forms on hands when handling. Granular soils tend to cohere and free water forms on hands when handling.

## PARTICLE SHAPES

ANGULAR	SUB-ANGULAR	SUB-ROUNDED	ROUNDED
			

## PARTICLE SIZES

BOULDERS	COBBLES	COARSE GRAVEL	MEDIUM GRAVEL	FINE GRAVEL	COARSE SAND	MEDIUM SAND	FINE SAND	SILT	CLAY
>200mm	63-200mm	20-63mm	6-20mm	2.36-6mm	0.6-2.36mm	0.2-0.6mm	0.075-0.2mm	0.002-0.075mm	<0.002mm

## GRAIN SIZE

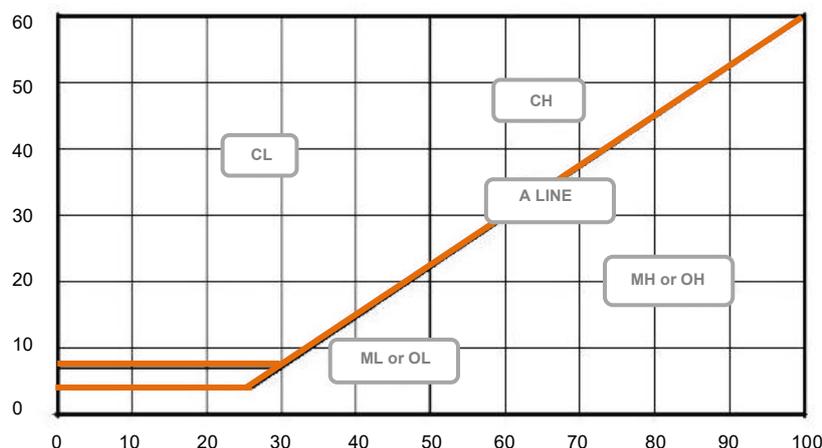
SOIL TYPE (ABBREV.)	CLAY (CL)	SILT (SI)	SAND (SA)			GRAVEL (GR)		COBBLES (CO)	
SIZE	< 2µm	2-75µm	Fine 0.075-0.2mm	Medium 0.2-0.6mm	Coarse 0.6-2.36mm	Fine 2.36-6mm	Medium 6-20mm	Coarse 20-63mm	63-200mm
SHAPE & TEXTURE	Shiny	Dull	← angular or sub angular or sub rounded or rounded →						
FIELD GUIDE	Not visible under 10x	Visible under 10x	Visible by eye	Visible at < 1m	Visible at < 3m	Visible at < 5m	Road gravel	Rail ballast	Beaching

## CLASSIFICATION CHART

FIELD IDENTIFICATION PROCEDURES (Excluding particles larger than 60mm and basing fractions on estimated mass)				GROUP SYMBOLS	TYPICAL NAMES	
<b>COARSE GRAINED SOILS</b> More than 50% of material less than 63 mm is larger than 0.075 mm	<b>GRAVELS</b> More than 50% of coarse fraction is larger than 2.36mm	<b>CLEAN GRAVELS</b> (Little or no fines)	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength	GW	Well graded gravels, gravel-sand mixtures, little or no fines	
			Predominantly one size or range of sizes with some intermediate sizes missing, not enough fines to bind coarse grains, no dry strength	GP	Poorly Graded gravels and gravel-sand mixtures, little or no fines, uniform gravels	
		<b>GRAVELS WITH FINES</b> (Appreciable amount of fines)	Dirty' materials with excess of non-plastic fines, zero to medium dry strength	GM	Silty gravels, gravel-sand-silt mixtures	
			'Dirty' materials with excess of plastic fines, medium to high dry strength	GC	Clayey gravels, gravel-sand-clay mixtures	
	<b>SANDS</b> More than 50% of coarse fraction is smaller than 2.36mm	<b>CLEAN SANDS</b> (Little or no fines)	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength	SW	Well graded sands, gravelly sands, little or no fines	
			Predominantly one size or range of sizes with some intermediate sizes missing, not enough fines to bind coarse grains, no dry strength	SP	Poorly graded sands and gravelly sands; little or no fines, uniform sands	
		<b>SANDS WITH FINES</b> (Appreciable amount of fines)	Dirty' materials with excess of non-plastic fines, zero to medium dry strength	SM	Silty sands, sand-silt mixtures	
			'Dirty' materials with excess of plastic fines, medium to high dry strength	SC	Clayey sands, sand-clay mixtures	
<b>FINE GRAINED SOILS</b> More than 50% of material less than 63 mm is smaller than 0.075 mm	IDENTIFICATION PROCEDURES ON FRACTIONS <0.2mm					
	<b>SILTS AND CLAYS</b> Liquid limit less than 50	DRY STRENGTH	DILATANCY	TOUGHNESS		
		None to low	Quick to slow	None	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with low plasticity. Silts of low to medium Liquid Limit.
		Medium to high	None to very slow	Medium	CL, CI	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays.
	<b>SILTS AND CLAYS</b> Liquid limit greater than 50	Low to medium	Slow	Low	OL	Organic silts and organic silt-clays of low to medium plasticity.
		Low to medium	Slow to none	Low to medium	MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, silts of high Liquid Limit.
		High to very high	None	High	CH	Inorganic clays of high plasticity.
	<b>SILTS AND CLAYS</b> Liquid limit greater than 50	Medium to high	None to very slow	Low to medium	OH	Organic clays of high plasticity
		HIGHLY ORGANIC SOILS Readily identified by colour, odour, spongy feel and frequently by fibrous texture			Pt	Peat and other highly organic soils

## PLASTICITY CHART

For laboratory classification of fine grained soils



## PLASTICITY

DESCRIPTIVE TERM	OF LOW PLASTICITY	OF MEDIUM PLASTICITY	OF HIGH PLASTICITY
Range Of Liquid Limit (%)	≤ 35	> 35 ≤ 50	> 50

## DESCRIPTION OF ORGANIC OR ARTIFICIAL MATERIALS

PREFERRED TERMS	SECONDARY DESCRIPTION
Organic Matter	Fibrous Peat/ Charcoal/ Wood Fragments/ Roots (greater than approximately 2mm diameter)/ Root Fibres (less than approximately 2mm diameter)
Waste Fill	Domestic Refuse/ Oil/ Bitumen/ Brickbats/ Concrete Rubble/ Fibrous Plaster/ Wood Pieces/ Wood Shavings/ Sawdust/ Iron Filings/ Drums/ Steel Bars/ Steel Scrap/ Bottles/ Broken Glass/ Leather

## CONSISTENCY – Cohesive soils

TERM	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD
Symbol	VS	S	F	St	VSt	H
Undrained Shear Strength (kPa)	< 12	12 – 25	25 – 50	50 – 100	100 – 200	> 200
SPT (N) Blowcount	0 – 2	2 – 4	4 – 8	8 – 15	15 – 30	> 30
Field Guide	Exudes between the fingers when squeezed	Can be moulded by light finger pressure	Can be moulded by strong finger pressure	Cannot be moulded by fingers. Can be indented by thumb nail	Can be indented by thumb nail	Can be indented with difficulty with thumb nail

## CONSISTENCY – Non-cohesive soils

TERM	VERY LOOSE	LOOSE	MEDIUM DENSE	DENSE	VERY DENSE	COMPACT
Symbol	VL	L	MD	D	VD	CO
SPT (N) Blowcount	0 – 4	4 – 10	10 – 30	30 – 50	50 – 100	> 50/150 mm
Density Index (%)	< 15	15 – 35	35 – 65	65 – 85	85 – 95	> 95
Field Guide	Ravels	Shovels easily	Shovelling very difficult	Pick required	Pick difficult	Cannot be picked

## MINOR COMPONENTS

TERM	TRACE	WITH
% Minor Component	Coarse grained soils: < 5% Fine grained soils: <15%	Coarse grained soils: 5 – 12% Fine grained soils: 15 – 30%
Field Guide	Presence just detectable by feel or eye, but soil properties little or no different to general properties of primary components	Presence easily detectable by feel or eye, soil properties little different to general properties of primary component

## GEOLOGICAL ORIGIN

	TYPE	DETAILS
TRANSPORTED SOILS	Aeolian Soils	Deposited by wind
	Alluvial Soils	Deposited by streams and rivers
	Colluvial Soils	Deposited on slopes
	Lacustrine Soils	Deposited by lakes
	Marine Soils	Deposited in ocean, bays, beaches and estuaries
FILL MATERIALS	Soil Fill	Describe soil type, UCS symbol and add 'FILL'
	Rock Fill	Rock type, degree of weathering, and word 'FILL'.
	Domestic Fill	Percent soil or rock, whether pretrucible or not.
	Industrial Fill	Percent soil, whether contaminated, particle size & type of waste product, ie brick, concrete, metal

## STRENGTH OF ROCK MATERIAL

TERM	SYMBOL	IS (50)	(MPA)	FIELD GUIDE TO STRENGTH
Extremely Low	EL	≤0.03		Easily remoulded by hand to a material with soil properties.
Very Low	VL	>0.03	≤0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxle sample by hand. Pieces up to 3 cm thick can be broken by finger pressure.
Low	L	>0.1	≤0.3	Easily scored with a knife; indentations 1 mm to 3 mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150 mm long by 50 mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.
Medium	M	>0.3	≤1.0	Readily scored with a knife; a piece of core 150 mm long by 50 mm diameter can be broken by hand with difficulty.
High	H	>1	≤3	A piece of core 150 mm long by 50 mm diameter cannot be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.
Very High	VH	>3	≤10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.
Extremely High	EH	>10		Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.

## ROCK MATERIAL WEATHERING CLASSIFICATION

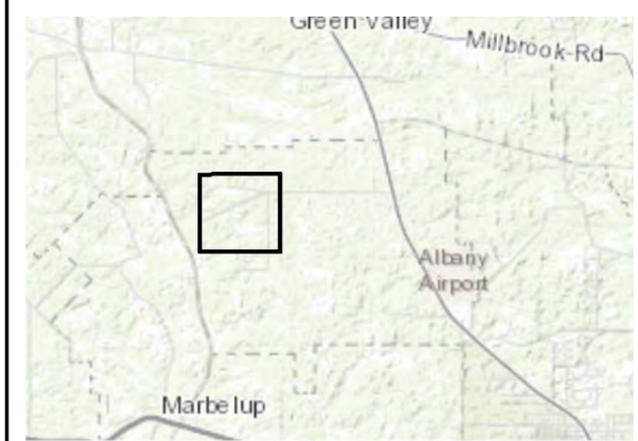
TERM	SYMBOL	DEFINITION
Residual Soil	RS	Soil developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported
Extremely Weathered Rock	XW	Rock is weathered to such an extent that it has 'soil' properties, i.e. it either disintegrates or can be remoulded, in water.
Distinctly Weathered Rock	DW	Rock strength usually changed by weathering. Rock may be highly discoloured, usually be iron staining. Porosity may be increased by leaching or may be decreased due to deposition of weathering products in pores.
Slightly Weathered Rock	SW	Rock is slightly discoloured but shows little or no change of strength from fresh rock.
Fresh Rock	FR	Rock shows no sign of decomposition or staining.

# Appendix C

**Bio Diverse Solutions monitoring**



Unit 5A, 209 Chester Pass Rd  
Albany, WA 6330  
Australia  
Tel: 08 9842 1575  
Fax: 08 9842 1575



Overview Map Scale 1:100,000

**Legend**

- Subject Site
- Cadastre
- 5m Contours
- Deep Bore
- ▲ Shallow Bore
- Creek Sample
- 50m Buffer



Scale  
1:7,882 @ A3  
GDA MGA 94 Zone 50

**Data Sources**  
Aerial Imagery: SLIP Virtual Mosaic WMS Service, Landgate 2016  
Cadastre and Contours: Landgate 2016  
Overview Map: World Topographic map service, ESRI 2012

**CLIENT**  
City of Albany  
Lot 5780 Down Road  
Drome, WA 6330

**Monitoring Plan**

STATUS	FILE	DATE
FINAL	MSC0137	28/02/2019



29 Hercules Cres  
Albany WA 6330  
98421575  
kath@biodiversesolutions.com.au  
ABN 48 138 824 272

21<sup>st</sup> March 2018

Great Southern Motorplex  
PO Box 1905  
Albany, WA 6330

**Lot 5780 Down Road, Drome WA 6330**  
**Water Quality Monitoring**

Dear Great Southern Motorplex Group,

On the 27<sup>th</sup> February 2018 the shallow monitoring bores were installed at Lot 5780 Down Road, Drome. A total of 12 sampling bores were installed to a depth of 2m as per the DoW Approved Monitoring Plan.

A copy of details relating to this supplied:

- Field test bore logs;
- MPL Laboratory results; and
- BDS Field and Laboratory summary sheets.

Preliminary analysis of the land from the site soil testing indicates that the majority of the land will be sand over gravels/laterite rock. Low lying areas adjacent to the creek will have silty sands with coffee rock and will generally be waterlogged. Water table was only encountered at the lower lying bores of SB06, SB07 and SB09 which I would expect in summer conditions this to prevail. The creek was running albeit at a very low level which indicates there is groundwater movement into the creek system year round.

I am expecting given the soil results, that there will be limited groundwater in test pits SB11, SB03, SB02, SB05, and SB10 through the year. Marginal groundwater will most likely appear in SB04, SB08 and SB12. Refer to finalised Test Pit locations mapping.

Due to limited funds available the deep water bore is yet to be done but recommend this is done as soon as the full quote is approved.

Field analysis of the WQ at the creek indicates the creek is gaining acidity through the catchment. A higher pH in the upper reaches with a pH 6.34 at CS02 and lower (more acidic) pH in the lower catchment CS01 of 4.46, which is to be expected when cattle are entering the system to feed, water and defecating (generally disturbing the upper catchment).

Laboratory testing results are partially available, we are still waiting Salinity, hardness/alkalinity. Biological analytes are not available this round. Full analysis has not been undertaken of the laboratory results as yet.

This information is provided as preliminary, if you have any queries regarding this matter, please feel free to contact me via email on [kath@biodiversesolutions.com.au](mailto:kath@biodiversesolutions.com.au) or phone/fax on 9842 1575.

Kind regards,

Kathryn Kinnear  
Director,  
Bio Diverse Solutions

## Soil Profile Sampling



**Location:** Lot 5780 Down Road

**Date tested:** 27/02/2018

**Sampled by:** Kathryn Kinnear

**Weather:** Windy, cool 21 degrees Overcast

<u>Location</u>	<u>Site description</u>	<u>Depth of profile (mm)</u>	<u>Soil Description</u>
SB1	South west corner Open Paddock	0-150 150-300 300-500  500-1200 1200-1500  1500-2000	Dark grey sandy top soil, veg matter. Grey silty sand. Orange, light brown sandy gravel pebbles 10-30mm. Laterite rock . Light brown pebbles 10-30mm, orange sandy silty gravel. Light brown sandy clay, slightly moist. No WT.
SB02	Paddock near creek west side Jarrah/Cas/Marri Forrest adjacent	0-50 50-200 200-800 800-1200 1200-1500 1500-2000  2000-2500	Dark grey sandy top soil, veg matter. Grey sandy silt. Light grey sandy silt, slightly moist. Cream sandy silt, slightly moist Laterite rock. Moist light brown orange sandy silt gravel, pebbles 10-30mm, minor clay. Light grey silty sand. No WT.
SB03	Open paddock North in minor Drainage swale	0-50 50-500 500-1000 1000-1200 1200-1600 1600-1800 1800-2000	Light brown slightly moist silty sand top soil, veg matter. Light brown silty gravel, pebbles 5-10mm. Brown silty gravel pebbles 20-30mm. Dark brown gravelly silt pebbles 20-30mm. Grey silty sand. Light grey moist silty sand. Light brown/orange silty sand, gravel pebbles 10-30mm. No WT.
SB04	Paddock near Creek in Depression area.	0-50 50-200 700-900 900-1300  1300-1500 1500-1800 1800-2000	Dark brown peaty organic matter. Dark grey silty sand slightly moist. Light grey silty sand moist. Laterite rock, moist dark brown gravelly silt (coffee rock) mottled orange. Light brown silty clay wet. Light grey moist clay. White clay not wet. No WT.
SB05	North paddock Area	0-50 50-200 200-700 700-900 900-1500  1500-1800 1800-1900 1900-2000	Slightly moist dark brown peaty sandy silt top soil, veg matter. Dry dark grey silty sand. Dry light grey silty sand. Dry gravelly silty sand orange pebbles. Dry cream quartz gravelly silty sand pebbles 30-50mm. Pink/orange silty sand gravel, cemented compacted gavel pebbles 10-30mm. Moist dark clayey sand. Dry compacted silty gravel orange/pink. No WT.

<u>Location</u>	<u>Site description</u>	<u>Depth of profile (mm)</u>	<u>Soil Description</u>
SB06	Near creek North side In reed beds	0-100 100-400 400-700 700-1800 1800-2000	Dark brown peaty organic matter moist. Dark grey silty sand moist. Grey silty sand moist. Light grey silty sand wet (smell). Wet brown silty sand (smell) WT 870mm BGL
SB07	Near creek Crossing North side	0-200 200-400 400-600 600-1800 1800-2000	Dark brown/black peaty moist. Black/dark grey peaty sand moist. Dark grey silty sand moist. Light brown silty sand smell. Cream wet silty sand smell. WT 640mm BGL
SB08	Mid creek near dam	0-50 50-200 200-500 500-900 900-1200 1200-1400 1400-1800 1800-2000	Slightly moist dark brown peaty silt, veg matter. Dark brown sandy peaty silt moist. Dark grey silty sand moist. Grey slightly moist silty sand. Dark brown cemented silt, coffee rock. Dark grey moist to wet silty sand. Grey silty sand wet. Dark brown silt minor pebbles 10mm. No WT.
SB09	South side of creek	0-50 50-200 200-600 600-700 700-1100 1100-1300 1300-2000	Dark brown peaty organic matter moist. Dark grey silty sand. Grey silty sand. Light brown gravelly silt. Laterite rock. Wet silt pebbles 30-40mm. White moist clayey silt. WT 660mm BGL
SB010	South boundary east of bush line in paddock	0-50 50-300  300-500  500-1200  1200-2000	Brown silty sand organic matter dry. Brown silty sand gravels 40-50mm, boulders 200mm Laterite, dry. Brown/orange silty sandy gravel cemented Laterite. Light brown/orange cemented silt. White mottles sandstone dry. Light brown/orange cemented silt. White mottles sandstone dry. No WT.
SB011	Mid paddock, top of hill eastern side of site	0-50 50-300 300-400 400-1200 1200-1800 1800-2000	Dark brown silty sand dry. Grey silty sand dry. Light brown silty gravel pebble 30-50mm. Light brown cemented silt Laterite. Light brown, mottles pink * white clay dry. Orange mottled red dry clay. No WT.
SB012		0-400 400-1000 1000-1500 1500-1800  1800-2000	Grey sandy silt organic matter dry. Light grey silty sand. Cream silty sand slightly moist. Dark brown sandy silt, slightly moist gravel minor pebbles. Light brown silty clayey slightly moist boulder Laterite gravels 40mm. No WT.

### Groundwater Monitoring Data Record Sheet



Date 30/05/2018 Name of recorder Kathryn Kinnear / Bianca Theyer  
 Location Down Road Project No. MSC0137

Test ID	Time	BCH	WD	WD-BCH	CW	pH	EC	DO	Temp	TDS	Additional Information
SB09	9:15	932	1500	568	N/A	6.28	0.25	4.84	18.13	0.161	Slight smell
SB10	8:30				N/A						Dry
SB11	8:35				N/A						Dry
SB12	8:50				N/A						Dry
SB08	9:45	930	2480	1550	N/A	4.56	0.217	4.68	18.33	0.14	Sediment, tannins and smell
SB06	10:00	955	1653	698	N/A	4.78	0.321	2.24	17.48	0.208	Sediment, tannins and smell
SB07	10:25	965	1500	535	N/A	4.77	0.28	5.34	19.89	0.181	Smell, coloured
SB05	9:22				N/A						Dry
SB04	10:52	920	1830	910	N/A	5.9	0.242	4.79	17.37	0.157	Slight colouration and smell
CS02	10:55				40cm	5.78	1.05	4.66	14.22	0.675	20cm water depth, clear some sediments when disturbed
SB01	10:10				N/A						Dry
SB02	10:20				N/A						Dry
CS01	11:20				1.5m	6.09	0.923	9.54	11.93	0.59	30cm Clear, slight tannin, flowing

BCH = Bore Casing Height WD = Water Depth below casing WD-BCH = Groundwater level BGL  
 CW = Creek width

Notes:  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_





Envirolab Services (WA) Pty Ltd trading as MPL Laboratories

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ph 08 9317 2505 fax 08 9317 4163

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## CERTIFICATE OF ANALYSIS 207409

### Client Details

**Client** Biodiverse Solutions  
**Attention** Kathryn Kinnear  
**Address**

### Sample Details

**Your Reference** Biodiverse Solutions  
**Number of Samples** 5 Water  
**Date samples received** 01/03/2018  
**Date completed instructions received** 01/03/2018

### Analysis Details

Please refer to the following pages for results, methodology summary and quality control data.

Samples were analysed as received from the client. Results relate specifically to the samples as received.

Results are reported on a dry weight basis for solids and on an as received basis for other matrices.

**Please refer to the last page of this report for any comments relating to the results.**

### Report Details

**Date results requested by** 09/03/2018

**Date of Issue** 12/03/2018

NATA Accreditation Number 2901. This document shall not be reproduced except in full.

Accredited for compliance with ISO/IEC 17025 - Testing. **Tests not covered by NATA are denoted with \***

#### Results Approved By

Joshua Lim, Operations Manager  
Michael Kubiak, Organics Supervisor

#### Authorised By

Todd Lee, Laboratory Manager

MPL Reference 207409  
Revision No R00



Client Reference: Biodiverse Solutions

Nutrients in Water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date prepared	-		08/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
Date analysed	-		08/03/2018	08/03/2018	08/03/2018	08/03/2018	02/03/2018
Total Nitrogen	mg/L	0.1	1.0	3.0	1.1	0.2	0.3
Nitrate as N	mg/L	0.005	0.26	0.007	<0.005	0.024	0.27
Nitrite as N	mg/L	0.005	<0.005	<0.005	<0.005	<0.005	<0.005
Ammonia as N	mg/L	0.005	<0.005	<0.005	0.11	0.70	0.22
Total Phosphorus	mg/L	0.05	<0.05	0.26	<0.05	1.3	0.65
Phosphate as P	mg/L	0.005	<0.005	<0.005	<0.005	1.1	0.52

Client Reference: Biodiverse Solutions

Dissolved Metals in Water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date prepared	-		07/03/2018	07/03/2018	07/03/2018	07/03/2018	07/03/2018
Date analysed	-		07/03/2018	07/03/2018	07/03/2018	07/03/2018	07/03/2018
Aluminium-Dissolved	mg/L	0.01	0.06	0.46	1.2	1.8	0.86
Arsenic-Dissolved	mg/L	0.001	<0.001	0.013	0.006	<0.001	<0.001
Cadmium-Dissolved	mg/L	0.0001	<0.0001	<0.0001	<0.0001	<0.0001	0.0002
Chromium-Dissolved	mg/L	0.001	<0.001	0.002	0.003	0.002	0.002
Copper-Dissolved	mg/L	0.001	<0.001	<0.001	0.002	<0.001	0.002
Iron-Dissolved	mg/L	0.01	0.86	40	2.8	0.90	1.1
Mercury-Dissolved	mg/L	0.00005	<0.00005	<0.00005	<0.00005	<0.00005	<0.00005
Manganese-Dissolved	mg/L	0.005	<0.005	<0.005	0.007	0.01	0.009
Nickel-Dissolved	mg/L	0.001	<0.001	<0.001	<0.001	0.003	<0.001
Lead-Dissolved	mg/L	0.001	<0.001	<0.001	<0.001	0.006	0.001
Zinc-Dissolved	mg/L	0.001	0.008	0.002	0.069	0.097	0.065

Client Reference: Biodiverse Solutions

VTRH(C6-C10)/MBTEXN in water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date analysed	-		02/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
TRH C <sub>6</sub> - C <sub>9</sub>	µg/L	10	<10	<10	<10	<10	<10
TRH C <sub>6</sub> - C <sub>10</sub>	µg/L	10	<10	<10	<10	<10	<10
TRH C <sub>6</sub> -C <sub>10</sub> less BTEX (F1)	µg/L	10	<10	<10	<10	<10	<10
MTBE	µg/L	1	<1	<1	<1	<1	<1
Benzene	µg/L	1	<1	<1	<1	<1	<1
Toluene	µg/L	1	<1	<1	<1	<1	<1
Ethylbenzene	µg/L	1	<1	<1	<1	<1	<1
m+p-xylene	µg/L	2	<2	<2	<2	<2	<2
o-xylene	µg/L	1	<1	<1	<1	<1	<1
Naphthalene	µg/L	1	<1	<1	<1	<1	<1
Surrogate Dibromofluoromethane	%		111	110	114	106	112
Surrogate toluene-d8	%		107	103	105	99	105
Surrogate 4-BFB	%		98	97	96	97	96

Client Reference: Biodiverse Solutions

svTRH(C10-C40) in water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date extracted	-		02/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
Date analysed	-		06/03/2018	06/03/2018	06/03/2018	06/03/2018	06/03/2018
TRH C <sub>10</sub> - C <sub>14</sub>	µg/L	50	<50	<50	<50	<50	<50
TRH C <sub>15</sub> - C <sub>28</sub>	µg/L	100	<100	<100	<100	<100	<100
TRH C <sub>29</sub> - C <sub>36</sub>	µg/L	100	<100	<100	<100	110	330
TRH >C <sub>10</sub> - C <sub>16</sub>	µg/L	50	<50	<50	<50	<50	<50
TRH >C <sub>10</sub> -C <sub>16</sub> less N (F2)	µg/L	50	<50	<50	<50	<50	<50
TRH >C <sub>16</sub> - C <sub>34</sub>	µg/L	100	<100	<100	<100	140	280
TRH >C <sub>34</sub> - C <sub>40</sub>	µg/L	100	<100	<100	<100	<100	220
Surrogate o-Terphenyl	%		84	85	94	37	19

Client Reference: Biodiverse Solutions

PAHs in Water							
Our Reference			207409-1	207409-2	207409-3	207409-4	207409-5
Your Reference	UNITS	PQL	CS01	CS02	SB09	SB06	SB07
Date Sampled			27/02/2018	27/02/2018	27/02/2018	27/02/2018	27/02/2018
Type of sample			Surface Water	Surface Water	Groundwater	Groundwater	Groundwater
Date extracted	-		02/03/2018	02/03/2018	02/03/2018	02/03/2018	02/03/2018
Date analysed	-		07/03/2018	07/03/2018	07/03/2018	07/03/2018	07/03/2018
Naphthalene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Acenaphthylene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Acenaphthene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Fluorene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Phenanthrene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Anthracene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Fluoranthene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Pyrene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(a)anthracene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Chrysene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(b,j+k)fluoranthene	µg/L	0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Benzo(a)pyrene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Indeno(1,2,3-c,d)pyrene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Dibenzo(a,h)anthracene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(g,h,i)perylene	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(a)pyrene TEQ	µg/L	0.5	<0.5	<0.5	<0.5	<0.5	<0.5
Total +ve PAH's	µg/L	0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Surrogate p-Terphenyl-D <sub>14</sub>	%		78	76	88	24	14

**Client Reference: Biodiverse Solutions**

<b>Method ID</b>	<b>Methodology Summary</b>
INORG-055	Nitrite - determined colourimetrically. Soils are analysed from a water extract.
INORG-055	Nitrate - determined colourimetrically. Soils are analysed from a water extract.
INORG-055	Total Nitrogen by colourimetric analysis based on APHA 4500-P J, 4500-NO3 F.
INORG-057	Ammonia by colourimetric analysis based on APHA latest edition 4500-NH3 F.
INORG-060	Phosphate- determined colourimetrically. Soils are analysed from a water extract.
METALS-020	Metals in soil and water by ICP-OES.
METALS-021	Determination of Mercury by Cold Vapour AAS.
METALS-022	Determination of various metals by ICP-MS.
ORG-003	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-FID. F2 = (>C10-C16)-Naphthalene as per NEPM B1 Guideline on Investigation Levels for Soil and Groundwater (HSLs Tables 1A (3, 4)). Note Naphthalene is determined from the VOC analysis.
ORG-004	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS.
ORG-012	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS.
ORG-012	Soil samples are extracted with Dichloromethane/Acetone and waters with Dichloromethane and analysed by GC-MS. Benzo(a)pyrene TEQ as per NEPM draft B1 Guideline on Investigation Levels for Soil and Groundwater.
ORG-016	Soil samples are extracted with methanol and spiked into water prior to analysing by purge and trap GC-MS. Water samples are analysed directly by purge and trap GC-MS. F1 = (C6-C10)-BTEX as per NEPM B1 Guideline on Investigation Levels for Soil and Groundwater.

Client Reference: Biodiverse Solutions

Test Description	Units	QUALITY CONTROL Nutrients in Water			#	Duplicate			Spike Recovery %	
		PQL	Method	Blank		Base	Dup.	RPD	LCS-1	[NT]
Date prepared	-			02/03/2018					02/03/2018	
Date analysed	-			02/03/2018					02/03/2018	
Total Nitrogen	mg/L	0.1	INORG-055	<0.1					96	
Nitrate as N	mg/L	0.005	INORG-055	<0.005					116	
Nitrite as N	mg/L	0.005	INORG-055	<0.005					117	
Ammonia as N	mg/L	0.005	INORG-057	<0.005					100	
Total Phosphorus	mg/L	0.05	METALS-020	<0.05					103	
Phosphate as P	mg/L	0.005	INORG-060	<0.005					92	

Client Reference: Biodiverse Solutions

QUALITY CONTROL: Dissolved Metals in Water					Duplicate			Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	207409-2
Date prepared	-			07/03/2018	1	07/03/2018	07/03/2018		07/03/2018	07/03/2018
Date analysed	-			07/03/2018	1	07/03/2018	07/03/2018		07/03/2018	07/03/2018
Aluminium-Dissolved	mg/L	0.01	METALS-022	<0.01	1	0.06	0.06	0	109	77
Arsenic-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	103	108
Cadmium-Dissolved	mg/L	0.0001	METALS-022	<0.0001	1	<0.0001	<0.0001	0	104	109
Chromium-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	105	104
Copper-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	103	99
Iron-Dissolved	mg/L	0.01	METALS-022	<0.01	1	0.86	0.87	1	105	#
Mercury-Dissolved	mg/L	0.00005	METALS-021	<0.00005	1	<0.00005	<0.00005	0	102	104
Manganese-Dissolved	mg/L	0.005	METALS-022	<0.005	1	<0.005	<0.005	0	108	107
Nickel-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	103	98
Lead-Dissolved	mg/L	0.001	METALS-022	<0.001	1	<0.001	<0.001	0	101	101
Zinc-Dissolved	mg/L	0.001	METALS-022	<0.001	1	0.008	0.008	0	103	104

Client Reference: Biodiverse Solutions

QUALITY CONTROL: vTRH(C6-C10)/MBTEXN in water					Duplicate			Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	[NT]
Date analysed	-			02/03/2018					02/03/2018	
TRH C <sub>6</sub> - C <sub>9</sub>	µg/L	10	ORG-016	<10					95	
TRH C <sub>6</sub> - C <sub>10</sub>	µg/L	10	ORG-016	<10					95	
MTBE	µg/L	1	ORG-016	<1						
Benzene	µg/L	1	ORG-016	<1					110	
Toluene	µg/L	1	ORG-016	<1					103	
Ethylbenzene	µg/L	1	ORG-016	<1					89	
m+p-xylene	µg/L	2	ORG-016	<2					86	
o-xylene	µg/L	1	ORG-016	<1					87	
Naphthalene	µg/L	1	ORG-016	<1						
Surrogate Dibromofluoromethane	%		ORG-016	109					106	
Surrogate toluene-d8	%		ORG-016	107					105	
Surrogate 4-BFB	%		ORG-016	99					105	

Client Reference: Biodiverse Solutions

QUALITY CONTROL: svTRH(C10-C40) in water				Duplicate			Spike Recovery %			
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	[NT]
Date extracted	-			02/03/2018	2	02/03/2018	02/03/2018		02/03/2018	
Date analysed	-			06/03/2018	2	06/03/2018	06/03/2018		06/03/2018	
TRH C <sub>10</sub> - C <sub>14</sub>	µg/L	50	ORG-003	<50	2	<50	<50	0	73	
TRH C <sub>15</sub> - C <sub>28</sub>	µg/L	100	ORG-003	<100	2	<100	<100	0	88	
TRH C <sub>29</sub> - C <sub>36</sub>	µg/L	100	ORG-003	<100	2	<100	<100	0	81	
TRH >C <sub>10</sub> - C <sub>16</sub>	µg/L	50	ORG-003	<50	2	<50	<50	0	78	
TRH >C <sub>16</sub> - C <sub>34</sub>	µg/L	100	ORG-003	<100	2	<100	<100	0	88	
TRH >C <sub>34</sub> - C <sub>40</sub>	µg/L	100	ORG-003	<100	2	<100	<100	0	75	
Surrogate α-Terphenyl	%		ORG-003	97	2	85	101	17	80	

Client Reference: Biodiverse Solutions

QUALITY CONTROL: PAHs in Water					Duplicate			Spike Recovery %		
Test Description	Units	PQL	Method	Blank	#	Base	Dup.	RPD	LCS-1	[NT]
Date extracted	-			02/03/2018	2	02/03/2018	02/03/2018		02/03/2018	
Date analysed	-			07/03/2018	2	07/03/2018	07/03/2018		07/03/2018	
Naphthalene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	94	
Acenaphthylene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Acenaphthene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Fluorene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	108	
Phenanthrene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	115	
Anthracene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Fluoranthene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	114	
Pyrene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	112	
Benzo(a)anthracene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Chrysene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	100	
Benzo(b,j+k)fluoranthene	µg/L	0.2	ORG-012	<0.2	2	<0.2	<0.2	0		
Benzo(a)pyrene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0	72	
Indeno(1,2,3-c,d)pyrene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Dibenzo(a,h)anthracene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Benzo(g,h,i)perylene	µg/L	0.1	ORG-012	<0.1	2	<0.1	<0.1	0		
Surrogate p-Terphenyl-D <sub>14</sub>	%		ORG-012	91	2	76	77	1	74	

**Result Definitions**

<b>NT</b>	Not tested
<b>NA</b>	Test not required
<b>INS</b>	Insufficient sample for this test
<b>PQL</b>	Practical Quantitation Limit
<b>&lt;</b>	Less than
<b>&gt;</b>	Greater than
<b>RPD</b>	Relative Percent Difference
<b>LCS</b>	Laboratory Control Sample
<b>NS</b>	Not specified
<b>NEPM</b>	National Environmental Protection Measure
<b>NR</b>	Not Reported

**Quality Control Definitions**

<b>Blank</b>	This is the component of the analytical signal which is not derived from the sample but from reagents, glassware etc, can be determined by processing solvents and reagents in exactly the same manner as for samples.
<b>Duplicate</b>	This is the complete duplicate analysis of a sample from the process batch. If possible, the sample selected should be one where the analyte concentration is easily measurable.
<b>Matrix Spike</b>	A portion of the sample is spiked with a known concentration of target analyte. The purpose of the matrix spike is to monitor the performance of the analytical method used and to determine whether matrix interferences exist.
<b>LCS (Laboratory Control Sample)</b>	This comprises either a standard reference material or a control matrix (such as a blank sand or water) fortified with analytes representative of the analyte class. It is simply a check sample.
<b>Surrogate Spike</b>	Surrogates are known additions to each sample, blank, matrix spike and LCS in a batch, of compounds which are similar to the analyte of interest, however are not expected to be found in real samples.

Australian Drinking Water Guidelines recommend that Thermotolerant Coliform, Faecal Enterococci, & E.Coli levels are less than 1cfu/100mL. The recommended maximums are taken from "Australian Drinking Water Guidelines", published by NHMRC & ARMC 2011.

## Laboratory Acceptance Criteria

Duplicate sample and matrix spike recoveries may not be reported on smaller jobs, however, were analysed at a frequency to meet or exceed NEPM requirements. All samples are tested in batches of 20. The duplicate sample RPD and matrix spike recoveries for the batch were within the laboratory acceptance criteria.

Filters, swabs, wipes, tubes and badges will not have duplicate data as the whole sample is generally extracted during sample extraction.

Spikes for Physical and Aggregate Tests are not applicable.

For VOCs in water samples, three vials are required for duplicate or spike analysis.

Duplicates: <5xPQL - any RPD is acceptable; >5xPQL - 0-50% RPD is acceptable.

Matrix Spikes, LCS and Surrogate recoveries: Generally 70-130% for inorganics/metals; 60-140% for organics (+/-50% surrogates) and 10-140% for labile SVOCs (including labile surrogates), ultra trace organics and speciated phenols is acceptable.

In circumstances where no duplicate and/or sample spike has been reported at 1 in 10 and/or 1 in 20 samples respectively, the sample volume submitted was insufficient in order to satisfy laboratory QA/QC protocols.

When samples are received where certain analytes are outside of recommended technical holding times (THTs), the analysis has proceeded. Where analytes are on the verge of breaching THTs, every effort will be made to analyse within the THT or as soon as practicable.

Where sampling dates are not provided, Envirolab are not in a position to comment on the validity of the analysis where recommended technical holding times may have been breached.

Measurement Uncertainty estimates are available for most tests upon request.

**Report Comments**

#4,5 - PAH: Surrogate recovery was low due to sample emulsifying during extraction

# Percent recovery not available due to the analyte signal being much greater than the spike amount. An acceptable recovery was achieved for the LCS.

#4,5 for Nox PQL raised due to sample matrix. Very dark samples

**Groundwater Monitoring Data Record Sheet**



Date 4/09/2018 Name of recorder Bianca Theyer / Chiquita Cramer

Location Down Road Project No. MSC0137

Test ID	Time	BCH (cm)	WD (cm)	WD-BCH (cm)	pH	EC (mg/cm)	DO (mg/L)	Temp (C°)	TDS	Additional Information
SB9	9:35	92.7	136.8	44.1	5.86	0.389		17.2	0.253	Lightly coloured brown
SB12	10:28	85	189	104	7.52	0.077		16.55	0.05	Lots of sediment, lightly coloured brown
SB8	10:48	95	113	18	4.41	1.2	2.57	15.86	0.768	Moderate amount of sediment, brown in colour
SB6	11:17	93	93	0	4.16	1.07	8.95	14.23	0.686	Moderate amount of sediment, brown in colour
SB7	11:35	91	135	44	4.5	0.211		15.55	0.137	Moderate to high amount of sediment, brown in colour
CS1	12:02	N/A	10	N/A	5.68	0.885	3.93	14.91	0.566	Clear water, creek flowing
SB3	12:29	92	213	121	6.09	0.963	2.07	16.73	0.616	Lightly coloured brown
SB4	12:35	90.6	121	30.4	5.38	0.328	1.93	16.12	0.213	Lightly coloured brown
CS2	12:48	N/A	20	N/A	6.09	0.659	7.83	12.35	0.422	clear water, creek flowing

*BCH = Bore Casing Height WD = Water Depth below casing WD-BCH = Groundwater level BGL*

CW = Creek width

Notes:

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# Appendix D

**Conceptual hydrogeological model**

## A-4 Conceptual hydrogeological model

A Conceptual Site Model was completed to assess the connectivity between shallow and deeper hydrogeological features of the Site and surrounds, and to identify key pathways for transport of potential contaminants in surface and groundwater, and potential receptors based on site

### A-4-1 Sources of information

- Local shallow soil setting from Motorplex Development, Down Road Surface and Groundwater Monitoring 2018 Summary Report (Bio Diverse Solutions 2018)
- Regional hydrogeological setting from Albany hinterland prospective groundwater resources map (Ryan, Yesertener, Maughan, & Thornton, 2017)
- Shallow soil profile descriptions
- Deep groundwater bore

### A-4-2 Local shallow hydrogeology

The typical local surficial geology is presented in Plate 3, and shows the following features:

- A thin shallow sandy/silty layer up to 1 meter thick overlies the Pallinup formation in areas leading to the creek, while on the upper-slopes lateritic gravels/cobbles predominate.
- Underlying the sandy/silty layer, the Pallinup formation comprises silty clays which appears to extend to 25 meters below the ground level.
- Although not tested, the permeability of the upper sandy/silt is likely higher than the underlying Pallinup Formation (silty clays) which may result in temporary perching of shallow groundwater in the sandy/silt (particularly during winter rainfall).
- Shallow groundwater levels derived from the monitoring of the shallow bores indicates that the levels appear to vary seasonally up to 1 meter.
- Shallow groundwater flow within the sandy/silty layer (and upper parts of the Pallinup Formation) are inferred as towards the creek line where groundwater is inferred to discharge.

### A-4-3 “Deeper” hydrogeology

The deeper hydrogeology setting is presented on the cross section and shows the following features:

- The site (shallow hydrogeology) is underlain by approximately 25 metres of the Pallinup formation, deemed to comprise silt, sand and clay (Ryan *et al.* 2017). The Pallinup aquifer is inferred to contain minor water resources and exhibits a low permeability.
- The Pallinup Formation is underlain by the Werillup Aquitard described as comprising clay, silt and sand and which is deemed to hydraulically separate the overlying Pallinup Formation with underlying units (Ryan *et al.*, 2017). The drilling logs indicates that the thickness of the Werillup aquitard is 31 meters and comprises predominantly clay. Based on map notes (Ryan *et al.* 2017) the Werillup aquitard is inferred as extensive throughout the King River area and likely lies below all areas of the site and beyond.
- Werillup aquitard is probably underlain by granite, based on evidence of minor cuttings returned to the surface exhibiting angular quartz and some mica.
- The groundwater levels of the Pallinup formation appears to be similar to the shallow groundwater levels. That is to say that, excluding times when winter rainfall may perch shallow groundwater, the shallow sandy silts are probably hydraulically connected with the Pallinup Formation.
- The groundwater flow direction of the Pallinup Formation is not well known, however, beneath the Site groundwater it is likely to follow the regional topography, and flow towards the south west where groundwater is likely to discharge into the rivers and creeks, such as dominant surface water feature in areas close to the Site - Marbelup Brook.

## A-4-4 Discussion/interpretations on pathway

The hydrogeological setting indicates the following Conceptual Site Model:

- The depth to groundwater plan indicates that in areas adjacent to the surface water creek/ feature, the depth to groundwater is less than 2 metres. In these areas, it is considered that there is an increased risk of impacts to groundwater from surface contaminants and spills given the thin geological profile (e.g. low adsorptive capacity).
- The shallow groundwater migration direction (shallow sands/silt and Pallinup Formation) indicates that any Site based groundwater impacts should migrate towards the creek line (on Site) where groundwater (and any impacted groundwater) is inferred to discharge. Any impacted surface water will migrate towards areas off-site and discharge into the major drainage of the area, the Marbelup Brook.
- Any Site based groundwater impacts should preferentially migrate within shallow sands/silts (towards the creek lines) and not migrate downwards into the deeper levels of the Pallinup Formation given the similar groundwater levels between the Pallinup Formation and the overlying shallow sandy silts, and that the shallow sandy silts have a higher permeability than the Pallinup Formation
- Given the low permeability of the Pallinup Formation, any Site based groundwater impacts, which may migrate downwards into the Pallinup formation should be subject to attenuation processes, which should limit the extent and migration rate of the any impacts.
- It appears from the limited drilling information (one monitoring well) that the Pallinup Formation is underlain by the Werillup Aquitard and granite, which should constrain any potential groundwater impacts to the Pallinup Formation.

## A-4-5 Potential receptors

The Conceptual Site Model indicates that Site groundwater impacts will migrate towards the on-site creek, the receptors comprise the following:

- the environment of the onsite creek (flora and fauna)
- creek systems down-gradient of the site (flora and fauna)
- groundwater bore users - where bores are located close to, and are in hydraulic connection, with the creek system
- surface water users/abstraction of surface water; and
- livestock accessing creek.

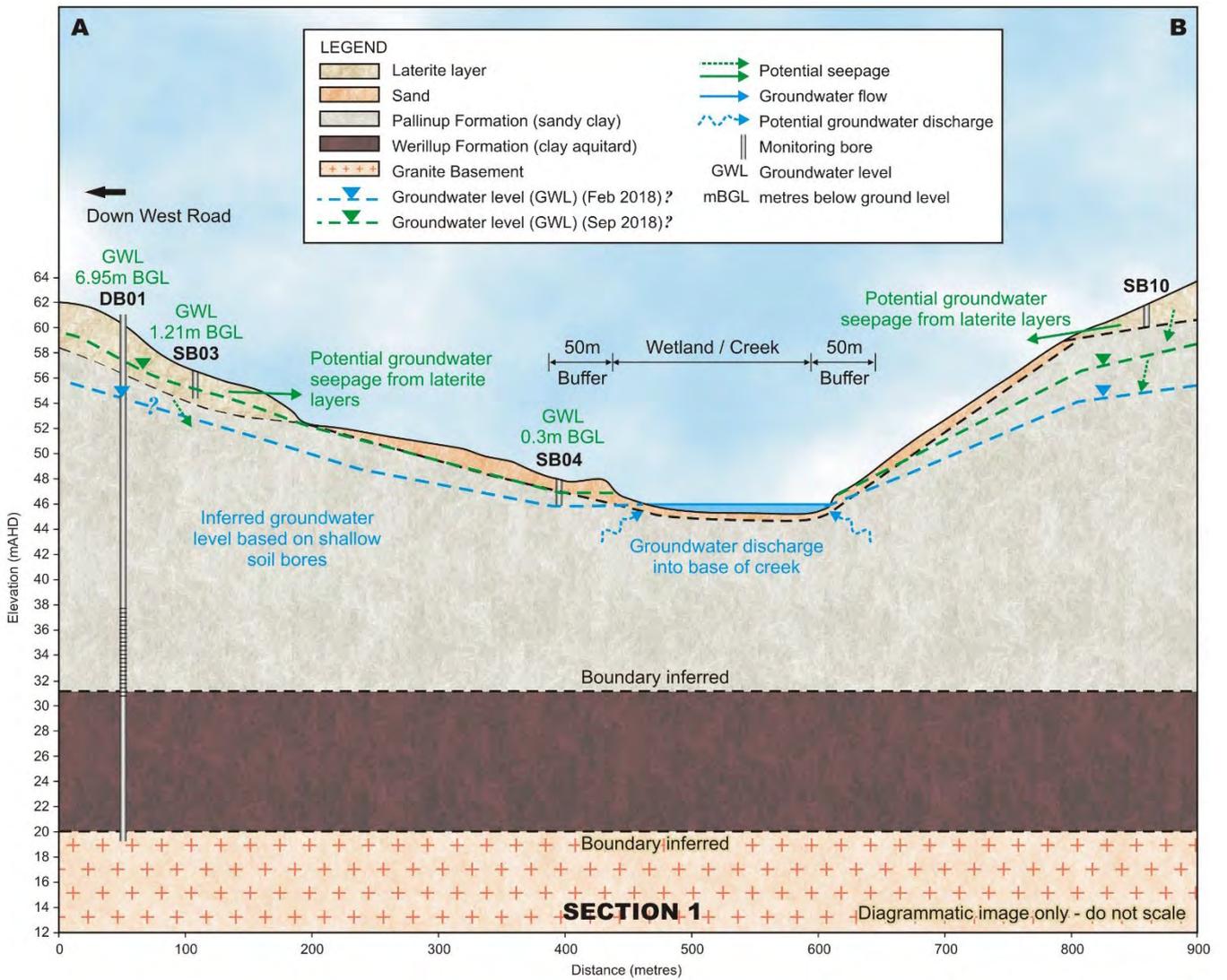


Plate 3 Preliminary hydrogeological section 1 (A-B)

# Appendix E

## Potential water users

Figure E.1 Potential surface water users

Table E.1 Licensed groundwater abstractions

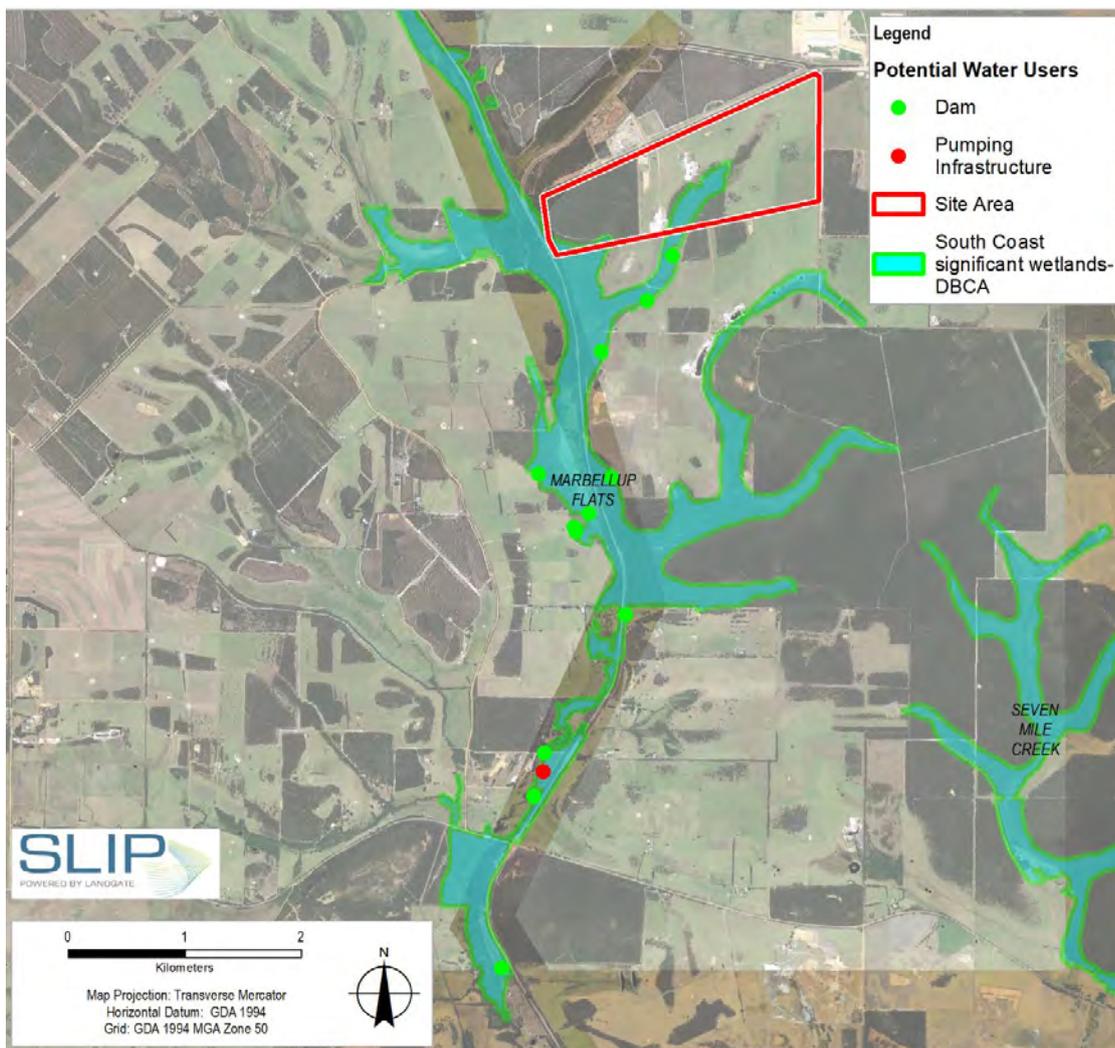


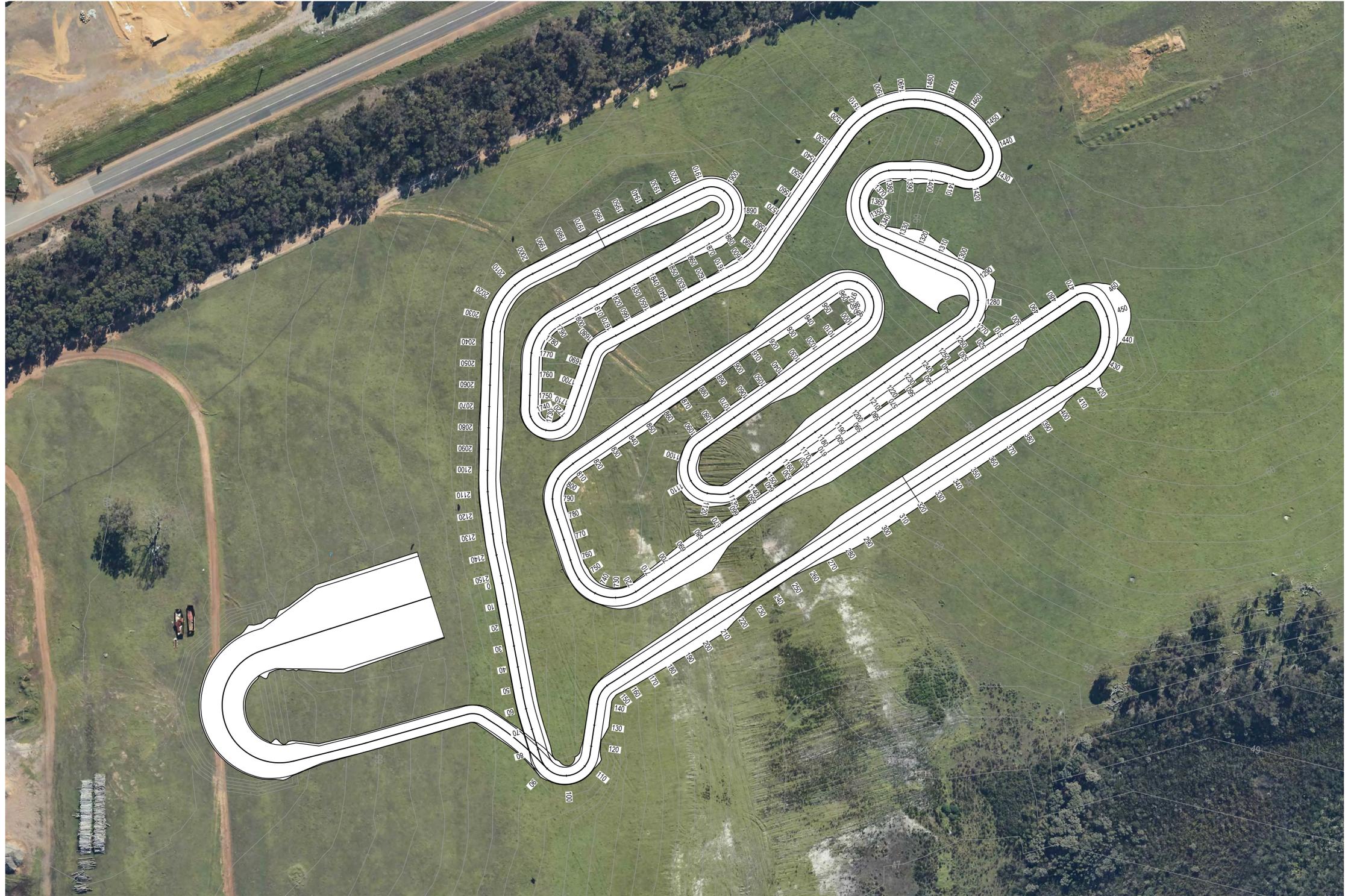
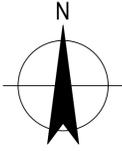
Figure E.1 Potential surface water users

Table E.1 Licensed groundwater abstractions

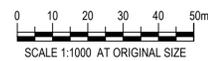
Licence No.	Licence allocation (kL/yr)	Expiry date	Location	Aquifer
168308	4000	31/8/2028	Project Site Lot 5780 Down Road, Drome	168308
156374	1400	30/09/2024	Lot 7235 Marbelup ~3.5 km downgradient	156374
76457	33200	8/04/2020	Lot 500 Marbelup ~6.5 km downgradient	76457
160280	1000	13/05/2026	Lot 86 Elleker Crown Reserve ~8 km downgradient	Bremer West – Superficial
155130	26000	20/10/2022	Lot 200 Lower Denmark Rd Elleker ~9.5 km downgradient	Bremer West – Sedimentary
173352	2100	16/05/2021	Wilgie Rd, Torbay	Bremer West – Superficial

# Appendix F

**Motocross track drawings**



PLAN  
SCALE 1:1000



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Project No.

Client CITY OF ALBANY

Project ALBANY MOTORSPORTS PARK  
MX TRACK

Status PRELIMINARY

Drawing Title PLAN

Size  
A1

Rev

Rev	Description	Checked	Approved	Date
Author	B SHAW		Drafting Check	
Designer	B SHAW		Design Check	

Plot Date: 12 August 2021 - 1:34 PM Plotted by: Bradley Shaw

File Name: C:\12d\SWdata\IP-00-12D-001\61-12546218 - Albany Motorsport Park DA\_1367\CADD\Drawings\12546218-C001.dwg

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Status Code

Drawing No.  
12546218-C001



CONTINUE ON LSEC BELOW

DATUM RL. 51.00

GROUNDWATER	54.25	54.94	55.41	55.72	56.49	57.23	58.09	58.95	59.50	59.82	60.27	60.41	60.55	60.55	60.50	60.40	60.35	60.27	60.19	60.99	61.62	62.22	62.79	63.26	63.67	64.10	64.57	64.98	65.36	65.71	66.03	66.31	66.54	66.72	66.85	66.93	66.97	66.97	66.93	66.85	66.72	66.54	66.31	66.03	65.71	65.36	64.98	64.57	64.10	63.67	63.26	62.79	62.22	61.62	60.99	60.40	60.35	60.27	60.19	60.00	59.82	59.50	58.95	58.09	56.49	55.72	55.41	54.94	54.25																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
BULK EARTHWORKS SURFACE LEVEL	56.25	56.94	57.41	57.72	58.49	59.23	60.09	60.95	61.50	61.82	62.27	62.41	62.55	62.55	62.50	62.40	62.35	62.27	62.19	61.99	61.62	62.22	62.79	63.26	63.67	64.10	64.57	64.98	65.36	65.71	66.03	66.31	66.54	66.72	66.85	66.93	66.97	66.97	66.93	66.85	66.72	66.54	66.31	66.03	65.71	65.36	64.98	64.57	64.10	63.67	63.26	62.79	62.22	61.62	60.99	60.40	60.35	60.27	60.19	60.00	59.82	59.50	58.95	58.09	56.49	55.72	55.41	54.94	54.25																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																		
LEVEL DIFFERENCE CUT - / FILL +	1.35	1.26	1.20	1.21	1.18	1.03	0.90	0.78	0.70	0.65	0.67	0.62	0.62	0.62	0.60	0.59	0.58	0.56	0.54	0.52	0.50	0.52	0.53	0.54	0.55	0.56	0.57	0.58	0.59	0.60	0.61	0.62	0.63	0.64	0.65	0.66	0.67	0.68	0.69	0.70	0.71	0.72	0.73	0.74	0.75	0.76	0.77	0.78	0.79	0.80	0.81	0.82	0.83	0.84	0.85	0.86	0.87	0.88	0.89	0.90	0.91	0.92	0.93	0.94	0.95	0.96	0.97	0.98	0.99	1.00	1.01	1.02	1.03	1.04	1.05	1.06	1.07	1.08	1.09	1.10	1.11	1.12	1.13	1.14	1.15	1.16	1.17	1.18	1.19	1.20	1.21	1.22	1.23	1.24	1.25	1.26	1.27	1.28	1.29	1.30	1.31	1.32	1.33	1.34	1.35																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																														
TRACK DESIGN SURFACE LEVEL	56.614	57.291	57.710	58.011	58.802	59.593	60.384	61.175	61.673	61.966	62.463	62.604	62.745	62.745	62.694	62.593	62.492	62.391	62.290	62.189	62.088	62.189	62.290	62.391	62.492	62.593	62.694	62.795	62.896	62.997	63.098	63.199	63.300	63.401	63.502	63.603	63.704	63.805	63.906	64.007	64.108	64.209	64.310	64.411	64.512	64.613	64.714	64.815	64.916	65.017	65.118	65.219	65.320	65.421	65.522	65.623	65.724	65.825	65.926	66.027	66.128	66.229	66.330	66.431	66.532	66.633	66.734	66.835	66.936	67.037	67.138	67.239	67.340	67.441	67.542	67.643	67.744	67.845	67.946	68.047	68.148	68.249	68.350	68.451	68.552	68.653	68.754	68.855	68.956	69.057	69.158	69.259	69.360	69.461	69.562	69.663	69.764	69.865	69.966	70.067	70.168	70.269	70.370	70.471	70.572	70.673	70.774	70.875	70.976	71.077	71.178	71.279	71.380	71.481	71.582	71.683	71.784	71.885	71.986	72.087	72.188	72.289	72.390	72.491	72.592	72.693	72.794	72.895	72.996	73.097	73.198	73.299	73.400	73.501	73.602	73.703	73.804	73.905	74.006	74.107	74.208	74.309	74.410	74.511	74.612	74.713	74.814	74.915	75.016	75.117	75.218	75.319	75.420	75.521	75.622	75.723	75.824	75.925	76.026	76.127	76.228	76.329	76.430	76.531	76.632	76.733	76.834	76.935	77.036	77.137	77.238	77.339	77.440	77.541	77.642	77.743	77.844	77.945	78.046	78.147	78.248	78.349	78.450	78.551	78.652	78.753	78.854	78.955	79.056	79.157	79.258	79.359	79.460	79.561	79.662	79.763	79.864	79.965	80.066	80.167	80.268	80.369	80.470	80.571	80.672	80.773	80.874	80.975	81.076	81.177	81.278	81.379	81.480	81.581	81.682	81.783	81.884	81.985	82.086	82.187	82.288	82.389	82.490	82.591	82.692	82.793	82.894	82.995	83.096	83.197	83.298	83.399	83.500	83.601	83.702	83.803	83.904	84.005	84.106	84.207	84.308	84.409	84.510	84.611	84.712	84.813	84.914	85.015	85.116	85.217	85.318	85.419	85.520	85.621	85.722	85.823	85.924	86.025	86.126	86.227	86.328	86.429	86.530	86.631	86.732	86.833	86.934	87.035	87.136	87.237	87.338	87.439	87.540	87.641	87.742	87.843	87.944	88.045	88.146	88.247	88.348	88.449	88.550	88.651	88.752	88.853	88.954	89.055	89.156	89.257	89.358	89.459	89.560	89.661	89.762	89.863	89.964	90.065	90.166	90.267	90.368	90.469	90.570	90.671	90.772	90.873	90.974	91.075	91.176	91.277	91.378	91.479	91.580	91.681	91.782	91.883	91.984	92.085	92.186	92.287	92.388	92.489	92.590	92.691	92.792	92.893	92.994	93.095	93.196	93.297	93.398	93.499	93.600	93.701	93.802	93.903	94.004	94.105	94.206	94.307	94.408	94.509	94.610	94.711	94.812	94.913	95.014	95.115	95.216	95.317	95.418	95.519	95.620	95.721	95.822	95.923	96.024	96.125	96.226	96.327	96.428	96.529	96.630	96.731	96.832	96.933	97.034	97.135	97.236	97.337	97.438	97.539	97.640	97.741	97.842	97.943	98.044	98.145	98.246	98.347	98.448	98.549	98.650	98.751	98.852	98.953	99.054	99.155	99.256	99.357	99.458	99.559	99.660	99.761	99.862	99.963	100.064	100.165	100.266	100.367	100.468	100.569	100.670	100.771	100.872	100.973	101.074	101.175	101.276	101.377	101.478	101.579	101.680	101.781	101.882	101.983	102.084	102.185	102.286	102.387	102.488	102.589	102.690	102.791	102.892	102.993	103.094	103.195	103.296	103.397	103.498	103.599	103.700	103.801	103.902	104.003	104.104	104.205	104.306	104.407	104.508	104.609	104.710	104.811	104.912	105.013	105.114	105.215	105.316	105.417	105.518	105.619	105.720	105.821	105.922	106.023	106.124	106.225	106.326	106.427	106.528	106.629	106.730	106.831	106.932	107.033	107.134	107.235	107.336	107.437	107.538	107.639	107.740	107.841	107.942	108.043	108.144	108.245	108.346	108.447	108.548	108.649	108.750	108.851	108.952	109.053	109.154	109.255	109.356	109.457	109.558	109.659	109.760	109.861	109.962	110.063	110.164	110.265	110.366	110.467	110.568	110.669	110.770	110.871	110.972	111.073	111.174	111.275	111.376	111.477	111.578	111.679	111.780	111.881	111.982	112.083	112.184	112.285	112.386	112.487	112.588	112.689	112.790	112.891	112.992	113.093	113.194	113.295	113.396	113.497	113.598	113.699	113.800	113.901	114.002	114.103	114.204	114.305	114.406	114.507	114.608	114.709	114.810	114.911	115.012	115.113	115.214	115.315	115.416	115.517	115.618	115.719	115.820	115.921	116.022	116.123	116.224	116.325	116.426	116.527	116.628	116.729	116.830	116.931	117.032	117.133	117.234	117.335	117.436	117.537	117.638	117.739	117.840	117.941	118.042	118.143	118.244	118.345	118.446	118.547	118.648	118.749	118.850	118.951	119.052	119.153	119.254	119.355	119.456	119.557	119.658	119.759	119.860	119.961	120.062	120.163	120.264	120.365	120.466	120.567	120.668	120.769	120.870	120.971	121.072	121.173	121.274	121.375	121.476	121.577	121.678	121.779	121.880	121.981	122.082	122.183	122.284	122.385	122.486	122.587	122.688	122.789	122.890	122.991	123.092	123.193	123.294	123.395	123.496	123.597	123.698	123.799	123.900	124.001	124.102	124.203	124.304	124.405	124.506	124.607	124.708	124.809	124.910	125.011	125.112	125.213	125.314	125.415	125.516	125.617	125.718	125.819	125.920	126.021	126.122	126.223	126.324	126.425	126.526	126.627	126.728	126.829	126.930	127.031	127.132	127.233	127.334	127.435	127.536	127.637	127.738	127.839	127.940	128.041	128.142	128.243	128.344	128.445	128.546	128.647	128.748	128.849	128.950	129.051	129.152	129.253	129.354	129.455	129.556	129.657	129.758	129.859	129.960	130.061	130.162	130.263	130.364	130.465	130.566	130.667	130.768	130.869	130.970	131.071	131.172	131.273	131.374	131.475	131.576	131.677	131.778	131.879	131.980	132.081	132.182	132.283	132.384	132.485	132.586	132.687	132.788	132.889	132.990	133.091	133.192	133.293	133.394	133.495	133.596	133.697	133.798	133.899	134.000	134.101	134.202	134.303	134.404	134.505	134.606	134.707	134.808	134.909	135.010	135.111	135.212	135.313	135.414	135.515	135.616	135.717	135.818	135.919	136.020	136.121	136.222	136.323	136.424	136.525	136.626	136.727	136.828	136.929	137.030	137.131	137.232	137.333	137.434	137.535	137.636	137.737	137.838	137.939	138.040	138.141	138.242	138.343	138.444	138.545	138.646	138.747	138.848	138.949	139.050	139.151	139.252	139.353	139.454	139.555	139.656	139.757	139.858	139.959	140.060	140.161	140.262	140.363	140.464	140.565	140.666	140.767	140.868	140.969	141.070	141.171	141.272	141.373	141.474	141.575	141.676	141.777	141.878	141.979	142.080	142.181	142.282	142.383	142.484	142.585	142.686	142.787	142.888	142.989	143.090	143.191	143.292	143.393	143.494	143.595	143.696	143.797	143.898	143.999	144.100	144.201	144.302	144.403	144.504	144.605	144.706	144.807	144.908	145.009	145.110	145.211	145.312	145.413	145.514	145.615	145.716	145.817	145.918	146.019	146.120	146.221	146.



# Appendix G

**DRAINS modelling results schematics**

Summary of DRAINS Results															
Basin	Peak Water Level			Peak Inflow			Peak Outflow			Peak Stored Vol			Critical Duration		
	1EY	10% AEP	1% AEP	1EY	10% AEP	1% AEP	1EY	10% AEP	1% AEP	1EY	10% AEP	1% AEP	1EY	10% AEP	1% AEP
East-B1	58.78	58.88	59.06	0.052	0.225	0.635	0.032	0.196	0.464	231	278	385	6hr	2hr	30min
East-B2	57.22	57.55	57.65	0.054	0.241	0.655	0.006	0.055	0.254	121	362	446	9hr	3hr	1hr
East-B3	70.27	70.56	70.75	0.072	0.272	0.647	0	0.031	0.282	110	277	410	3hr	1hr	1hr
East-B4	71.18	71.34	71.41	0.227	0.729	1.088	0	0.111	0.201	53	117	150	25min	25min	15min
East-B5	66.82	67.1	67.23	0.24	0.335	0.792	0.021	0.174	0.464	417	666	791	3hr	2hr	1hr
East-B6	61.19	61.4	61.61	0.032	0.534	1.834	0.018	0.405	0.628	127	300	516	6hr	2hr	30min
East-B7	65.53	65.66	65.97	0.329	0.386	1.241	0.04	0.287	0.679	223	298	528	6hr	2hr	9hr
East-B8	70.58	70.77	71.03	0.024	0.069	0.2	0	0	0.02	21	81	191	1hr	3hr	9hr
East-B9	63.02	63.3	63.65	0.042	0.163	0.499	0	0	0.255	18	314	788	2hr	3hr	2hr
East-B10	62.14	62.36	62.52	0.04	0.286	0.977	0.02	0.189	0.55	64	198	320	2hr	2hr	30min
West-B1	66.21	66.69	66.7	0.014	0.115	0.32	0	0.083	0.113	22	97	100	9hr	9hr	9hr
West-B2	62.3	62.39	62.43	0.137	0.269	0.435	0.014	0.047	0.116	79	121	144	1hr	45min	15min
West-B3	62.91	63.25	63.31	0.057	0.145	0.269	0	0.038	0.146	79	168	186	3hr	3hr	30min
West-B4	59.53	59.61	59.68	0.086	0.198	0.401	0.044	0.173	0.361	77	93	109	1hr	30min	15min
West-B5	53.92	54.13	54.25	0.057	0.296	0.641	0.029	0.242	0.582	55	94	118	3hr	1hr	30min
West-B6	58	58.42	58.57	0	0.044	0.158	0	0	0.069	0	67	106	-	3hr	2hr
West-B7	51.85	52.3	52.44	0.056	0.326	0.724	0	0.138	0.529	181	500	627	6hr	3hr	2hr
Drains/swales	Shape	Slope	Depth	Length	10% flow	1EY	10% AEP	1% AEP	1EY	10% AEP	1% AEP	1EY	10% AEP	1% AEP	
E-B1-01	1.6 swale	0.51	0.406	83	0.037	0.01	0.037	0.092	0.065	0.106	0.144				
E-B1-02A	1.6 swale	0.54	0.448	130.5	0.052	0.003	0.052	0.212	0.052	0.148	0.244				
E-B1-02B	1.6 swale	2.78	0.41	28.8	0.057	0.005	0.057	0.233	0.045	0.11	0.186				
E-B1-03A	1.6 swale	2.1	0.501	142.8	0.189	0.077	0.189	0.352	0.149	0.201	0.253				
E-B1-03B	1.6 swale	2.08	0.474	312.1	0.17	0.047	0.17	0.431	0.108	0.174	0.247				
E-B1-04	1.4 swale	0.54	0.44	184.8	0.024	0	0.024	0.104	0	0.14	0.23				
E-B1-04-CONNECT	Dummy OF	3.25	0.428	92.4	0.02	0	0.02	0.077	0	0.128	0.201				
E-B2-01	1.4 swale	4.23	0.459	142	0.125	0.027	0.125	0.338	0.089	0.159	0.231				
E-B2-02	1.6 swale	5.28	0.428	56.8	0.116	0.027	0.116	0.317	0.074	0.128	0.185				
E-B3-01	1.6 swale	1.26	0.437	118.7	0.067	0.023	0.067	0.171	0.092	0.137	0.249				
E-B3-02	1.6 swale	0.53	0.861	112.9	0.132	0.051	0.132	0.291	0.265	0.561	0.749				
E-B4-01	K300, 0.4m deep	0.5	0.57	150.2	0.09	0.046	0.09	0.15	0.161	0.27	0.405				
E-B4-02	1.4 swale	0.9	0.586	211.6	0.248	0.113	0.248	0.436	0.228	0.286	0.348				
E-B5-01	1.4 swale	2.56	1.291	159.6	0.113	0.057	0.113	0.228	0.574	0.991	1.247				
E-B5-02	1.4 swale	1.49	1.291	375.5	0.53	0.256	0.53	0.946	0.574	0.991	1.247				
E-B6-01	1.6 swale	3.87	0.699	142	0.094	0.007	0.094	0.32	0.19	0.399	0.614				
E-B6-02	1.4 swale	5.3	0.699	158.6	0.051	0.005	0.051	0.18	0.19	0.399	0.614				
E-B6-03	1.6 swale	0.8	0.699	310.6	0.158	0.011	0.158	0.655	0.19	0.399	0.614				
E-B7-01	1.4 swale	0.67	0.508	74.5	0.098	0.023	0.098	0.285	0.092	0.208	0.304				
E-B7-02	1.6 swale	0.62	0.408	160.6	0.025	0	0.025	0.128	0	0.108	0.195				
E-B7-03	1.6 swale	1.16	0.435	129.3	0.06	0.021	0.06	0.127	0.091	0.135	0.174				
E-B7-04	1.4 swale	0.97	0.685	61	0.101	0.052	0.101	0.164	0.285	0.385	0.524				
E-B7-05	1.4 swale	1.92	0.685	30.7	0.042	0.022	0.042	0.063	0.287	0.385	0.524				
E-B7-06	1.4 swale	2.67	0.854	149.8	0.13	0.065	0.13	0.289	0.226	0.365	0.854				
E-B7-07	1.4 swale	1.57	0.832	127.4	0.033	0	0.033	0.192	0	0.395	0.832				
E-B7-08	1.6 swale	2.66	0.446	153.8	0.115	0.054	0.115	0.222	0.113	0.146	0.179				
E-B7-09	1.6 swale	1.45	0.463	144.6	0.113	0.053	0.113	0.222	0.128	0.163	0.203				
E-B7-10A	1.6 swale	1.97	0.446	126.8	0.054	0.004	0.054	0.174	0.049	0.146	0.226				
E-B7-10B	1.4 swale	1.12	0.581	133.8	0.05	0.002	0.05	0.193	0.185	0.281	0.431				
E-B7-11	1.4 swale	0.01	0.773	73.1	0.227	0.077	0.227	0.579	0.412	0.473	0.691				
E-B8-01A	1.4 swale	0.56	0.569	126.1	0.037	0.013	0.037	0.113	0.108	0.269	0.53				
E-B8-01B	1.4 swale	2.08	0.569	120.2	0.032	0.011	0.032	0.087	0.083	0.269	0.53				
E-B9-01	1.6 swale	3.6	0.447	152.7	0.129	0.034	0.129	0.255	0.093	0.147	0.211				
E-B9-02	1.6 swale	1.57	0.441	95.6	0.059	0.015	0.059	0.115	0.077	0.141	0.211				
E-B9-03	1.6 swale	3.65	0.802	167	0.03	0	0.03	0.163	0	0.388	0.802				
E-B9-04	1.6 swale	1.85	0.802	113.2	0.019	0	0.019	0.105	0	0.388	0.802				
E-B9-05	1.4 swale	2.78	0.416	165.1	0.04	0.012	0.04	0.132	0.08	0.116	0.203				
E-B9-06	1.4 swale	1.37	0.405	116.3	0.023	0.007	0.023	0.073	0.069	0.105	0.206				
E-B9-07	1.4 swale	1.64	0.781	341.3	0.072	0	0.072	0.402	0	0.322	0.781				
E-B9-08	1.4 swale	0.94	0.781	115.5	0.024	0	0.024	0.125	0	0.322	0.781				
E-B10-01	1.6 swale	0.55	0.658	182.6	0.042	0.005	0.042	0.15	0.135	0.358	0.521				
E-B10-02	1.6 swale	0.49	0.658	306.3	0.181	0.026	0.181	0.617	0.135	0.358	0.521				
E-B10-03A	1.6 swale	3.09	0.41	83.7	0.041	0.012	0.041	0.095	0.062	0.11	0.176				
E-B10-03B	1.6 swale	1.69	0.658	54	0.064	0.01	0.064	0.21	0.135	0.358	0.521				
E-B10-04	1.6 swale	2.44	0.475	82	0.017	0	0.017	0.059	0	0.175	0.319				
E-B10-05	1.4 swale	3.18	0.475	94.3	0.027	0	0.027	0.061	0	0.175	0.319				
W-B1-01	1.6 swale	0.67	0.438	178.5	0.051	0.009	0.051	0.145	0.074	0.138	0.201				
W-B1-02	1.6 swale	0.85	0.417	100	0.029	0.006	0.029	0.073	0.069	0.117	0.178				
W-B1-03	1.6 swale	0.52	0.458	96.6	0.026	0.005	0.026	0.068	0.071	0.158	0.252				
W-B1-04	1.6 swale	0.91	1.003	109.3	0.464	0.001	0.464	0.473	0.248	0.703	0.707				
W-B1-05	1.6 swale	0.35	1.003	140.9	0.721	0.001	0.721	0.725	0.248	0.703	0.707				
W-B3-01	1.6 swale	5.88	1.047	80	0.145	0.057	0.145	0.269	0.41	0.747	0.808				
W-B4-01	1.6 swale	1.8	0.909	166.8	0.088	0.038	0.088	0.183	0.533	0.609	0.684				
W-B4-02	1.6 swale	4.81	0.909	197.5	0.11	0.048	0.11	0.22	0.533	0.609	0.684				
W-B5-01	1.6 swale	4.3	0.473	59.8	0.022	0.002	0.022	0.052	0.055	0.173	0.29				
W-B5-02	1.6 swale	3.34	0.473	32	0.013	0.002	0.013	0.03	0.055	0.173	0.29				
W-B5-03	1.6 swale	9	0.34	77.8	0.005	0	0.005	0.029	0	0.04	0.075				
W-B5-04	1.6 swale	3	0.811	40	0.188	0.044	0.188	0.574	0.224	0.511	0.763				
W-B5-05	1.6 swale	4.89	0.798	45	0.018	0.003	0.018	0.04	0.266	0.498	0.763				
W-B5-06 07	1.6 swale	5.8	0.695	150	0.104	0.025	0.104	0.235	0.218	0.395	0.649				
W-B5-08	1.6 swale	2.01	0.695	59.7	0.038	0.009	0.038	0.082	0.218	0.395	0.649				
W-B5-09	1.6 swale	4.63	0.479	80	0.044	0.01	0.044	0.093	0.153	0.179	0.291				
W-B5-11	1.6 swale	1.85	0.345	27.1	0.004	0	0.004	0.018	0	0.045	0.077				
W-B5-12	1.6 swale	5.19	0.347	28.9	0.007	0.001	0.007	0.016	0.027	0.047	0.063				
W-B5-13A	1.6 swale	1.01	0.935	79.3	0.359	0.054	0.359	0.552	0.419	0.635	0.753				
W-B5-13B	1.6 swale	1.75	0.935	51.9	0.143	0.007	0.143	0.18	0.419	0.635	0.753				
W-B5-16	1.6 swale	3.8	0.935	79	0.021	0	0.021	0.054	0	0.635	0.753				
W-B5-CULV14 15	1.6 swale	4.38	0.665	164.5	0.087	0.015	0.087	0.196	0.124	0.365	0.643				
W-B6-01	1.6 swale	0.69	0.717	175	0.041	0	0.041								



Stage 1A (WEST) DRAINS Results							
DRAINS results prepared from Version 2020.036							
1EY							
PIT / NODE DETAILS				Version 8			
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
DUMMY-SCALE2	10		0				
DUMMY-SCALE1	8		0				
W1-B1-01-US	69		0				
W-B1-02-US	68.65		0				
W-B1-03-US	68.65		0				
W-B1-04-US	67		0				
W-B1-05-US	66.5		0				
W-B4-01-US	62		0				
W-B4-02-US	68.5		0				
W-B5-CULV1-HW	56.49		0.008			0.51	0 None
W-B5-CULV1-DS	56.2		0				
W-B5-CULV2-HW	56.02		0.115			0.48	0 None
W-B5-CULV2-DS	55.52		0				
W-B5-CULV3-HW	54.97		0.112			0.53	0 None
W-B5-CULV3-DS	54.43		0.013				
W-B5-CULV4-HW	56.91		0			1.09	0 None
W-B5-CULV4-DS	56.51		0				
W-B5-CULV5-HW	55.35		0.002			1.15	0 None
W-B5-CULV5-DS	54.44		0				
W-B7-CULV2-HW	55.92		0			1.08	0 None
W-B7-CULV2-DS	55.42		0				
W-B5-CULV6-HW	52.12		0.028			0.88	0 None
N87219	51.86		0				
W-B1-CULV1-HW	68.22		0.011			0.78	0 None
W1-01-DS	67.87		0.032				
N87159	65.15		0				
N87076	64.01		0				
N87168	61.29		0				
W-EXT02-US	61.09		0.002				
W-EXT	60.57		0.016				
W-EXT-CULV1-HW	59.23		0.016			1.27	0 None
W-EXT-CULV1-DS	59.07		0				
N87207	61.65		0				
N87255	61.01		0				
W-EXT-HW	64.2		0			0.8	0 None
N87181	58.21		0				
W-B5-03-DS	57.1		0				
W-B5-03-US	62		0				
W-B5-06-US	63.5		0				
W-B5-01-US	59		0				
W-B5-02-US	57.5		0				
W-B5-05-US	58		0				
W-B5-08-US	56		0				
W-B5-09-US	58		0				
W-B5-11-US	58		0				
W-B5-12-US	57.5		0				
N87237	57.26		0				
N87238	57.1		0				
W-B6-01-US	59.2		0				
N87225	52.7		0				
N87218	52.42		0				
W-B5-16-US	56.5		0				
W-B5-CULV14-US	59.2		0				
W-B7-CULV1-HW	51.85		0.093			1.15	0 None
N87244	49.24		0				
N87245	49.01		0				
W-B7-02-US	62.5		0				
HW12	53.04		0.016			0.96	0 None
N87149	51.91		0				
HW13	47.01		0.009			0.99	0 None
N87150	46.8		0				
W-B3-01-US	67.2		0				
S1 US	57.5		0				
SUB-CATCHMENT DETAILS							
Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm
W-B5-CULV1-CAT	0.007	0	0.007	0	0	6.1	1EY AEP, 2 hour burst, Storm 2
W-B5-CULV2-CAT	0.008	0	0.008	0	0	8.08	3.94 1EY AEP, 2 hour burst, Storm 3
W-B5-CULV3-CAT	0.038	0	0.038	0	0	5.22	2.54 1EY AEP, 1 hour burst, Storm 1
W-B5-CULV3-DS-CAT	0.012	0	0.012	0	0	4.04	1.97 1EY AEP, 1 hour burst, Storm 1
W-B5-CULV4-CAT	0	0	0	0	0	1.98	0 1EY AEP, 10 min burst, Storm 5
W-B5-CULV5-CAT	0.002	0	0.002	0	0	4.6	2.24 1EY AEP, 1 hour burst, Storm 9
W-B5-CULV6-CAT	0.025	0	0.025	0	0	5.18	2.52 1EY AEP, 2 hour burst, Storm 3
W-B1-03-CAT	0.01	0	0.01	0	0	3.83	1.87 1EY AEP, 1 hour burst, Storm 1
W-B1-01-CAT	0.03	0	0.03	0	0	5.33	2.6 1EY AEP, 1 hour burst, Storm 1
WEST-B1-CAT	0.012	0	0.012	0	0	11.03	5.38 1EY AEP, 2 hour burst, Storm 3
WEST-B2-CAT	0.137	0.137	0	3.8	0	0	0 1EY AEP, 10 min burst, Storm 10
W-EXT-CAT	0	0	0	0	0	2.62	0 1EY AEP, 10 min burst, Storm 5
W-EXT04-CAT	0	0	0	0	0	2.18	1.06 1EY AEP, 10 min burst, Storm 5
WEST-B3-CAT	0.066	0	0.066	0	0	8.4	4.1 1EY AEP, 15 min burst, Storm 1
CulvW_ext	0	0	0	5	0	75	2 1EY AEP, 10 min burst, Storm 5
WEST-B4-CAT	0.161	0.161	0	4.34	0	10.08	0 1EY AEP, 10 min burst, Storm 4
W-B5-03-CAT	0	0	0	0	0	2.69	0 1EY AEP, 10 min burst, Storm 5
WEST-B6-CAT	0	0	0	0	0	3.56	1.74 1EY AEP, 10 min burst, Storm 5
WEST-B5-CAT	0	0	0	0	0	3.65	1.78 1EY AEP, 10 min burst, Storm 5
W-B7-01-CAT	0	0	0	0	0	3.33	0 1EY AEP, 10 min burst, Storm 5
WEST-B7-CAT	0.065	0	0.065	0	0	4.8	2.34 1EY AEP, 15 min burst, Storm 1
S1_catch	0	0	0	0	0	24.81	0 1EY AEP, 10 min burst, Storm 5
PIPE DETAILS							
Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm		
DUMMY-SCALE	0	0	10	8	1EY AEP, 10 min burst, Storm 5		
W-B5-CULV1	0.002	0.47	56.485	56.199	1EY AEP, 2 hour burst, Storm 9		
W-B5-CULV2	0.042	1.84	56.024	55.515	1EY AEP, 1 hour burst, Storm 1		
W-B5-CULV3	0.05	1.46	54.974	54.574	1EY AEP, 2 hour burst, Storm 3		
W-B5-CULV4	0	0	56.91	56.51	1EY AEP, 10 min burst, Storm 5		
W-B5-CULV5	0.001	0.31	55.347	54.44	1EY AEP, 2 hour burst, Storm 2		
Pipe20528	0	0	55.913	55.416	1EY AEP, 10 min burst, Storm 5		
W-B5-CULV6	0.012	0.87	52.121	51.862	1EY AEP, 2 hour burst, Storm 4		
W-B1-CULV1	0.004	0.23	68.22	67.869	1EY AEP, 2 hour burst, Storm 4		
Pipe20532	0	0	65.25	65.152	1EY AEP, 10 min burst, Storm 5		

Pipe20533	0	0	65.152	64.75	1EY AEP, 10 min burst, Storm 5				
Pipe20566	0	0	61.3	61.294	1EY AEP, 10 min burst, Storm 5				
Pipe20567	0.014	1.3	61.294	61.093	1EY AEP, 1 hour burst, Storm 1				
W-EXT-CULV1	0.013	0.81	59.229	59.072	1EY AEP, 3 hour burst, Storm 7				
Pipe20702	0	0	61.75	61.652	1EY AEP, 10 min burst, Storm 5				
Pipe20716	0	0	61.652	61.005	1EY AEP, 10 min burst, Storm 5				
W-EXT-CULV	0	0	64.2	61.093	1EY AEP, 10 min burst, Storm 5				
Pipe20591	0.02	1.23	58.397	58.211	1EY AEP, 1 hour burst, Storm 1				
Pipe20597	0.044	3.05	58.211	57.566	1EY AEP, 1 hour burst, Storm 1				
Pipe20785	0	0	57.303	57.263	1EY AEP, 10 min burst, Storm 5				
Pipe20790	0	0	57.263	57.105	1EY AEP, 10 min burst, Storm 5				
Pipe20745	0	0	52.7	52.695	1EY AEP, 10 min burst, Storm 5				
Pipe20746	0.029	1.72	52.695	52.425	1EY AEP, 3 hour burst, Storm 6				
Pipe20525	0.032	0.15	51.854	51.854	1EY AEP, 3 hour burst, Storm 6				
Pipe20821	0	0	49.3	49.242	1EY AEP, 10 min burst, Storm 5				
Pipe20830	0	0	49.242	49.008	1EY AEP, 10 min burst, Storm 5				
Pipe20526	0.013	1.58	53.037	51.956	1EY AEP, 3 hour burst, Storm 7				
Pipe20527	0	0	47.003	46.8	1EY AEP, 9 hour burst, Storm 3				

CHANNEL DETAILS

Name	Max Q (cu.m/s)	Max V (m/s)		Due to Storm
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OVERFLOW ROUTE DETAILS

Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V	Due to Storm
O134039	0.009	0	12.141	3	0	32	0	1EY AEP, 3 hour burst, Storm 6
O134055	0.009	0	12.141	3	0	32	0	1EY AEP, 3 hour burst, Storm 6
O137112	0.005	0	12.141	3	0	32	0	1EY AEP, 1 hour burst, Storm 1
O137116	0.005	0	12.141	3	0	32	0	1EY AEP, 1 hour burst, Storm 1
O137914	0.006	0	12.141	3	0	32	0	1EY AEP, 1 hour burst, Storm 1
O137918	0.012	0	12.141	3	0	32	0	1EY AEP, 1 hour burst, Storm 1
O90392	0	0	12.141	0	0	0	0	
O90396	0	0	12.141	0	0	0	0	
OF76225	0.016	0.016	0.338	0.248	0.04	2.97	0.57	1EY AEP, 2 hour burst, Storm 3
OF76315	0.014	0.014	0.656	0.127	0.05	1.02	0.69	1EY AEP, 3 hour burst, Storm 6
OF76316	0	0	0.436	0	0	0	0	
OF76323	0	0	1.311	0	0	0	0	
OF76327	0	0	19.113	0	0	0	0	
OF76345	0	0	1.305	0	0	0	0	
OF76352	0	0	0	0	0	0	0	
OF76354	0.002	0.002	0.332	0.266	0.01	3.19	0.38	1EY AEP, 2 hour burst, Storm 9
OF76357	0	0	0	0	0	0	0	
OF76359	0.042	0.042	0.35	0.174	0.08	2.09	0.86	1EY AEP, 1 hour burst, Storm 1
OF76363	0	0	0	0	0	0	0	
OF76364	0	0	0.369	0	0	0	0	
OF76369	0	0	19.201	0	0	0	0	
OF76373	0	0	1.322	0	0	0	0	
OF76375	0	0	0	0	0	0	0	
OF76377	0	0	0	0	0	0	0	
OF76384	0.013	0.013	19.15	0.003	0	32	0.13	1EY AEP, 3 hour burst, Storm 7
OF76391	0	0	1.379	0	0	0	0	
OF76405	0.029	0.029	0.393	0.294	0.06	3.53	0.85	1EY AEP, 3 hour burst, Storm 6
OF76407	0.012	0.012	0.261	0.294	0.03	3.53	0.5	1EY AEP, 2 hour burst, Storm 4
OF76410	0	0	19.24	0	0	0	0	
OF76413	0	0	0	0	0	0	0	
OF76415	0	0	0	0	0	0	0	
OF76418	0	0	1.329	0	0	0	0	
OF76420	0	0	0.589	0	0	0	0	
OF76424	0	0	0	0	0	0	0	
OF76426	0	0	19.114	0	0	0	0	
OF76429	0	0	0.225	0	0	0	0	
OF76432	0	0	19.225	0	0	0	0	
OF76434	0	0	0	0	0	0	0	
OF76436	0	0	0	0	0	0	0	
OF76444	0	0	19.201	0	0	0	0	
OF76451	0	0	0.608	0	0	0	0	
W-B1-01	0	0.009	0.14	0.074	0.02	0.89	0.32	1EY AEP, 2 hour burst, Storm 3
W-B1-02	0	0.006	0.157	0.069	0.01	0.83	0.19	1EY AEP, 2 hour burst, Storm 3
W-B1-03	0	0.005	0.123	0.071	0.01	0.86	0.17	1EY AEP, 2 hour burst, Storm 3
W-B1-04	0	0.001	0.163	0.248	0	2.97	0	1EY AEP, 2 hour burst, Storm 9
W-B1-05	0	0.001	0.101	0.248	0	2.97	0	1EY AEP, 9 hour burst, Storm 6
W-B2-01	0.005	0	12.141	3	0	32	0	1EY AEP, 1 hour burst, Storm 1
W-B3-01	0	0.057	0.414	0.41	0.06	4.92	0.63	1EY AEP, 15 min burst, Storm 1
W-B4-01	0	0.038	0.229	0.533	0.04	6.4	0.43	1EY AEP, 15 min burst, Storm 1
W-B4-02	0	0.048	0.375	0.533	0.06	6.4	0.68	1EY AEP, 15 min burst, Storm 1
W-B4-01	0.006	0	12.141	3	0	32	0	1EY AEP, 1 hour burst, Storm 1
W-B5-01	0	0.002	0.354	0.055	0.01	0.66	0.13	1EY AEP, 2 hour burst, Storm 9
W-B5-02	0	0.002	0.312	0.055	0.01	0.66	0.09	1EY AEP, 2 hour burst, Storm 9
W-B5-03	0	0	0.512	0	0	0	0	
W-B5-04	0.044	0.044	0.296	0.224	0.07	2.69	0.76	1EY AEP, 1 hour burst, Storm 1
W-B5-05	0	0.003	0.378	0.266	0.01	3.19	0.26	1EY AEP, 2 hour burst, Storm 9
W-B5-06 07	0	0.025	0.411	0.218	0.05	2.62	0.65	1EY AEP, 2 hour burst, Storm 9
W-B5-08	0	0.009	0.242	0.218	0.02	2.62	0.27	1EY AEP, 2 hour burst, Storm 9
W-B5-09 10	0	0.01	0.367	0.153	0.02	1.83	0.36	1EY AEP, 2 hour burst, Storm 9
W-B5-11	0	0	0.232	0	0	0	0	
W-B5-12	0	0.001	0.389	0.027	0.01	0.32	0.4	1EY AEP, 2 hour burst, Storm 2
W-B5-13A	0.055	0.054	0.172	0.419	0.07	5.03	0.53	1EY AEP, 2 hour burst, Storm 3
W-B5-13B	0.001	0.007	0.226	0.419	0.04	5.03	1.72	1EY AEP, 9 hour burst, Storm 6
W-B5-16	0	0	0.333	0	0	0	0	
W-B5-CULV14 15	0	0.015	0.357	0.124	0.03	1.49	0.45	1EY AEP, 2 hour burst, Storm 9
W-B5-01	0.009	0	12.141	3	0	32	0	1EY AEP, 3 hour burst, Storm 6
W-B6-01	0	0	0.142	0	0	0	0	
W-B7-02	0	0.031	0.478	0.354	0.04	4.25	0.47	1EY AEP, 1 hour burst, Storm 9
W-B7-01	0	0	12.141	0	0	0	0	
W-EXT02	0.014	0.014	0.105	0.095	0.03	1.14	0.45	1EY AEP, 3 hour burst, Storm 6
W-EXT03	0	0	0.379	0	0	0	0	
W-EXT04	0.013	0.013	0.213	0.13	0.03	1.56	0.44	1EY AEP, 3 hour burst, Storm 6
W-S1	0	0	0.385	0	0	0	0	

DETENTION BASIN DETAILS

Name	Max WL	MaxVol	Max Q Total	Max Q Low Level	Max Q High Level
WEST-B1	66.25	26.5	0	0	0
WEST-B2	62.3	78.6	0.014	0	0.014
WEST-B3	62.91	79.4	0	0	0
WEST-B4	59.53	77.4	0.043	0.02	0.023
WEST-B6	58	0	0	0	0
WEST-B5	53.92	55.4	0.028	0	0.028
WEST-B7	51.85	181.3	0	0	0

Run Log for 12546218 AlbanyMotorPark west run at 14:33:26 on 14/7/2021 using version 2020.036

The maximum flow in these overflow routes is unsafe: OF76444, OF76410, OF76407, OF76405, OF76377, OF76354, W-B4-01, W-B3-01, OF76316, W-B7-02, W-B5-13B, W-B5-13A, W-B5-16, W-B5-

Stage 1A (WEST) DRAINS Results							
DRAINS results prepared from Version 2020.036							
10% AEP							
PIT / NODE DETAILS				Version 8			
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
DUMMY-SCALE2	10		0				
DUMMY-SCALE1	8		0				
W1-B1-01-US	69		0				
W-B1-02-US	68.65		0				
W-B1-03-US	68.65		0				
W-B1-04-US	67		0				
W-B1-05-US	66.64		0				
W-B4-01-US	62		0				
W-B4-02-US	68.5		0				
W-B5-CULV1-HW	56.6		0.028			0.4	0 None
W-B5-CULV1-DS	56.31		0				
W-B5-CULV2-HW	56.3		0.314			0.2	0 None
W-B5-CULV2-DS	55.59		0				
W-B5-CULV3-HW	55.19		0.29			0.31	0 None
W-B5-CULV3-DS	54.53		0.032				
W-B5-CULV4-HW	56.98		0.006			1.02	0 None
W-B5-CULV4-DS	56.55		0				
W-B5-CULV5-HW	55.39		0.012			1.11	0 None
W-B5-CULV5-DS	54.47		0				
W-B7-CULV2-HW	55.92		0			1.08	0 None
W-B7-CULV2-DS	55.42		0				
W-B5-CULV6-HW	52.37		0.074			0.63	0 None
N87219	52.36		0				
W-B1-CULV1-HW	68.31		0.026			0.69	0 None
W1-01-DS	67.92		0.087				
N87159	65.27		0				
N87076	64.13		0				
N87168	61.33		0				
W-EXT02-US	61.24		0.093				
W-EXT	60.69		0.371				
W-EXT-CULV1-HW	59.64		0.372			0.86	0 None
W-EXT-CULV1-DS	59.19		0				
N87207	61.73		0				
N87255	61.07		0				
W-EXT-HW	64.63		0.26			0.37	0 None
N87181	58.28		0				
W-B5-03-DS	57.16		0.038				
W-B5-03-US	62		0				
W-B5-06-US	63.5		0				
W-B5-01-US	59		0				
W-B5-02-US	57.5		0				
W-B5-05-US	58		0				
W-B5-08-US	56		0				
W-B5-09-US	58		0				
W-B5-11-US	58		0				
W-B5-12-US	57.5		0				
N87237	57.26		0				
N87238	57.1		0				
W-B6-01-US	59.2		0				
N87225	52.82		0				
N87218	52.52		0				
W-B5-16-US	56.5		0				
W-B5-CULV14-US	59.2		0				
W-B7-CULV1-HW	52.36		0.379			0.64	0 None
N87244	49.39		0				
N87245	49.17		0				
W-B7-02-US	62.5		0				
HW12	53.44		0.317			0.56	0 None
N87149	51.93		0				
HW13	47.42		0.239			0.58	0 None
N87150	46.81		0				
W-B3-01-US	67.2		0				
S1 US	57.5		0				
SUB-CATCHMENT DETAILS							
Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm
W-B5-CULV1-CAT	0.04	0	0.04	0	0	2.63	1.28 10% AEP, 10 min burst, Storm 5
W-B5-CULV2-CAT	0.035	0	0.035	0	0	3.48	1.69 10% AEP, 10 min burst, Storm 7
W-B5-CULV3-CAT	0.169	0	0.169	0	0	2.76	1.34 10% AEP, 10 min burst, Storm 5
W-B5-CULV3-DS-CAT	0.053	0	0.053	0	0	2.14	1.04 10% AEP, 10 min burst, Storm 4
W-B5-CULV4-CAT	0.007	0	0.007	0	0	1.56	0 10% AEP, 10 min burst, Storm 3
W-B5-CULV5-CAT	0.009	0	0.009	0	0	2.35	1.14 10% AEP, 10 min burst, Storm 5
W-B5-CULV6-CAT	0.118	0	0.118	0	0	2.23	1.09 10% AEP, 10 min burst, Storm 5
W-B1-03-CAT	0.044	0	0.044	0	0	2.02	0.99 10% AEP, 10 min burst, Storm 4
W-B1-01-CAT	0.132	0	0.132	0	0	2.82	1.37 10% AEP, 10 min burst, Storm 5
WEST-B1-CAT	0.103	0	0.103	0	0	4.75	2.31 10% AEP, 10 min burst, Storm 3
WEST-B2-CAT	0.269	0.269	0	3	0	0	0 10% AEP, 10 min burst, Storm 1
W-EXT-CAT	0.043	0	0.043	0	0	2.06	0 10% AEP, 10 min burst, Storm 3
W-EXT04-CAT	0.029	0	0.029	0	0	1.72	0.84 10% AEP, 10 min burst, Storm 9
WEST-B3-CAT	0.175	0	0.175	0	0	6.04	2.94 10% AEP, 10 min burst, Storm 9
CulvW_ext	0.142	0	0.142	5	0	75	2 10% AEP, 3 hour burst, Storm 6
WEST-B4-CAT	0.335	0.322	0.013	3.42	0	7.95	0 10% AEP, 10 min burst, Storm 4
W-B5-03-CAT	0.013	0	0.013	0	0	2.12	0 10% AEP, 10 min burst, Storm 3
WEST-B6-CAT	0.124	0	0.124	0	0	2.81	1.37 10% AEP, 10 min burst, Storm 9
WEST-B5-CAT	0.073	0	0.073	0	0	2.88	1.4 10% AEP, 10 min burst, Storm 9
W-B7-01-CAT	0.007	0	0.007	0	0	2.63	0 10% AEP, 10 min burst, Storm 6
WEST-B7-CAT	0.225	0	0.225	0	0	3.45	1.68 10% AEP, 10 min burst, Storm 5
S1 catch	0.27	0	0.27	0	0	39.9	0 10% AEP, 3 hour burst, Storm 2
PIPE DETAILS							
Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm		
DUMMY-SCALE	0	0	10	8	10% AEP, 10 min burst, Storm 5		
W-B5-CULV1	0.025	0.57	56.603	56.313	10% AEP, 15 min burst, Storm 6		
W-B5-CULV2	0.209	2.98	56.12	55.63	10% AEP, 30 min burst, Storm 5		
W-B5-CULV3	0.249	2.03	55.046	54.684	10% AEP, 30 min burst, Storm 5		
W-B5-CULV4	0.004	0.64	56.982	56.545	10% AEP, 2 hour burst, Storm 3		
W-B5-CULV5	0.007	0.61	55.393	54.465	10% AEP, 10 min burst, Storm 3		
Pipe20528	0	0	55.913	55.416	10% AEP, 10 min burst, Storm 5		
W-B5-CULV6	0.064	0.46	52.365	52.363	10% AEP, 30 min burst, Storm 7		
W-B1-CULV1	0.02	0.58	68.308	67.923	10% AEP, 30 min burst, Storm 5		
Pipe20532	0.091	2.66	65.459	65.27	10% AEP, 9 hour burst, Storm 5		

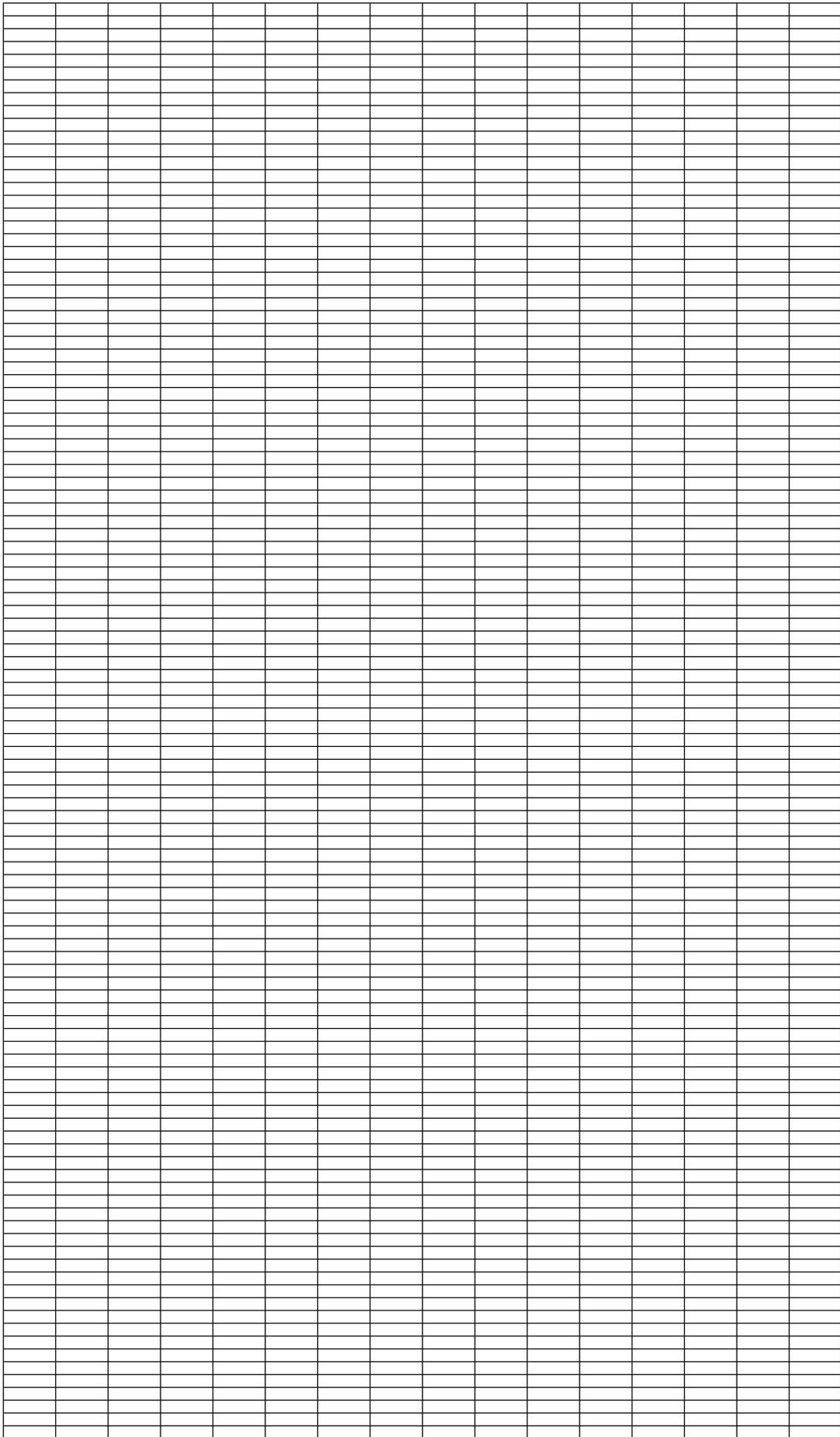
Pipe20533	0.101	3.1	65.27	64.866	10% AEP, 9 hour burst, Storm 5				
Pipe20566	0.029	1.23	61.417	61.333	10% AEP, 45 min burst, Storm 8				
Pipe20567	0.047	1.95	61.333	61.242	10% AEP, 45 min burst, Storm 8				
W-EXT-CULV1	0.215	1.75	59.55	59.324	10% AEP, 3 hour burst, Storm 2				
Pipe20702	0.037	2.08	61.882	61.726	10% AEP, 3 hour burst, Storm 2				
Pipe20716	0.037	2.33	61.726	61.07	10% AEP, 3 hour burst, Storm 2				
W-EXT-CULV	0.141	1.62	64.469	61.242	10% AEP, 3 hour burst, Storm 6				
Pipe20591	0.148	3.44	58.568	58.282	10% AEP, 30 min burst, Storm 7				
Pipe20597	0.173	4.09	58.282	57.64	10% AEP, 30 min burst, Storm 7				
Pipe20785	0	0	57.303	57.263	10% AEP, 10 min burst, Storm 5				
Pipe20790	0	0	57.263	57.105	10% AEP, 15 min burst, Storm 10				
Pipe20745	0.206	2.72	52.993	52.818	10% AEP, 1 hour burst, Storm 6				
Pipe20746	0.242	3.26	52.818	52.535	10% AEP, 1 hour burst, Storm 6				
Pipe20525	0.249	0.78	52.338	52.301	10% AEP, 1 hour burst, Storm 1				
Pipe20821	0.131	2.33	49.533	49.392	10% AEP, 3 hour burst, Storm 2				
Pipe20830	0.15	2.66	49.392	49.17	10% AEP, 3 hour burst, Storm 2				
Pipe20526	0.209	4.16	53.23	52.069	10% AEP, 3 hour burst, Storm 2				
Pipe20527	0.138	2.28	47.259	46.982	10% AEP, 3 hour burst, Storm 2				
CHANNEL DETAILS									
Name	Max Q	Max V			Due to Storm				
	(cu.m/s)	(m/s)							
OVERFLOW ROUTE DETAILS									
Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V		Due to Storm
O134039	0.012	0	12.141	3		0	32	0	10% AEP, 1 hour burst, Storm 6
O134055	0.012	0	12.141	3		0	32	0	10% AEP, 1 hour burst, Storm 6
O137112	0.006	0	12.141	3		0	32	0	10% AEP, 45 min burst, Storm 8
O137116	0.006	0	12.141	3		0	32	0	10% AEP, 45 min burst, Storm 8
O137914	0.006	0	12.141	3		0	32	0	10% AEP, 30 min burst, Storm 7
O137918	0.013	0	12.141	3		0	32	0	10% AEP, 30 min burst, Storm 7
O90392	0.006	0	12.141	3		0	32	0	10% AEP, 3 hour burst, Storm 2
O90396	0.006	0	12.141	3		0	32	0	10% AEP, 3 hour burst, Storm 2
OF76225	0.092	0.092	0.338	0.703		0.13	8.44	1.02	10% AEP, 30 min burst, Storm 5
OF76315	0.204	0.204	0.656	0.533		0.27	4.27	1.4	10% AEP, 3 hour burst, Storm 2
OF76316	0	0	0.436	0		0	0	0	
OF76323	0	0	1.311	0		0	0	0	
OF76327	0.06	0.06	19.113	0.209		0	32	0.33	10% AEP, 45 min burst, Storm 8
OF76345	0.006	0.006	1.305	0.003		0.03	0.35	9.26	10% AEP, 30 min burst, Storm 7
OF76352	0	0	0	0		0	0	0	
OF76354	0.026	0.026	0.332	0.511		0.03	6.13	0.21	10% AEP, 30 min burst, Storm 7
OF76357	0	0	0	0		0	0	0	
OF76359	0.199	0.199	0.35	0.398		0.21	4.77	1.27	10% AEP, 30 min burst, Storm 7
OF76363	0	0	0	0		0	0	0	
OF76364	0.003	0.003	0.369	0.038		0.01	0.45	0.39	10% AEP, 2 hour burst, Storm 2
OF76369	0	0	19.201	0		0	0	0	
OF76373	0	0	1.322	0		0	0	0	
OF76375	0	0	0	0		0	0	0	
OF76377	0	0	0	0		0	0	0	
OF76384	0.204	0.204	19.15	0.017		0.01	32	0.38	10% AEP, 3 hour burst, Storm 2
OF76391	0	0	1.379	0		0	0	0	
OF76405	0.242	0.242	0.393	0.803		0.24	9.64	1.47	10% AEP, 1 hour burst, Storm 6
OF76407	0.155	0.155	0.261	0.803		0.05	9.64	0.08	10% AEP, 6 hour burst, Storm 6
OF76410	0	0	19.24	0		0	0	0	
OF76413	0	0	0	0		0	0	0	
OF76415	0	0	0	0		0	0	0	
OF76418	0	0	1.329	0		0	0	0	
OF76420	0	0	0.589	0		0	0	0	
OF76424	0	0	0	0		0	0	0	
OF76426	0	0	19.114	0		0	0	0	
OF76429	0.148	0.146	0.225	0.423		0.15	5.07	0.86	10% AEP, 3 hour burst, Storm 2
OF76432	0.138	0.138	19.225	0.015		0	32	0.29	10% AEP, 3 hour burst, Storm 2
OF76434	0	0	0	0		0	0	0	
OF76436	0	0	0	0		0	0	0	
OF76444	0	0	19.201	0		0	0	0	
OF76451	0.037	0.037	0.608	0.538		0.09	6.45	1.25	10% AEP, 3 hour burst, Storm 2
W-B1-01	0	0.051	0.14	0.138		0.07	1.66	0.56	10% AEP, 30 min burst, Storm 5
W-B1-02	0	0.029	0.157	0.117		0.04	1.41	0.35	10% AEP, 15 min burst, Storm 6
W-B1-03	0	0.026	0.123	0.158		0.03	1.89	0.17	10% AEP, 15 min burst, Storm 6
W-B1-04	0	0.464	0.163	0.703		1.3	8.44	22.89	10% AEP, 9 hour burst, Storm 5
W-B1-05	0.011	0.721	0.101	0.703		0.31	8.44	0.84	10% AEP, 9 hour burst, Storm 5
W-B2-01	0.006	0	12.141	3		0	32	0	10% AEP, 45 min burst, Storm 8
W-B3-01	0	0.145	0.414	0.747		0.12	8.97	0.88	10% AEP, 10 min burst, Storm 9
W-B4-01	0	0.088	0.229	0.609		0.08	7.31	0.55	10% AEP, 10 min burst, Storm 3
W-B4-02	0	0.11	0.375	0.609		0.11	7.31	0.86	10% AEP, 10 min burst, Storm 9
W-B4-01	0.006	0	12.141	3		0	32	0	10% AEP, 30 min burst, Storm 7
W-B5-01	0	0.022	0.354	0.173		0.03	2.07	0.45	10% AEP, 10 min burst, Storm 3
W-B5-02	0	0.013	0.312	0.173		0.02	2.07	0.38	10% AEP, 10 min burst, Storm 9
W-B5-03	0	0.005	0.512	0.04		0.02	0.48	0.56	10% AEP, 2 hour burst, Storm 2
W-B5-04	0.179	0.188	0.296	0.511		0.18	6.13	1.1	10% AEP, 30 min burst, Storm 7
W-B5-05	0	0.018	0.378	0.498		0.03	5.98	0.47	10% AEP, 10 min burst, Storm 9
W-B5-06 07	0	0.104	0.411	0.395		0.11	4.74	0.92	10% AEP, 10 min burst, Storm 3
W-B5-08	0	0.038	0.242	0.395		0.04	4.74	0.39	10% AEP, 10 min burst, Storm 9
W-B5-09 10	0	0.044	0.367	0.179		0.05	2.15	0.53	10% AEP, 10 min burst, Storm 9
W-B5-11	0	0.004	0.232	0.045		0.02	0.54	0.43	10% AEP, 2 hour burst, Storm 3
W-B5-12	0	0.007	0.389	0.047		0.03	0.56	0.58	10% AEP, 10 min burst, Storm 3
W-B5-13A	0.139	0.359	0.172	0.635		0.31	7.62	1.7	10% AEP, 9 hour burst, Storm 1
W-B5-13B	0.004	0.143	0.226	0.635		0.43	7.62	8.42	10% AEP, 9 hour burst, Storm 1
W-B5-16	0	0.021	0.333	0.635		0.03	7.62	0.38	10% AEP, 10 min burst, Storm 3
W-B5-CULV14 15	0	0.087	0.357	0.365		0.09	4.39	0.76	10% AEP, 10 min burst, Storm 3
W-B5-01	0.012	0	12.141	3		0	32	0	10% AEP, 1 hour burst, Storm 6
W-B6-01	0	0.041	0.142	0.417		0.02	5.01	0.13	10% AEP, 1 hour burst, Storm 4
W-B7-02	0	0.12	0.478	0.801		0.1	9.62	0.77	10% AEP, 10 min burst, Storm 9
W-B7-01	0.006	0	12.141	3		0	32	0	10% AEP, 3 hour burst, Storm 2
W-EXT02	0.172	0.172	0.105	0.242		0.16	2.9	0.84	10% AEP, 3 hour burst, Storm 2
W-EXT03	0.099	0.067	0.379	0.188		0.12	2.25	0.97	10% AEP, 9 hour burst, Storm 5
W-EXT04	0.185	0.186	0.213	0.538		0.16	6.45	0.87	10% AEP, 9 hour burst, Storm 10
W-S1	0	0.265	0.385	0.178		0.25	2.13	1.4	10% AEP, 3 hour burst, Storm 2
DETENTION BASIN DETAILS									
Name	Max WL	MaxVol	Max Q	Max Q	Max Q				
			Total	Low Level	High Level				
WEST-B1	66.7	100.5	0.091	0.091					0
WEST-B2	62.39	121.3	0.106	0.029					0.077
WEST-B3	63.25	167.8	0.037	0.037					0
WEST-B4	59.61	92.9	0.179	0.148					0.031
WEST-B6	58.42	67	0	0					0
WEST-B5	54.13	93.8	0.242	0.206					0.037
WEST-B7	52.3	504.5	0.15	0.131					0.019
Run Log for 12546218 AlbanyMotorPark_west run at 13:48:04 on 14/7/2021 using version 2020.036									

38, W-B5-0 The maximum flow in these overflow routes is unsafe: OF76451, OF76444, OF76429, OF76410, OF76407, OF76405, OF76377, OF76359, OF76354, W-B4-01, W-B3-01, OF76316, OF76315, W-

Stage 1A (WEST) DRAINS Results							
DRAINS results prepared from Version 2020.036							
1% AEP							
PIT / NODE DETAILS				Version 8			
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
DUMMY-SCALE2	10		0				
DUMMY-SCALE1	8		0				
W1-B1-01-US	69		0				
W-B1-02-US	68.65		0				
W-B1-03-US	68.65		0				
W-B1-04-US	67		0				
W-B1-05-US	66.71		0				
W-B4-01-US	62		0				
W-B4-02-US	68.5		0				
W-B5-CULV1-HW	56.72		0.05			0.28	0 None
W-B5-CULV1-DS	56.57		0				
W-B5-CULV2-HW	56.56		0.789			-0.06	0.243 Headwall height/system capacity
W-B5-CULV2-DS	55.66		0.471				
W-B5-CULV3-HW	55.45		0.864			0.05	0 None
W-B5-CULV3-DS	54.61		0.317				
W-B5-CULV4-HW	57.06		0.011			0.94	0 None
W-B5-CULV4-DS	56.57		0				
W-B5-CULV5-HW	55.5		0.032			1	0 None
W-B5-CULV5-DS	54.51		0				
W-B7-CULV2-HW	56.2		0.148			0.8	0 None
W-B7-CULV2-DS	55.51		0				
W-B5-CULV6-HW	52.64		0.129			0.36	0 None
N87219	52.62		0				
W-B1-CULV1-HW	68.4		0.045			0.6	0 None
W1-01-DS	67.98		0.151				
N87159	65.29		0				
N87076	64.14		0.032				
N87168	61.39		0				
W-EXT02-US	61.36		0.252				
W-EXT	60.79		0.912				
W-EXT-CULV1-HW	60.52		1.092			-0.02	0.051 Headwall height/system capacity
W-EXT-CULV1-DS	59.26		0.321				
N87207	61.8		0				
N87255	61.12		0				
W-EXT-HW	65.04		0.694			-0.04	0.176 Headwall height/system capacity
N87181	58.35		0				
W-B5-03-DS	57.25		0.239				
W-B5-03-US	62		0				
W-B5-06-US	63.5		0				
W-B5-01-US	59		0				
W-B5-02-US	57.5		0				
W-B5-05-US	58		0				
W-B5-08-US	56		0				
W-B5-09-US	58		0				
W-B5-11-US	58		0				
W-B5-12-US	57.5		0				
N87237	57.39		0				
N87238	57.19		0				
W-B6-01-US	59.2		0				
N87225	52.93		0				
N87218	52.63		0.134				
W-B5-16-US	56.5		0				
W-B5-CULV14-US	59.2		0				
W-B7-CULV1-HW	52.62		1.016			0.38	0 None
N87244	49.54		0				
N87245	49.27		0.121				
W-B7-02-US	62.5		0				
HW12	54.03		0.745			-0.03	0.107 Headwall height/system capacity
N87149	51.94		0.373				
HW13	48.04		0.805			-0.04	0.153 Headwall height/system capacity
N87150	46.83		0.448				
W-B3-01-US	67.2		0				
S1 US	57.5		0				
SUB-CATCHMENT DETAILS							
Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm
W-B5-CULV1-CAT	0.082	0	0.082	0	0	2.33	1.13 1% AEP, 15 min burst, Storm 8
W-B5-CULV2-CAT	0.074	0	0.074	0	0	2.82	1.37 1% AEP, 10 min burst, Storm 4
W-B5-CULV3-CAT	0.319	0	0.319	0	0	2.45	1.19 1% AEP, 15 min burst, Storm 4
W-B5-CULV3-DS-CAT	0.091	0	0.091	0	0	1.9	0.92 1% AEP, 15 min burst, Storm 4
W-B5-CULV4-CAT	0.018	0	0.018	0	0	1.38	0 1% AEP, 15 min burst, Storm 8
W-B5-CULV5-CAT	0.016	0	0.016	0	0	2.08	1.01 1% AEP, 15 min burst, Storm 4
W-B5-CULV6-CAT	0.215	0	0.215	0	0	1.98	0.96 1% AEP, 15 min burst, Storm 8
W-B1-03-CAT	0.075	0	0.075	0	0	1.79	0.87 1% AEP, 15 min burst, Storm 4
W-B1-01-CAT	0.252	0	0.252	0	0	2.5	1.22 1% AEP, 15 min burst, Storm 4
WEST-B1-CAT	0.211	0	0.211	0	0	3.84	1.87 1% AEP, 10 min burst, Storm 4
WEST-B2-CAT	0.435	0.435	0	2.43	0	0	0 1% AEP, 10 min burst, Storm 4
W-EXT-CAT	0.107	0	0.107	0	0	1.83	0 1% AEP, 15 min burst, Storm 8
W-EXT04-CAT	0.068	0	0.068	0	0	1.53	0.74 1% AEP, 15 min burst, Storm 8
WEST-B3-CAT	0.324	0	0.324	0	0	4.89	2.38 1% AEP, 10 min burst, Storm 4
CulvW_ext	0.479	0	0.479	5	5	75	2 1% AEP, 3 hour burst, Storm 8
WEST-B4-CAT	0.589	0.516	0.082	3.03	0	7.05	0 1% AEP, 15 min burst, Storm 8
W-B5-03-CAT	0.032	0	0.032	0	0	1.88	0 1% AEP, 15 min burst, Storm 8
WEST-B6-CAT	0.281	0	0.281	0	0	2.49	1.22 1% AEP, 15 min burst, Storm 8
WEST-B5-CAT	0.162	0	0.162	0	0	2.55	1.24 1% AEP, 15 min burst, Storm 8
W-B7-01-CAT	0.018	0	0.018	0	0	2.13	0 1% AEP, 10 min burst, Storm 4
WEST-B7-CAT	0.427	0	0.427	0	0	2.79	1.36 1% AEP, 10 min burst, Storm 4
S1 catch	1.641	0	1.641	0	0	19.68	0 1% AEP, 25 min burst, Storm 8
PIPE DETAILS							
Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm		
DUMMY-SCALE	0	0	10	8	1% AEP, 10 min burst, Storm 5		
W-B5-CULV1	0.069	0.71	56.696	56.566	1% AEP, 15 min burst, Storm 8		
W-B5-CULV2	0.286	3.27	56.204	55.668	1% AEP, 15 min burst, Storm 1		
W-B5-CULV3	0.517	2.46	55.197	54.783	1% AEP, 30 min burst, Storm 3		
W-B5-CULV4	0.017	1.24	57.056	56.575	1% AEP, 15 min burst, Storm 8		
W-B5-CULV5	0.033	1.31	55.496	54.507	1% AEP, 15 min burst, Storm 8		
Pipe20528	0.069	2.46	56.107	55.515	1% AEP, 2 hour burst, Storm 10		
W-B5-CULV6	0.163	1.03	52.637	52.624	1% AEP, 15 min burst, Storm 8		
W-B1-CULV1	0.053	0.9	68.389	67.978	1% AEP, 15 min burst, Storm 1		
Pipe20532	0.143	3.23	65.513	65.295	1% AEP, 2 hour burst, Storm 10		

Pipe20533	0.143	3.27	65.295	64.894	1% AEP, 2 hour burst, Storm 10				
Pipe20566	0.097	2.12	61.516	61.388	1% AEP, 15 min burst, Storm 1				
Pipe20567	0.115	2.53	61.388	61.36	1% AEP, 15 min burst, Storm 1				
W-EXT-CULV1	0.418	2.72	60.157	59.416	1% AEP, 2 hour burst, Storm 7				
Pipe20702	0.146	3.12	62.016	61.801	1% AEP, 30 min burst, Storm 5				
Pipe20716	0.146	3.28	61.801	61.145	1% AEP, 30 min burst, Storm 5				
W-EXT-CULV	0.303	2.22	64.851	61.36	1% AEP, 3 hour burst, Storm 8				
Pipe20591	0.334	4.55	58.69	58.351	1% AEP, 15 min burst, Storm 8				
Pipe20597	0.362	4.94	58.351	57.711	1% AEP, 15 min burst, Storm 8				
Pipe20785	0.069	1.89	57.482	57.387	1% AEP, 2 hour burst, Storm 10				
Pipe20790	0.069	1.98	57.387	57.222	1% AEP, 2 hour burst, Storm 10				
Pipe20745	0.542	3.79	53.181	52.933	1% AEP, 30 min burst, Storm 8				
Pipe20746	0.583	4.08	52.933	52.652	1% AEP, 30 min burst, Storm 8				
Pipe20525	0.49	1.54	52.55	52.44	1% AEP, 30 min burst, Storm 8				
Pipe20821	0.506	3.6	49.764	49.539	1% AEP, 2 hour burst, Storm 2				
Pipe20830	0.528	3.75	49.539	49.299	1% AEP, 2 hour burst, Storm 2				
Pipe20526	0.362	4.84	53.309	52.125	1% AEP, 2 hour burst, Storm 7				
Pipe20527	0.346	2.82	47.498	47.124	1% AEP, 1 hour burst, Storm 6				
CHANNEL DETAILS									
Name	Max Q (cu.m/s)	Max V (m/s)			Due to Storm				
OVERFLOW ROUTE DETAILS									
Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DxV	Max Width	Max V		Due to Storm
O134039	0.014	0	12.141	3	0	32	0	1.34	1% AEP, 30 min burst, Storm 8
O134055	0.014	0	12.141	3	0	32	0	1.7	1% AEP, 30 min burst, Storm 8
O137112	0.006	0	12.141	3	0	32	0	0.82	1% AEP, 15 min burst, Storm 1
O137116	0.006	0	12.141	3	0	32	0	1.62	1% AEP, 15 min burst, Storm 1
O137914	0.007	0	12.141	3	0	32	0	0.7	1% AEP, 15 min burst, Storm 8
O137918	0.014	0	12.141	3	0	32	0	0.79	1% AEP, 15 min burst, Storm 8
O90392	0.007	0	12.141	3	0	32	0	0.42	1% AEP, 2 hour burst, Storm 2
O90396	0.007	0	12.141	3	0	32	0	0.72	1% AEP, 2 hour burst, Storm 2
OF76225	0.255	0.255	0.996	0.707	0.24	8.48	0.04	0.81	1% AEP, 15 min burst, Storm 8
OF76315	0.469	0.469	1.729	1.124	0.45	8.99	0.07	0.48	1% AEP, 2 hour burst, Storm 7
OF76316	0.069	0.069	1.286	0.996	0.11	11.96	0.07	0.88	1% AEP, 2 hour burst, Storm 1
OF76323	0	0	1.311	0	0	0	0	0.59	1% AEP, 2 hour burst, Storm 10
OF76327	0.173	0.173	19.113	0.348	0.01	32	0.04	0.71	1% AEP, 15 min burst, Storm 1
OF76345	0.164	0.164	1.305	0.025	0.1	4	0.04	3.93	1% AEP, 15 min burst, Storm 8
OF76352	0	0	0.357	0	0	0	0	0	
OF76354	0.095	0.095	0.979	0.778	0.04	9.34	0.04	0.09	1% AEP, 15 min burst, Storm 9
OF76357	0.243	0.243	0.364	0.042	0.03	10.86	0.03	0.82	1% AEP, 15 min burst, Storm 1
OF76359	0.527	0.527	1.031	0.649	0.38	7.79	0.03	1.62	1% AEP, 15 min burst, Storm 1
OF76363	0	0	0.757	0	0	0	0	0	
OF76364	0.017	0.017	1.089	0.065	0.04	0.78	0.04	0.7	1% AEP, 15 min burst, Storm 8
OF76369	0	0	19.201	0	0	0	0	0	
OF76373	0	0	1.322	0	0	0	0	0	
OF76375	0.051	0.051	0.644	0.017	0.01	6.66	0.01	0.74	1% AEP, 2 hour burst, Storm 7
OF76377	0.107	0.107	0.79	0.021	0.02	7.52	0.02	1.07	1% AEP, 2 hour burst, Storm 7
OF76384	0.469	0.469	19.15	0.028	0.01	32	0.01	0.53	1% AEP, 2 hour burst, Storm 7
OF76391	0.001	0.001	1.379	0.001	0	0.13	0	0	1% AEP, 30 min burst, Storm 8
OF76405	0.583	0.583	1.159	1.064	0.36	12.77	0.36	1.3	1% AEP, 30 min burst, Storm 8
OF76407	0.243	0.243	0.769	1.064	0.05	12.77	0.05	0.06	1% AEP, 9 hour burst, Storm 10
OF76410	0	0	19.24	0	0	0	0	0	
OF76413	0	0	0.455	0	0	0	0	0	
OF76415	0	0	0.464	0	0	0	0	0	
OF76418	0	0	1.329	0	0	0	0	0	
OF76420	0.069	0.069	1.737	0.288	0.13	3.45	0.13	1.43	1% AEP, 2 hour burst, Storm 10
OF76424	0	0	0.526	0	0	0	0	0	
OF76426	0	0	19.114	0	0	0	0	0	
OF76429	0.528	0.517	0.664	1.046	0.32	12.56	0.32	1.18	1% AEP, 2 hour burst, Storm 2
OF76432	0.499	0.499	19.225	0.032	0.02	32	0.02	0.49	1% AEP, 1 hour burst, Storm 6
OF76434	0.153	0.153	0.526	0.029	0.03	9.12	0.03	0.92	1% AEP, 1 hour burst, Storm 6
OF76436	0	0	0.526	0	0	0	0	0	
OF76444	0.176	0.176	19.201	0.684	0.01	32	0.01	0.47	1% AEP, 3 hour burst, Storm 8
OF76451	0.146	0.146	1.792	1.423	0.21	17.07	0.21	1.77	1% AEP, 30 min burst, Storm 5
W-B1-01	0	0.145	0.412	0.201	0.14	2.41	0.14	0.76	1% AEP, 15 min burst, Storm 8
W-B1-02	0	0.073	0.464	0.178	0.07	2.13	0.07	0.39	1% AEP, 15 min burst, Storm 8
W-B1-03	0	0.068	0.363	0.252	0.05	3.03	0.05	0.28	1% AEP, 15 min burst, Storm 8
W-B1-04	0	0.473	0.48	0.707	1.17	8.48	1.17	19.49	1% AEP, 9 hour burst, Storm 2
W-B1-05	0.012	0.725	0.298	0.707	0.29	8.48	0.29	0.79	1% AEP, 9 hour burst, Storm 2
W-B2-01	0.006	0	12.141	3	0	32	0	0	1% AEP, 15 min burst, Storm 1
W-B3-01	0	0.269	1.221	0.808	0.18	9.7	0.18	1.04	1% AEP, 10 min burst, Storm 4
W-B4-01	0	0.183	0.676	0.684	0.13	8.21	0.13	0.72	1% AEP, 10 min burst, Storm 6
W-B4-02	0	0.22	1.104	0.684	0.18	8.21	0.18	1.07	1% AEP, 10 min burst, Storm 10
W-B4-01	0.007	0	12.141	3	0	32	0	0	1% AEP, 15 min burst, Storm 8
W-B5-01	0	0.052	1.044	0.29	0.06	3.47	0.06	0.61	1% AEP, 15 min burst, Storm 8
W-B5-02	0	0.03	0.92	0.29	0.04	3.47	0.04	0.48	1% AEP, 15 min burst, Storm 8
W-B5-03	0	0.029	1.511	0.075	0.07	0.89	0.07	0.88	1% AEP, 15 min burst, Storm 1
W-B5-04	0.551	0.574	0.872	0.763	0.37	9.15	0.37	1.45	1% AEP, 15 min burst, Storm 8
W-B5-05	0	0.04	1.113	0.763	0.05	9.15	0.05	0.59	1% AEP, 15 min burst, Storm 8
W-B5-06 07	0	0.235	1.213	0.649	0.19	7.79	0.19	1.19	1% AEP, 15 min burst, Storm 8
W-B5-08	0	0.082	0.714	0.649	0.04	7.79	0.04	0.42	1% AEP, 15 min burst, Storm 8
W-B5-09 10	0	0.093	1.083	0.291	0.09	3.49	0.09	0.72	1% AEP, 10 min burst, Storm 4
W-B5-11	0	0.018	0.685	0.077	0.04	0.92	0.04	0.59	1% AEP, 15 min burst, Storm 8
W-B5-12	0	0.016	1.147	0.063	0.04	0.75	0.04	0.73	1% AEP, 15 min burst, Storm 8
W-B5-13A	0.548	0.552	0.506	0.753	0.3	9.03	0.3	0.96	1% AEP, 30 min burst, Storm 8
W-B5-13B	0.005	0.18	0.666	0.753	0.18	9.03	0.18	1.24	1% AEP, 9 hour burst, Storm 5
W-B5-16	0	0.054	0.982	0.753	0.06	9.03	0.06	0.55	1% AEP, 10 min burst, Storm 4
W-B5-CULV14 15	0	0.196	1.054	0.643	0.16	7.72	0.16	1.1	1% AEP, 10 min burst, Storm 9
W-B5-01	0.014	0	12.141	3	0	32	0	0	1% AEP, 30 min burst, Storm 8
W-B6-01	0	0.159	0.418	0.569	0.07	6.82	0.07	0.37	1% AEP, 15 min burst, Storm 8
W-B7-02	0	0.24	1.408	0.94	0.16	11.28	0.16	0.97	1% AEP, 10 min burst, Storm 4
W-B7-01	0.007	0	12.141	3	0	32	0	0	1% AEP, 2 hour burst, Storm 2
W-EXT02	0.521	0.524	0.31	0.363	0.31	4.36	0.31	1.1	1% AEP, 30 min burst, Storm 8
W-EXT03	0.143	0.149	1.117	0.293	0.17	3.52	0.17	1.23	1% AEP, 2 hour burst, Storm 10
W-EXT04	0.59	0.463	0.629	1.423	0.34	17.07	0.34	1.16	1% AEP, 1 hour burst, Storm 7
W-S1	0	1.604	1.134	0.341	0.78	4.1	0.78	2.3	1% AEP, 20 min burst, Storm 4
DETENTION BASIN DETAILS									
Name	Max WL	MaxVol	Max Q Total	Max Q Low Level	Max Q High Level				
WEST-B1	66.71	101.3	0.143	0.143	0				
WEST-B2	62.43	143.9	0.289	0.097	0.192				
WEST-B3	63.31	186.2	0.146	0.146	0				
WEST-B4	59.68	109.3	0.526	0.334	0.192				
WEST-B6	58.57	106.2	0.069	0.069	0				
WEST-B5	54.25	118.1	0.584	0.542	0.041				
WEST-B7	52.44	628.9	0.528	0.506	0.022				
Run Log for 12546218 AlbanyMotorPark_west run at 15:24:01 on 14/7/2021 using version 2020.036									

B7-02, W-B5 The maximum flow in these overflow routes is unsafe: W-S1, OF76451, OF76444, OF76429, OF76410, OF76407, OF76405, OF76359, OF76354, W-B4-01, OF76327, W-B3-01, OF76316, OF76315, W-B





Stage 1B (EAST) DRAINS Input Data

PIT / NODE DETAILS		Version 15		Ponding		Pressure		Surface		Max Pond		Base		Blocking		x		y		Bolt-down		Part Full		Inflow		Pit is		Internal		Inflow is		Minor Safe		Major Safe				
Name	Type	Family	Size	Volume (cu.m)	Change	Coeff. Ku	Change	Depth (m)	Depth (m)	Depth (m)	Depth (m)	Inflow (cu.m/s)	Factor	x	y	id	id	Shock	Loss	Hydrograph	Pit is	Width (mm)	Flow is	Misaligned (m)	Minor Safe Pond Deg (m)	Major Safe Pond Depth (m)												
E-82-02-US	Node							60.5						0	568175	6133948		97325		No																		
dummys1	Node							9						0	567155	6133587		97367		No																		
N57	Node							58						0	568106	6133961		97505		No																		
N58	Node							69						0	569093	6133965		97516		No																		
E-82-01-US	Node							63.5						0	568158	6134105		97469		No																		
E-85-CULV1-HW	Headwall							68	0.5					0	568616	6133924		97687		No																		
N6143	Node							67.5						0	568663	6133920		1336204		No																		
N302	Node							64.5						0	568673	6133907		99131		No																		
DUMMY-SCALE2	Node							10.5						0	568871	6134218		97701		No																		
DUMMY-SCALE1	Node							8						0	568834	6134070		97702		No																		
E-85-01-US	Node							71						0	568522	6133990		97795		No																		
E-85-02-US	Node							72.5						0	568572	6134258		97815		No																		
E-87-CULV2-HW	Headwall							72	0.5					0	568460	6134257		97929		No																		
E-87-CULV2-DS	Node							72						0	568452	6134269		97831		No																		
E-87-04-US	Node							73						0	568445	6134203		97846		No																		
E-87-05-US	Node							73						0	568460	6134258		97849		No																		
E-89-CULV1-HW	Headwall							68.5	0.5					0	568636	6134618		97880		No																		
E-89-CULV1-DS	Node							67.5						0	568622	6134619		97882		No																		
E-89-07-US	Node							73						0	568623	6134277		97904		No																		
E-89-08-US	Node							68.5						0	568636	6134754		97910		No																		
E-89-05-US	Node							71						0	568577	6134468		97923		No																		
E-89-06-US	Node							68						0	568622	6134736		97926		No																		
E-89-CULV2-HW	Headwall							69	0.5					0	568493	6134029		97939		No																		
E-89-CULV2-DS	Node							64						0	568547	6134645		97960		No																		
E-89-03-US	Node							71						0	568560	6134465		97945		No																		
E-89-04-US	Node							67						0	568596	6134741		97951		No																		
E-89-01-US	Node							69.5						0	568513	6134498		97977		No																		
E-89-02-US	Node							65.5						0	568566	6134737		97985		No																		
N308	Node							61.5						0	568167	6134263		99152		No																		
N297	Node							57						0	568128	6134265		99115		No																		
E-87-07-US	Node							70						0	568465	6134420		98259		No																		
N296	Node							62.25						0	568511	6134661		99112		No																		
N305	Node							59.5						0	567984	6133886		99135		No																		
N304	Node							53.5						0	567968	6133945		99134		No																		
N6149	Node							66						0	568245	6134293		1337247		No																		
N298	Node							63						0	568227	6134274		99116		No																		
N367	Node							62.5						0	568520	6134829		100059		No																		
N294	Node							61						0	568465	6134822		99109		No																		
E-89-CULV3-HW	Headwall							62	0.5					0	568491	6134668		98030		No																		
E-89-CULV3-DS	Node							60						0	568450	6134694		98032		No																		
E-81-01-US	Node							63						0	568467	6134664		98042		No																		
E-81-02-US	Node							63.5						0	568362	6134548		98052		No																		
E-81-03-US	Node							65.5						0	568569	6134752		98066		No																		
E-81-02-CULV1-HW	Headwall							64	0.5					0	568607	6134686		98068		No																		
E-81-02-CULV1-DS	Node							64						0	568579	6134834		98071		No																		
E-81-04-US	Node							67						0	568596	6134759		98119		No																		
E-81-05-US	Node							68						0	568623	6134757		98121		No																		
E-86-01-US	Node							66.5						0	568308	6134064		98149		No																		
E-86-02-US	Node							69.5						0	568325	6134226		98154		No																		
E-86-03-US	Node							63.5						0	568373	6134534		98162		No		</																

P13783	EAST-B3	N61629	2	69.3	69.233	3.35	Concrete, under roads, 0.5% min/s	600	600	0.013	New/Feed	EAST-B3	0
P13826	EAST-B5	N61643	1.5	65.3	65.24	6.5	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	EAST-B5	0
P13854	EAST-B7	N61649	2	64.3	64.17	6.5	Concrete, under roads, 0.5% min/s	600	600	0.013	New/Feed	EAST-B7	0
P21	N57	N58	8.5	56.255	56	3	Concrete, under roads, 1% min/s	450	450	0.013	New	N57	0
P3176	E-B7-CULV1-HW	P11448	5	68	66.91	2.1	Concrete, under roads, 1% min/s	450	450	0.013	New/Feed	E-B7-CUL	0
Pipe10	EAST-B2	N57	1.5	56.3	56.255	1.5	Concrete, under roads, 1% min/s	450	450	0.013	New/Feed	EAST-B2	0
Pipe122	E-B10-CULV1-HW	E-B10-CU	29.4	64.41	62.91	5.1	Concrete, under roads, 1% min/s	450	450	0.013	New/Feed	E-B10-CU	0
Pipe177	N61629	N299	58	69.233	68	2.13	Concrete, under roads, 0.5% min/s	600	600	0.013	New/Feed	N61629	0
Pipe178	EAST-B4	N57	70.4	70	0.4	Concrete, under roads, 0.5% min/s	600	600	0.013	New/Feed	EAST-B4	0	
Pipe179	N61643	N302	18.5	65.24	64.5	4	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	N61643	0
Pipe182	N61649	N296	18	64.17	63	6.5	Concrete, under roads, 0.5% min/s	600	600	0.013	New/Feed	N61649	0
Pipe183	N305	N297	39	60.155	59.1	12.23	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	N305	0
Pipe184	EAST-B8	E-B7-07-U	10	70.05	70	0.5	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	EAST-B8	0
Pipe185	N61649	N296	15	62.3	62.225	0.2	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	EAST-B9	0
Pipe186	N307	N294	48	61.268	60.5	1.5	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	N307	0
Pipe213	EAST-B1	N305	1.5	57	56.915	5.67	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	EAST-B1	0
Pipe220	N305	N304	60	56.915	53.5	5.69	Concrete, under roads, 0.5% min/s	450	450	0.013	New	N305	0
Pipe283	EAST-B6	N306	2	60.4	60.155	12.23	Concrete, under roads, 0.5% min/s	600	600	0.013	New/Feed	EAST-B6	0
Pipe2927	P11296	EAST-B4	95.2	71.4	71	0.42	Concrete, under roads, 0.5% min/s	375	375	0.013	New/Feed	P11296	0
Pipe349	EAST-B10	N367	2	61.3	61.268	1.6	Concrete, under roads, 0.5% min/s	600	600	0.013	New/Feed	EAST-B10	0
Pipe353	HW1478	N59	20	48.41	47.41	5	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	HW1478	0
Pipe564	HW1479	N38873	15	51.91	50.91	6.67	Concrete, under roads, 0.5% min/s	900	900	0.013	New/Feed	HW1479	0
Pipe568	HW1480	N38880	25	56.41	55.41	4	Concrete, under roads, 0.5% min/s	450	450	0.013	New/Feed	HW1480	0

DETAILS OF SERVICES CROSSING PIPES

Pipe	Chg	Bottom Elev (m)	Height of Chg (m)	Bottom Elev (m)	Height of Chg (m)	Bottom Elev (m)	Height of S/c etc (m)
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CHANNEL DETAILS

Name	From	To	Type	Length (m)	US/IL (m)	D/S IL (m)	Slope (%)	Base Width (m)	L.B. Slope (1:n)	R.B. Slope (1:n)	Manning	Depth (m)	Roofed
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OVERFLOW ROUTE DETAILS

Name	From	To	Travel Time (min)	Spill Level (m)	Crest Length (m)	Weir Coeff	Cross Section	Safe Depth (m)	Safe Depth (m)	Safe Bed Slope (%)	D/S Area Contributing (%)	id	US/IL (m)	D/S IL (m)	Length (m)	
E-B10-01	E-B10-01-US	EAST-B10	4.4	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.55	16.11	88059	63	62	182.6
E-B10-02	E-B10-02-US	EAST-B10	7.8	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.49	69.04	88055	63.5	62	306.3
E-B10-03A	E-B10-03-US	E-B10-CU	0.9	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	3.09	100	99062	65.5	62.91	83.7
E-B10-03B	E-B10-CULV1-DS	E-B10-CU	0.7	0.2	0.1	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.69	4.95	99059	62.91	62	54
E-B10-04	E-B10-04-US	E-B10-CU	0.9	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	2.44	49	98124	67	64.41	82
E-B10-05	E-B10-05-US	E-B10-CU	0.7	0.2	0.1	1	Swate with 1.4 sideslopes	0.45	0.3	1	3.18	51	98125	68	64.41	94.3
E-B1-01	E-B1-01-US	N294	2.1	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.51	100	98401	58.5	58	83
E-B1-02A	E-B1-02-US	E-B1-CUL	3.2	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.54	100	98420	60.5	59.8	130.5
E-B1-02B	E-B1-CULV1-DS	EAST-B1	0.3	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	2.78	4.7	98819	59.8	59	28.8
E-B1-03A	E-B1-03-US	EAST-B3	1.8	0.4	0.3	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.51	100	98463	68.5	65.3	142.8
E-B1-03B	E-B1-03-SPLIT	EAST-B1	3.9	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	2.08	66.3	98467	65.5	59	312.1
E-B1-04	E-B1-04-US	E-B1-04-C	3.5	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	0.54	100	98459	69.5	68.5	184.8
E-B1-04-CONNECT	E-B1-04-US	E-B1-04-C	3.5	0.3	0.2	1	Dummy CF	0.3	0.3	0.6	0.25	0	98876	68.5	65.3	82.4
E-B2-01	E-B2-01-US	EAST-B2	0.4	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	4.23	50.08	97461	63.5	57.5	142
E-B2-02	E-B2-02-US	EAST-B2	0.7	0.4	0.3	1	Swate with 1.8 sideslopes	0.3	0.2	1	5.28	45.25	98482	60.5	57.5	56.8
E-B3-01	E-B3-01-US	EAST-B3	1.9	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.23	25.59	98348	70.5	70.5	118.7
E-B3-02	E-B3-02-US	EAST-B3	2.8	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.33	47.07	98344	70.5	70	112.9
E-B4-01	E-B4-01-US	P11296	2.2	0.3	0.2	1	K300, 0.4m deep, wall on one side	0.3	0.2	0.6	0.5	100	98369	72.6	71.8	150.2
E-B4-02	E-B4-02-US	E-B4-02-C	3.1	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	0.9	100	98365	73	71.1	211.6
E-B5-01	E-B5-01-US	E-B5-CUL	1.4	0.4	0.3	1	Swate with 1.4 sideslopes	0.45	0.3	1	2.56	15.7	97787	67.1	66.91	159.6
E-B5-02	E-B5-02-US	E-B5-CUL	4.2	0.4	0.3	1	Swate with 1.4 sideslopes	0.45	0.3	1	1.49	84.3	97818	72.5	66.91	375.5
E-B6-01	E-B6-01-US	EAST-B6	1.3	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	3.67	19.7	98156	66.5	61	142
E-B6-02	E-B6-02-US	EAST-B6	1.6	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	5.3	11.25	98164	69.5	61	158.6
E-B6-03	E-B6-03-US	EAST-B6	6.2	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.8	49.41	98188	63.5	61	310.6
E-B7-01	E-B7-01-US	P18	1.3	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	0.67	100	98209	69.5	69	74.8
E-B7-02	E-B7-02-US	E-B7-02-D	3.6	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.51	100	98229	70.5	69.5	103.6
E-B7-03	E-B7-03-US	E-B7-03-C	2.1	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.16	100	98233	72	70.5	129.3
E-B7-04	E-B7-04-US	E-B7-CUL	0.9	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	0.97	70.93	97852	73	72.41	81
E-B7-05	E-B7-05-US	E-B7-CUL	1.3	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	1.92	29.07	97866	73	72.41	30.7
E-B7-06	E-B7-CULV2-DS	E-B7-CUL	1.3	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	2.67	32.5	98251	72	68	149.8
E-B7-07	E-B7-07-US	E-B7-CUL	1.4	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	1.57	67.5	98258	70	68	127.4
E-B7-08	E-B7-08-US	P11448	1.7	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	2.66	49.8	98290	62	62	154
E-B7-09	E-B7-09-US	P11448	2.1	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.45	50.2	98296	70	67.91	144.6
E-B7-10A	E-B7-10-US	N511	1.6	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.97	100	102028	69.5	67	126.8
E-B7-10B	E-B7-10-US	N511	1.7	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	1.12	100	102051	67	65.5	133.8
E-B7-11	E-B7-CULV1-DS	E-B7-11-C	10.1	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	0.01	100	98325	65.5	65.1	73.1
E-B8-01A	E-B8-01A-US	EAST-B8	2.3	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	0.56	41.89	98986	71.2	70.5	126.1
E-B8-01B	E-B8-01B-US	EAST-B8	1.1	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	2.08	31.15	99020	73	70.5	167
E-B9-01	E-B9-01-US	E-B9-CUL	1.4	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	3.6	68.8	97981	69.5	64	152.7
E-B9-02	E-B9-02-US	E-B9-CUL	1.4	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.57	31.2	97987	65.5	64	95.6
E-B9-03	E-B9-03-US	E-B9-CUL	1.6	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.69	49.8	97987	67.1	66.91	167
E-B9-04	E-B9-04-US	E-B9-CUL	1.5	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	1.83	39.1	97956	67	64.91	113.2
E-B9-05	E-B9-05-US	E-B9-CUL	1.4	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	2.78	64.3	97929	71	66.41	165.1
E-B9-06	E-B9-06-US	E-B9-CUL	1.4	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	1.57	67.5	97933	71	66.41	165.1
E-B9-07	E-B9-07-US	E-B9-CUL	3.7	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	1.64	75.8	97937	73	67.91	341.3
E-B9-08	E-B9-08-US	E-B9-CUL	1.6	0.3	0.2	1	Swate with 1.4 sideslopes	0.45	0.3	1	0.94	24.2	97909	68.5	67.91	115.5
OF139	P18	EAST-B6	1.7	0.3	0.2	1	Dummy CF	0.05	0	0.6	2.54	0	98548	69.5	61	114.4
OF144	E-B7-03-DS	E-B7-03-C	0.4	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	2.83	100	98993	70	69.5	35.3
OF153	E-B7-02-DS	N266	0.3	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	6.01	50	98614	69.5	66.75	41.6
OF159	E-B7-CULV3-DS	N266	0.5	0.3	0.2	1	Swate with 1.8 sideslopes	0.3	0.2	1	0.94	50	98625	67	66.75	26.7
OF165	N266	EAST-B7	0.3	0.3	0.2	1	Dummy CF	0.3	0.3	0.6	0.25	0	98649	66.75	65	40
OF18	N58	N59	0.8	0.3	0.2	1	Dummy CF	0.3	0.3	0.6	0.05	0	97517	56	51.5	111.2
OF22	EAST-B2	N58	0.1	0.1	0.1	5	1.45 m wide pathway	0.3	0.15	0.4	17.5	0	97566	57.75	56	10
OF26	E-B4-02-DS	EAST-B4	0.1	0.3	0.3	1	Dummy CF	0.3	0.3	0.6	10	100	98909	71.1	71	1
OF244	E-B7-11-DS	EAST-B7	0.1	0.3	0.3	0.6	10	0	0	0	0	98967	65.1	65	1	
OF262	P11296	EAST-B4	1.4	0.3	0.3	0.6	10	0	0	0	0	99025	72.2	71	90	
OF268																

Stage 1B (EAST) DRAINS Results							
DRAINS results prepared from Version 2020.036							
1EY							
PIT / NODE DETAILS							
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Version 8 Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
E-B2-02-US	60.5		0				
N57	56.3		0				
N58	56		0				
E-B2-01-US	63.5		0				
E-B5-CULV1-HW	67.48		0.22			0.52	0 Headwall height/system capacity
N61643	65.3		0				
N302	64.61		0				
DUMMY-SCALE2	10		0				
DUMMY-SCALE1	8		0				
E-B5-01-US	71		0				
E-B5-02-US	72.5		0				
E-B7-CULV2-HW	72.69		0.041			0.81	0 Headwall height/system capacity
E-B7-CULV2-DS	72.14		0				
E-B7-04-US	73		0				
E-B7-05-US	73		0				
E-B9-CULV1-HW	67.41		0			1.09	0 Headwall height/system capacity
E-B9-CULV1-DS	66.47		0.014				
E-B9-07-US	73		0				
E-B9-08-US	68.5		0				
E-B9-05-US	71		0				
E-B9-06-US	68		0				
E-B9-CULV2-HW	65.01		0.016			0.99	0 Headwall height/system capacity
E-B9-CULV2-DS	64.1		0.041				
E-B9-03-US	71		0				
E-B9-04-US	67		0				
E-B9-01-US	69.5		0				
E-B9-02-US	65.5		0				
N306	60.2		0				
N297	55.5		0				
E-B7-07-US	70.01		0				
N296	62.23		0				
N305	56.98		0				
N304	53.99		0				
N61649	64.24		0				
N298	63.09		0				
N367	61.33		0				
N294	60.59		0				
E-B9-CULV3-HW	60.92		0			1.08	0 Headwall height/system capacity
E-B9-CULV3-DS	60.01		0				
E-B10-01-US	63		0				
E-B10-02-US	63.5		0				
E-B10-03-US	65.5		0				
E-B10-CULV1-HW	64.41		0.003			1.09	0 None
E-B10-CULV1-DS	62.97		0.008				
E-B10-04-US	67		0				
E-B10-05-US	68		0				
E-B6-01-US	66.5		0				
E-B6-02-US	69.5		0				
E-B6-03-US	63.5		0				
E-B7-01-US	69.5		0				
E-B7-02-DS	69.56		0.027				
E-B7-03-DS	70.57		0.017				
E-B7-02-US	70.5		0				
E-B7-03-US	72		0				
E-B7-CULV1-HW	68.23		0.068			0.77	0 None
Pit1448	67.18	68	0.077	0		0.73	0 Inlet Capacity
E-B7-CULV1-DS	65.68		0.007				
E-B7-08-US	72		0				
E-B7-09-US	70		0				
E-B7-10-US	69.5		0				
E-B7-11-DS	65.52		0.109				
E-B3-02-US	70.6		0				
E-B3-01-US	72		0				
E-B4-01-US	72		0				
E-B4-02-DS	71.18		0.075				
E-B4-02-US	73		0				
E-B1-01-US	58.5		0				
E-B1-CULV1-DS	59.83		0.006				
E-B1-02-US	60.5		0				
E-B1-03-SPLIT	65.59		0.05				
E-B1-03-US	68.5		0				
E-B1-04-DS	68.5		0				
E-B1-04-US	69.5		0				
Pit8	67.6	69.04	0.015	0.6		1.4	0 Inlet Capacity
E-B7-CULV3-DS	67.09		0				
N266	66.83		0.049				
E-B8-01A-US	71.2		0				
E-B8-01B-US	73		0				
N388	55.5		0.008				
N511	67.05		0.005				
N539	51.59		0.056				
Pit1296	71.6	71.86	0.029	0		0.2	0 Inlet Capacity
N61629	69.24		0				
N259	68		0				
HW1478	48.6		0.044			0.9	0 None
N59	47.42		0				
HW1479	52.04		0.138			0.96	0 None
N38873	50.98		0				
HW1480	56.56		0.026			0.94	0 None
N38880	55.5		0				
SUB-CATCHMENT DETAILS							
Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm
EAST-B2-CAT	0.062	0	0	4.85		11.28	5.5 1EY AEP, 10 min burst, Storm 10
E-B5	0.409	0	0	4.96		0	0 1EY AEP, 10 min burst, Storm 10
EAST-B5-CAT	0	0	0	0		25.62	0 1EY AEP, 10 min burst, Storm 5
E-B7-A	0.078	0	0	5.95		0	0 1EY AEP, 10 min burst, Storm 10
E-B9-A	0	0	0	0		14.24	0 1EY AEP, 10 min burst, Storm 5
E-B9-B	0.023	0	0	1.7		3.96	0 1EY AEP, 10 min burst, Storm 9
E-B9-C	0	0	0	0		5.97	0 1EY AEP, 10 min burst, Storm 5
E-B9-D	0.06	0	0	2.59		6.01	2.93 1EY AEP, 10 min burst, Storm 7
EAST-B6-CAT	0.066	163.253	0.255	3.11		7.23	3.53 1EY AEP, 10 min burst, Storm 9
EAST-B8-CAT	0.041	0	0	1.59		3.69	0 1EY AEP, 10 min burst, Storm 9
EAST-B9-CAT	0	-9999	0	0		3.51	0 1EY AEP, 10 min burst, Storm 5
EAST-B1-CAT	0.116	0	0	3.34		7.76	3.78 1EY AEP, 10 min burst, Storm 9
EAST-B7-CAT	0	0.178	0	0		10.99	0 1EY AEP, 10 min burst, Storm 5
EAST-B10-CAT	0.091	0	0	2.36		5.48	2.67 1EY AEP, 10 min burst, Storm 9
E-B10-A	0	0	0	1.68		3.91	1.91 1EY AEP, 10 min burst, Storm 5
E-B10-03-CATA	0.014	0	0	1.87		4.35	2.12 1EY AEP, 10 min burst, Storm 9
E-B7-02-CAT	0	0	0	0		8.69	0 1EY AEP, 10 min burst, Storm 5
E-B7-03-CAT	0.029	0	0	3.4		7.89	3.85 1EY AEP, 10 min burst, Storm 9
E-B7-B-CAT	0	0	0	0		17.2	0 1EY AEP, 10 min burst, Storm 5
E-B7-C	0.125	0	0	3.58		8.31	4.05 1EY AEP, 10 min burst, Storm 9
E-B7-10-CATB	0	0	0	4.02		9.34	4.55 1EY AEP, 10 min burst, Storm 5
E-B7-11-CAT	0	0	0	0		5.77	0 1EY AEP, 10 min burst, Storm 5
E-B4-02-CAT	0.144	0	0	6.48		0	0 1EY AEP, 10 min burst, Storm 10
E-B1-02-CATA	0.01	0	0	2.71		6.3	3.07 1EY AEP, 10 min burst, Storm 9
E-B1-03-US-CAT	0.086	0	0	3.76		8.73	4.26 1EY AEP, 10 min burst, Storm 7
E-B1-04-CAT	0	0	0	0		3.99	0 1EY AEP, 10 min burst, Storm 5
E-B7-01-CAT	0.025	0	0	4		9.29	4.53 1EY AEP, 10 min burst, Storm 9





Stage 1B (EAST) DRAINS Results							
DRAINS results prepared from Version 2020.036							
10% AEP							
PIT / NODE DETAILS							
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Version 8 Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint
E-B2-02-US	60.5		0				
N67	56.37		0				
N68	56.01		0				
E-B2-01-US	63.5		0				
E-B5-CULV1-HW	67.9		0.48			0.1	0 None
N61643	65.41		0				
N302	64.74		0				
DUMMY-SCALE2	10		0				
DUMMY-SCALE1	8		0				
E-B6-01-US	71		0				
E-B6-02-US	72.5		0				
E-B7-CULV2-HW	72.8		0.091			0.7	0 None
E-B7-CULV2-DS	72.17		0				
E-B7-04-US	73		0				
E-B7-05-US	73		0				
E-B9-CULV1-HW	67.73		0.099			0.77	0 None
E-B9-CULV1-DS	66.54		0.055				
E-B9-07-US	73		0				
E-B9-08-US	68.5		0				
E-B9-05-US	71		0				
E-B9-06-US	68		0				
E-B9-CULV2-HW	65.27		0.204			0.73	0 None
E-B9-CULV2-DS	64.15		0.122				
E-B9-03-US	71		0				
E-B9-04-US	67		0				
E-B9-01-US	69.5		0				
E-B9-02-US	65.5		0				
N306	60.37		0				
N297	55.52		0.039				
E-B7-07-US	70.01		0				
N296	62.23		0				
N305	57.08		0				
N304	53.7		0				
N81649	64.34		0				
N298	63.2		0				
N367	61.47		0				
N294	60.71		0				
E-B9-CULV3-HW	60.92		0			1.08	0 None
E-B9-CULV3-DS	60.01		0				
E-B10-01-US	63		0				
E-B10-02-US	63.5		0				
E-B10-03-US	65.5		0				
E-B10-CULV1-HW	64.59		0.038			0.91	0 None
E-B10-CULV1-DS	63.02		0.03				
E-B10-04-US	67		0				
E-B10-05-US	68		0				
E-B6-01-US	66.5		0				
E-B6-02-US	69.5		0				
E-B6-03-US	63.5		0				
E-B7-01-US	69.5		0				
E-B7-02-DS	69.6		0.071				
E-B7-03-DS	70.61		0.042				
E-B7-02-US	70.5		0				
E-B7-03-US	72		0				
E-B7-CULV1-HW	68.36		0.149			0.64	0 None
Pit1448	67.36	68.06	0.154	0.1		0.55	0 Inlet Capacity
E-B7-CULV1-DS	65.79		0.073				
E-B7-08-US	72		0				
E-B7-09-US	70		0				
E-B7-10-US	69.5		0				
E-B7-11-DS	65.66		0.319				
E-B3-02-US	70.6		0				
E-B3-01-US	72		0				
E-B4-01-US	72		0				
E-B4-02-DS	71.34		0.168				
E-B4-02-US	73		0				
E-B1-01-US	58.5		0				
E-B1-CULV1-DS	59.91		0.054				
E-B1-02-US	60.5		0				
E-B1-03-SPLIT	65.64		0.115				
E-B1-03-US	68.5		0				
E-B1-04-DS	68.51		0.038				
E-B1-04-US	69.5		0				
Pit8	67.73	69.08	0.063	1.7		1.27	0 Inlet Capacity
E-B7-CULV3-DS	67.16		0				
N266	66.9		0.22				
E-B8-01A-US	71.2		0				
E-B8-01B-US	73		0				
N388	55.51		0.026				
N511	67.15		0.034				
N539	51.67		0.341				
Pit1296	71.69	71.88	0.055	0		0.11	0 Inlet Capacity
N81629	68.31		0				
N259	68.1		0				
HW1478	48.93		0.286			0.57	0 None
N59	47.43		0				
HW1479	52.4		0.637			0.6	0 None
N38873	51.12		0				
HW1480	56.87		0.343			0.63	0 None
N38880	55.61		0				
SUB-CATCHMENT DETAILS							
Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm
EAST-B2-CAT	0.264	0.031	0.021	3.83		8.9	4.34 10% AEP, 10 min burst, Storm 3
E-B5	0.807	216.25	52.036	3.92		0	0 10% AEP, 10 min burst, Storm 1
EAST-B5-CAT	0.045	0	0.02	0		41.19	0 10% AEP, 3 hour burst, Storm 2
E-B7-A	0.157	50.983	0	4.69		0	0 10% AEP, 10 min burst, Storm 4
E-B9-A	0.059	0	0	0		20.71	0 10% AEP, 2 hour burst, Storm 2
E-B9-B	0.08	56.562	0	1.34		3.12	0 10% AEP, 10 min burst, Storm 3
E-B9-C	0.067	0	0	0		5.16	0 10% AEP, 15 min burst, Storm 7
E-B9-D	0.192	0	0	2.04		4.74	2.31 10% AEP, 10 min burst, Storm 8
EAST-B6-CAT	0.493	0	61.741	2.46		5.71	2.78 10% AEP, 10 min burst, Storm 3
EAST-B8-CAT	0.119	0	0	1.25		2.91	0 10% AEP, 10 min burst, Storm 9
EAST-B9-CAT	0.013	0.037	0	0		2.77	0 10% AEP, 10 min burst, Storm 6
EAST-B1-CAT	0.275	0	0	2.63		6.12	2.98 10% AEP, 10 min burst, Storm 7
EAST-B7-CAT	0.014	0	0	0		15.98	0 10% AEP, 2 hour burst, Storm 2
EAST-B10-CAT	0.47	0	0	1.86		4.32	2.11 10% AEP, 10 min burst, Storm 3
E-B10-A	0.052	0	0	1.33		3.08	1.5 10% AEP, 10 min burst, Storm 8
E-B10-03-CATA	0.045	0	0	1.48		3.43	1.67 10% AEP, 10 min burst, Storm 9
E-B7-02-CAT	0.028	57.217	118.72	0		7.5	0 10% AEP, 15 min burst, Storm 4
E-B7-03-CAT	0.068	0	0	2.68		6.23	3.03 10% AEP, 10 min burst, Storm 7
E-B7-B-CAT	0.049	0	1.489	0		25.01	0 10% AEP, 2 hour burst, Storm 2
E-B7-C	0.27	8	0	2.82		6.56	3.2 10% AEP, 10 min burst, Storm 4
E-B7-10-CATB	0.008	0	0	3.47		8.06	3.93 10% AEP, 15 min burst, Storm 1
E-B7-11-CAT	0.016	60.92	67.598	0		4.98	0 10% AEP, 15 min burst, Storm 1
E-B4-02-CAT	0.292	0	0	5.11		0	0 10% AEP, 10 min burst, Storm 4
E-B1-02-CATA	0.082	0	0	2.14		4.97	2.42 10% AEP, 10 min burst, Storm 3
E-B1-03-US-CAT	0.198	0	0	2.96		6.89	3.36 10% AEP, 10 min burst, Storm 9
E-B1-04-CAT	0.046	0	0	0		3.15	0 10% AEP, 10 min burst, Storm 7
E-B7-01-CAT	0.106	0.006	0	3.15		7.33	3.57 10% AEP, 10 min burst, Storm 3





Stage 1B (EAST) DRAINS Results								
DRAINS results prepared from Version 2020.036								
1% AEP								
PIT / NODE DETAILS								
Name	Max HGL	Max Pond HGL	Max Surface Flow Arriving (cu.m/s)	Version 8 Max Pond Volume (cu.m)	Min Freeboard (m)	Overflow (cu.m/s)	Constraint	
E-B2-02-US	60.5		0					
N67	56.49		0					
N68	56.02		0					
E-B2-01-US	63.5		0					
E-B5-CULV1-HW	68.16		0.761			-0.16	0.406	Headwall height/system capacity
N61643	65.55		0					
N302	64.85		0.176					
DUMMY-SCALE2	10		0					
DUMMY-SCALE1	8		0					
E-B6-01-US	71		0					
E-B6-02-US	72.5		0					
E-B7-CULV2-HW	72.93		0.15			0.57	0	None
E-B7-CULV2-DS	72.21		0					
E-B7-04-US	73		0					
E-B7-05-US	73		0					
E-B9-CULV1-HW	68.19		0.317			0.31	0	None
E-B9-CULV1-DS	66.62		0.125					
E-B9-07-US	73		0					
E-B9-08-US	68.5		0					
E-B9-05-US	71		0					
E-B9-06-US	68		0					
E-B9-CULV2-HW	65.71		0.49			0.29	0	None
E-B9-CULV2-DS	64.21		0.227					
E-B9-03-US	71		0					
E-B9-04-US	67		0					
E-B9-01-US	69.5		0					
E-B9-02-US	65.5		0					
N306	60.42		0					
N297	55.54		1.878					
E-B7-07-US	70.1		0					
N296	62.39		0					
N305	57.19		0					
N304	53.78		0					
N61649	64.45		0					
N298	63.35		1.119					
N367	61.64		0					
N294	60.83		0.33					
E-B9-CULV3-HW	61.52		0.332			0.48	0	None
E-B9-CULV3-DS	60.22		0					
E-B10-01-US	63		0					
E-B10-02-US	63.5		0					
E-B10-03-US	65.5		0					
E-B10-CULV1-HW	64.73		0.074			0.77	0	None
E-B10-CULV1-DS	63.09		0.057					
E-B10-04-US	67		0					
E-B10-05-US	68		0					
E-B6-01-US	66.5		0					
E-B6-02-US	69.5		0					
E-B6-03-US	63.5		0					
E-B7-01-US	69.57		0					
E-B7-02-DS	69.66		0.146					
E-B7-03-DS	70.65		0.078					
E-B7-02-US	70.5		0					
E-B7-03-US	72		0					
E-B7-CULV1-HW	68.83		0.372			0.17	0	None
Pit1448	68.18	68.3	0.267	0.4		0	0	Outlet System
E-B7-CULV1-DS	65.94		0.213					
E-B7-08-US	72		0					
E-B7-09-US	70		0					
E-B7-10-US	69.5		0					
E-B7-11-DS	65.92		0.628					
E-B3-02-US	70.75		0					
E-B3-01-US	72		0					
E-B4-01-US	72		0					
E-B4-02-DS	71.41		0.277					
E-B4-02-US	73		0					
E-B1-01-US	58.5		0					
E-B1-CULV1-DS	59.98		0.156					
E-B1-02-US	60.5		0					
E-B1-03-SPLIT	65.7		0.266					
E-B1-03-US	68.5		0					
E-B1-04-DS	68.51		0.09					
E-B1-04-US	69.5		0					
Pit8	68.57	69.17	0.173	3.5		0.43	0	Inlet Capacity
E-B7-CULV3-DS	67.25		0					
N266	66.99		0.654					
E-B8-01A-US	71.2		0					
E-B8-01B-US	73		0					
N388	55.51		0.056					
N511	67.23		0.107					
N539	51.79		0.876					
Pit1296	72.06	72.16	0.087	0.2		0	0	Outlet System
N61629	69.47		0					
N299	68.23		0					
HW1478	49.8		1.196			-0.1	0.545	Headwall height/system capacity
N59	47.46		0.801					
HW1479	52.97		2.531			0.03	0	None
N38873	51.27		1.1					
HW1480	57.53		0.878			-0.03	0.088	Headwall height/system capacity
N38880	55.7		0.383					
SUB-CATCHMENT DETAILS								
Name	Max Flow Q (cu.m/s)	Paved Max Q (cu.m/s)	Grassed Max Q (cu.m/s)	Paved Tc (min)	Grassed Tc (min)	Supp. Tc (min)	Due to Storm	
EAST-B2-CAT	0.71	0	-0.013	3.1		7.2	3.51	1% AEP, 10 min burst, Storm 2
E-B5	1.304	0	0	3.17		0	0	1% AEP, 10 min burst, Storm 4
EAST-B5-CAT	0.284	0	0	0		19.2	0	1% AEP, 20 min burst, Storm 7
E-B7-A	0.256	0	0	3.8		0	0	1% AEP, 10 min burst, Storm 4
E-B9-A	0.602	0	0	0		9.96	0	1% AEP, 15 min burst, Storm 5
E-B9-B	0.206	0	0	1.19		2.77	0	1% AEP, 15 min burst, Storm 8
E-B9-C	0.297	0	0	0		4.18	0	1% AEP, 15 min burst, Storm 8
E-B9-D	0.384	0	0	1.65		3.84	1.87	1% AEP, 10 min burst, Storm 4
EAST-B6-CAT	1.694	0	824.713	2.18		5.06	2.47	1% AEP, 15 min burst, Storm 1
EAST-B8-CAT	0.28	0	443.483	1.11		2.58	0	1% AEP, 15 min burst, Storm 8
EAST-B9-CAT	0.035	0	0	0		2.24	0	1% AEP, 10 min burst, Storm 4
EAST-B1-CAT	0.646	0.023	0	2.13		4.96	2.42	1% AEP, 10 min burst, Storm 10
EAST-B7-CAT	0.078	61.47	0	0		7.02	0	1% AEP, 10 min burst, Storm 10
EAST-B10-CAT	1.225	0	0	1.65		3.83	1.87	1% AEP, 15 min burst, Storm 8
E-B10-A	0.122	0.362	60.712	1.07		2.5	1.22	1% AEP, 10 min burst, Storm 4
E-B10-03-CATA	0.095	1108.18	72	1.31		3.04	1.48	1% AEP, 15 min burst, Storm 8
E-B7-02-CAT	0.155	0.011	57.562	0		6.08	0	1% AEP, 15 min burst, Storm 1
E-B7-03-CAT	0.133	0	63.5	2.17		5.04	2.46	1% AEP, 10 min burst, Storm 9
E-B7-B-CAT	0.298	0.113	0.121	0		12.03	0	1% AEP, 15 min burst, Storm 7
E-B7-C	0.455	73	0	2.5		5.91	2.83	1% AEP, 15 min burst, Storm 9
E-B7-10-CATB	0.041	10	0	2.81		6.53	3.18	1% AEP, 15 min burst, Storm 1
E-B7-11-CAT	0.071	0	0	0		4.04	0	1% AEP, 15 min burst, Storm 8
E-B4-02-CAT	0.48	0.137	0.023	4.14		0	0	1% AEP, 10 min burst, Storm 4
E-B1-02-CATA	0.256	0	0	1.89		4.4	2.15	1% AEP, 15 min burst, Storm 8
E-B1-03-US-CAT	0.356	0.105	0	2.4		5.58	2.72	1% AEP, 10 min burst, Storm 6
E-B1-04-CAT	0.144	70.769	0.145	0		2.55	0	1% AEP, 10 min burst, Storm 4
E-B7-01-CAT	0.29	56.369	0.054	2.55		5.94	2.89	1% AEP, 10 min burst, Storm 2

Cat314	0.078	0	0	0	7.02	0	1% AEP, 10 min burst, Storm 10	
E-B8-02	0.222	0	0.493	0	17.34	0	1% AEP, 20 min burst, Storm 5	
E-B1-01-CAT	0.093	62.358	71.342	1.64	3.81	1.86	1% AEP, 15 min burst, Storm 8	
E-B7-10-CATA	0.182	0.174	0	2.57	5.96	2.91	1% AEP, 10 min burst, Storm 2	
E-B4-01-CAT	0.148	0.101	0.02	1.5	0	0	1% AEP, 10 min burst, Storm 4	
EAST-B4-CAT	0.05	0	68	3.56	8.26	4.03	1% AEP, 10 min burst, Storm 6	
EAST-B3-CAT	0.72	0	0.024	2.15	4.99	2.43	1% AEP, 10 min burst, Storm 10	
PIPE DETAILS								
Name	Max Q (cu.m/s)	Max V (m/s)	Max U/S HGL (m)	Max D/S HGL (m)	Due to Storm			
Pipe10	0.241	2.81	57.071	56.494	1% AEP, 1 hour burst, Storm 10			
P21	0.254	3.13	56.494	56.228	1% AEP, 1 hour burst, Storm 10			
E-B6-CULV1	0.386	2.43	67.978	67.238	1% AEP, 15 min burst, Storm 6			
P13826	0.424	3.65	66.388	65.548	1% AEP, 1 hour burst, Storm 7			
Pipe179	0.464	3.97	65.55	64.847	1% AEP, 1 hour burst, Storm 7			
DUMMY-SCALE	0	0	10	8	1% AEP, 10 min burst, Storm 5			
E-B7-CULV2	0.214	3.02	72.734	72.206	1% AEP, 10 min burst, Storm 3			
E-B9-CULV1	0.29	4.01	67.785	66.619	1% AEP, 30 min burst, Storm 8			
E-B9-CULV2	0.295	3.38	65.375	64.242	1% AEP, 2 hour burst, Storm 5			
Pipe283	0.582	4.87	61.018	60.422	1% AEP, 30 min burst, Storm 2			
Pipe183	0.628	6.51	60.422	55.724	1% AEP, 30 min burst, Storm 2			
Pipe184	0.024	0.88	70.56	70.103	1% AEP, 2 hour burst, Storm 3			
Pipe185	0.255	1.9	63.117	62.578	1% AEP, 2 hour burst, Storm 3			
Pipe213	0.45	4.38	59.124	57.192	1% AEP, 30 min burst, Storm 8			
Pipe220	0.484	4.52	67.192	63.781	1% AEP, 30 min burst, Storm 8			
P13854	0.683	5.09	65.212	64.452	1% AEP, 30 min burst, Storm 8			
Pipe182	0.702	5.38	64.452	63.352	1% AEP, 30 min burst, Storm 8			
Pipe349	0.496	2.66	62.083	61.644	1% AEP, 30 min burst, Storm 8			
Pipe186	0.55	3.01	61.644	60.87	1% AEP, 30 min burst, Storm 8			
E-B9-CULV3	0.249	2.63	61.333	60.258	1% AEP, 2 hour burst, Storm 3			
Pipe122	0.086	1.51	64.614	63.085	1% AEP, 15 min burst, Storm 1			
P3176	0.301	1.89	68.741	68.187	1% AEP, 15 min burst, Storm 6			
E-B7-CULV1	0.479	3.03	67.487	65.942	1% AEP, 15 min burst, Storm 8			
E-B7-CULV3	0.284	2.02	68.38	67.373	1% AEP, 15 min burst, Storm 1			
Pipe2927	0.137	1.24	71.973	71.424	1% AEP, 10 min burst, Storm 4			
Pipe178	0.201	1.26	71.099	70.758	1% AEP, 10 min burst, Storm 7			
P13783	0.241	2.37	70.108	69.466	1% AEP, 1 hour burst, Storm 2			
Pipe177	0.282	2.77	69.466	68.233	1% AEP, 1 hour burst, Storm 2			
Pipe8633	0.3174	4.24	48.976	47.655	1% AEP, 1 hour burst, Storm 6			
Pipe8646	1.207	5.03	52.521	51.272	1% AEP, 1 hour burst, Storm 6			
Pipe8668	0.362	3.31	57.08	55.702	1% AEP, 2 hour burst, Storm 1			
CHANNEL DETAILS								
Name	Max Q (cu.m/s)	Max V (m/s)				Due to Storm		
OVERFLOW ROUTE DETAILS								
Name	Max Q U/S	Max Q D/S	Safe Q	Max D	Max DvX	Max Width	Max V	Due to Storm
Basin 1	0.012	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 10
EAST-B10-O	0.018	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 8
EAST-B1-O	0.014	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 8
EAST-B6-O	0.012	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 2
E-B10-01	0	0.15	0.373	0.521	0.06	6.26	0.29	1% AEP, 15 min burst, Storm 9
E-B10-02	0	0.617	0.352	0.521	0.22	6.26	0.59	1% AEP, 15 min burst, Storm 1
E-B10-03A	0	0.095	0.885	0.176	0.09	2.11	0.68	1% AEP, 10 min burst, Storm 9
E-B10-03B	0.161	0.21	0.655	0.521	0.15	6.26	0.87	1% AEP, 15 min burst, Storm 1
E-B10-04	0	0.059	0.787	0.319	0.06	3.83	0.59	1% AEP, 10 min burst, Storm 9
E-B10-05	0	0.061	1.746	0.319	0.08	2.56	0.7	1% AEP, 10 min burst, Storm 9
E-B1-01	0	0.092	0.36	0.144	0.13	1.73	1.04	1% AEP, 10 min burst, Storm 9
E-B1-02A	0	0.212	0.37	0.244	0.18	2.92	0.97	1% AEP, 15 min burst, Storm 8
E-B1-02B	0.212	0.233	0.84	0.186	0.21	2.23	1.13	1% AEP, 15 min burst, Storm 1
E-B1-03A	0	0.352	0.73	0.253	0.26	3.03	1.14	1% AEP, 10 min burst, Storm 6
E-B1-03B	0.265	0.431	0.726	0.247	0.29	2.96	1.18	1% AEP, 30 min burst, Storm 8
E-B1-04	0	0.104	0.719	0.23	0.15	1.84	0.91	1% AEP, 15 min burst, Storm 1
E-B1-04-CONNECT	0.09	0.077	19.197	0.201	0	32	0.24	1% AEP, 15 min burst, Storm 8
E-B2-01	0	0.338	1.685	0.231	0.37	1.85	1.59	1% AEP, 10 min burst, Storm 2
E-B2-02	0	0.317	1.157	0.185	0.29	2.22	1.54	1% AEP, 10 min burst, Storm 2
E-B3-01	0	0.171	0.565	0.249	0.11	2.99	0.5	1% AEP, 15 min burst, Storm 8
E-B3-02	0.01	0.291	0.367	0.749	0.06	8.99	0.1	1% AEP, 10 min burst, Storm 6
E-B4-01	0	0.15	0.099	0.405	0.41	0.54	1.02	1% AEP, 10 min burst, Storm 4
E-B4-02	0	0.436	0.929	0.348	0.36	2.79	1.21	1% AEP, 10 min burst, Storm 4
E-B5-01	0	0.228	1.566	1.247	0.2	9.97	1.11	1% AEP, 10 min burst, Storm 8
E-B5-02	0	0.846	1.195	1.247	0.43	9.97	1.04	1% AEP, 10 min burst, Storm 7
E-B6-01	0	0.32	0.991	0.614	0.18	7.37	0.93	1% AEP, 15 min burst, Storm 8
E-B6-02	0	0.18	1.569	0.614	0.21	4.91	1.19	1% AEP, 15 min burst, Storm 8
E-B6-03	0	0.655	0.45	0.614	0.26	7.37	0.76	1% AEP, 15 min burst, Storm 8
E-B7-01	0.003	0.285	0.801	0.304	0.15	2.43	0.51	1% AEP, 15 min burst, Storm 1
E-B7-02	0	0.128	0.396	0.195	0.13	2.34	0.83	1% AEP, 15 min burst, Storm 8
E-B7-03	0	0.127	0.542	0.174	0.14	2.09	0.91	1% AEP, 10 min burst, Storm 6
E-B7-04	0	0.164	0.964	0.524	0.08	4.19	0.34	1% AEP, 10 min burst, Storm 9
E-B7-05	0	0.063	1.356	0.524	0.03	4.19	0.19	1% AEP, 10 min burst, Storm 9
E-B7-06	0.207	0.289	1.599	0.854	0.27	6.83	1.21	1% AEP, 15 min burst, Storm 8
E-B7-07	0.024	0.192	1.226	0.832	0.14	6.66	0.63	1% AEP, 15 min burst, Storm 6
E-B7-08	0	0.222	0.821	0.179	0.17	2.14	0.92	1% AEP, 10 min burst, Storm 9
E-B7-09	0	0.222	0.606	0.203	0.12	2.44	0.59	1% AEP, 15 min burst, Storm 9
E-B7-10A	0	0.174	0.707	0.226	0.13	2.71	0.61	1% AEP, 15 min burst, Storm 9
E-B7-10B	0.169	0.193	1.036	0.431	0.19	3.45	0.82	1% AEP, 15 min burst, Storm 8
E-B7-11	0.592	0.578	0.098	0.691	0.34	5.53	0.8	1% AEP, 15 min burst, Storm 8
E-B7-01	0.012	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 8
E-B8-01A	0	0.113	0.732	0.53	0.06	4.24	0.29	1% AEP, 15 min burst, Storm 8
E-B8-01B	0	0.087	1.412	0.53	0.09	4.24	0.6	1% AEP, 10 min burst, Storm 9
E-B9-01	0	0.255	0.955	0.211	0.2	2.53	1.05	1% AEP, 10 min burst, Storm 9
E-B9-02	0	0.115	0.631	0.211	0.09	2.53	0.51	1% AEP, 10 min burst, Storm 9
E-B9-03	0	0.163	0.962	0.802	0.14	9.62	0.89	1% AEP, 15 min burst, Storm 8
E-B9-04	0	0.105	0.685	0.802	0.07	9.62	0.5	1% AEP, 15 min burst, Storm 8
E-B9-05	0	0.132	1.632	0.203	0.16	1.62	0.83	1% AEP, 15 min burst, Storm 8
E-B9-06	0	0.073	1.146	0.206	0.09	1.65	0.47	1% AEP, 15 min burst, Storm 9
E-B9-07	0	0.402	1.254	0.781	0.29	6.25	0.99	1% AEP, 15 min burst, Storm 6
E-B9-08	0	0.125	0.949	0.781	0.05	6.25	0.27	1% AEP, 10 min burst, Storm 10
low-25	0.012	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 7
low0.5	0.012	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 7
O22992	0.018	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 8
O23058	0.018	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 8
O29065	0.013	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 8
O29069	0.014	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 8
O31534	0.013	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 2
O31545	0.013	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 2
O31559	0.013	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 2
O72267	0.012	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 2
O72283	0.012	0	12.141	3	0	32	0	1% AEP, 30 min burst, Storm 2
O9296	0.016	0	12.141	3	0	32	0	1% AEP, 1 hour burst, Storm 7
OF139	0	0	1.7	0	0	0	0	
OF144	0.131	0.282	0.847	0.201	0.24	2.41	1.19	1% AEP, 15 min burst, Storm 1
OF153	0.239	0.277	1.234	0.242	0.26	2.9	1.57	1% AEP, 15 min burst, Storm 1
OF159	0.284	0.319	0.488	0.248	0.22	2.98	0.94	1% AEP, 10 min burst, Storm 2
OF165	0.592	0.837	1.126	0.972	0.54	11.67	2.2	1% AEP, 15 min burst, Storm 1
OF18	0.253	0.252	19.227	0.286	0.01	32	0.41	1% AEP, 1 hour burst, Storm 10
OF22	0	0	1.333	0	0	0	0	
OF226	0.953	0.953	19.201	0.413	0.03	32	0.1	1% AEP, 10 min burst, Storm 2
OF244	1.294	1.294	19.201	0.972	0.04	32	0.05	1% AEP, 30 min burst, Storm 3
OF282	0	0	10.302	0	0	0	0	
OF286	0.36	0.36	0.915	0.802	0.29	9.62	1.37	1% AEP, 30 min burst, Storm 9
OF293	0	0	19.196	0	0	0	0	
OF309	0.089	0.085	19.13	0.206	0	32	0.29	1% AEP, 15 min burst, Storm 9
OF311	0	0	0.9	0	0	0	0	
OF315	0	0	1.403	0	0	0	0	
OF320	0	0	0.644	0	0	0	0	



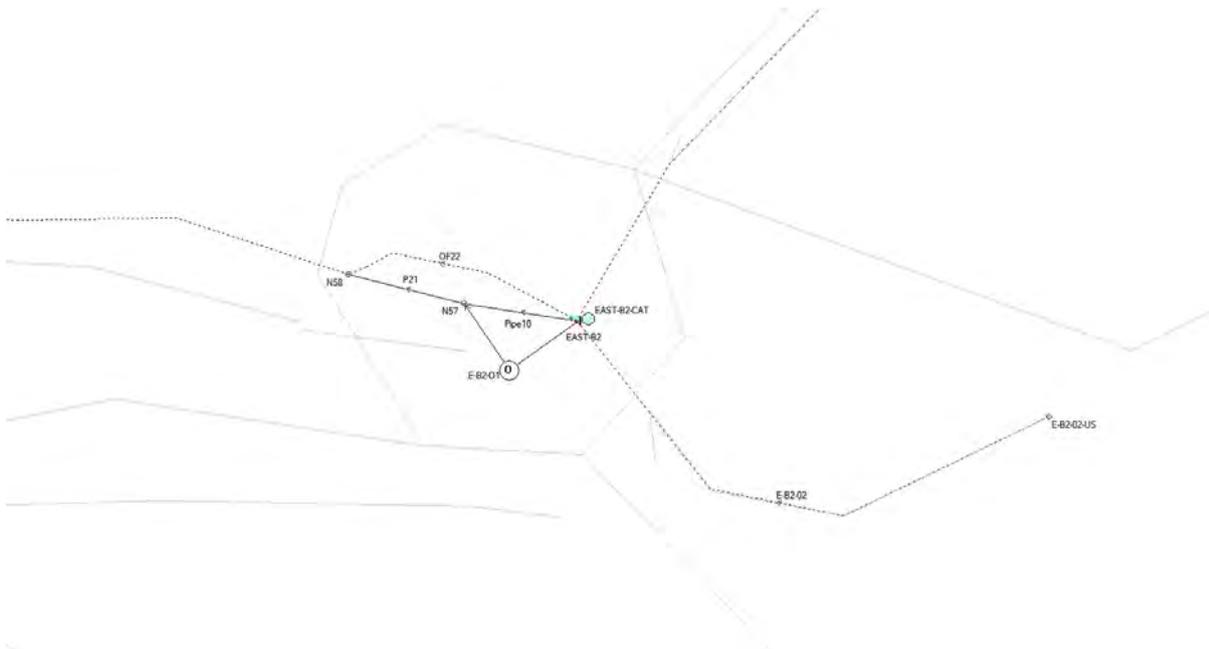


Figure G.1 Typical basin set-up

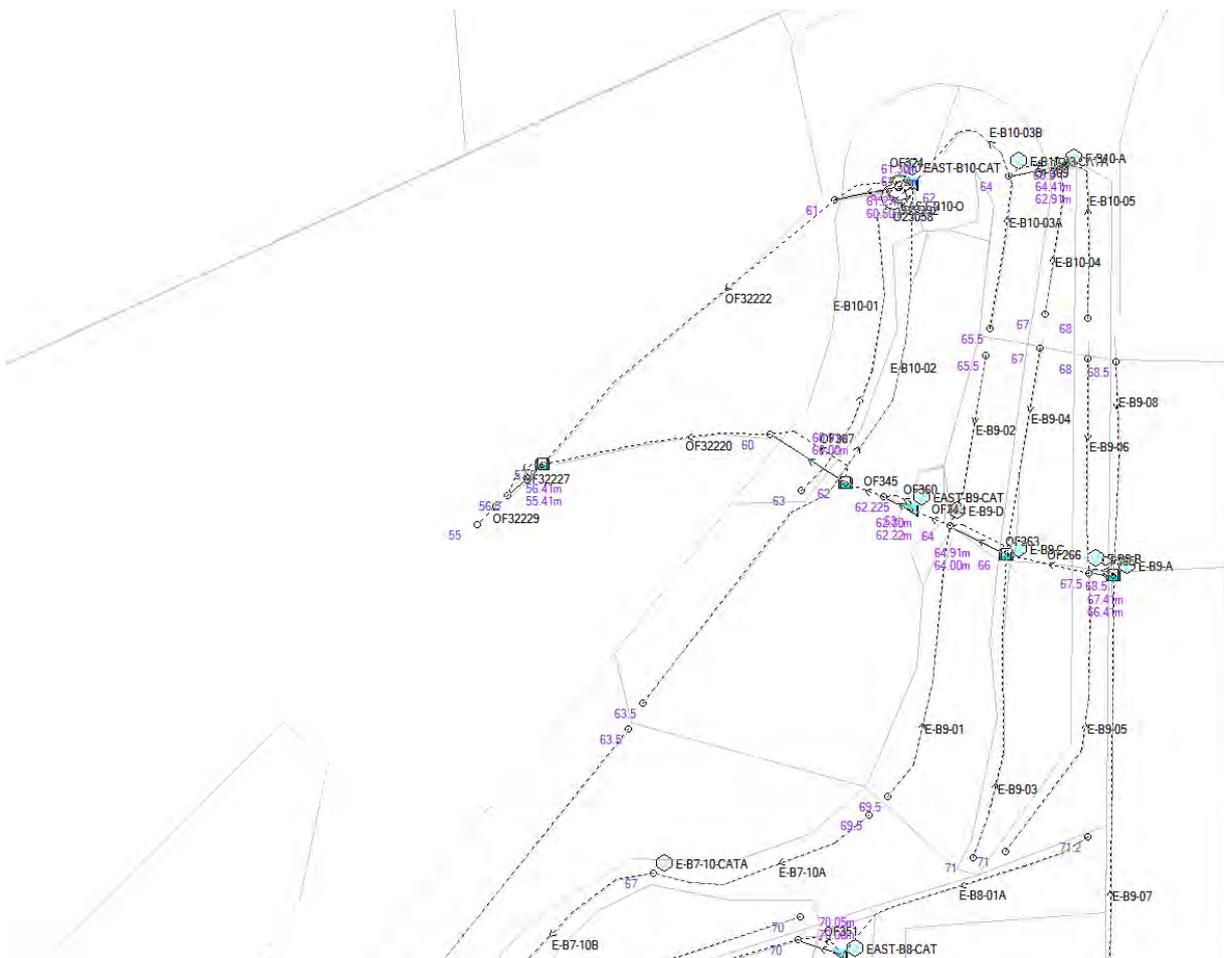


Figure G.2 East-1 schematic diagram



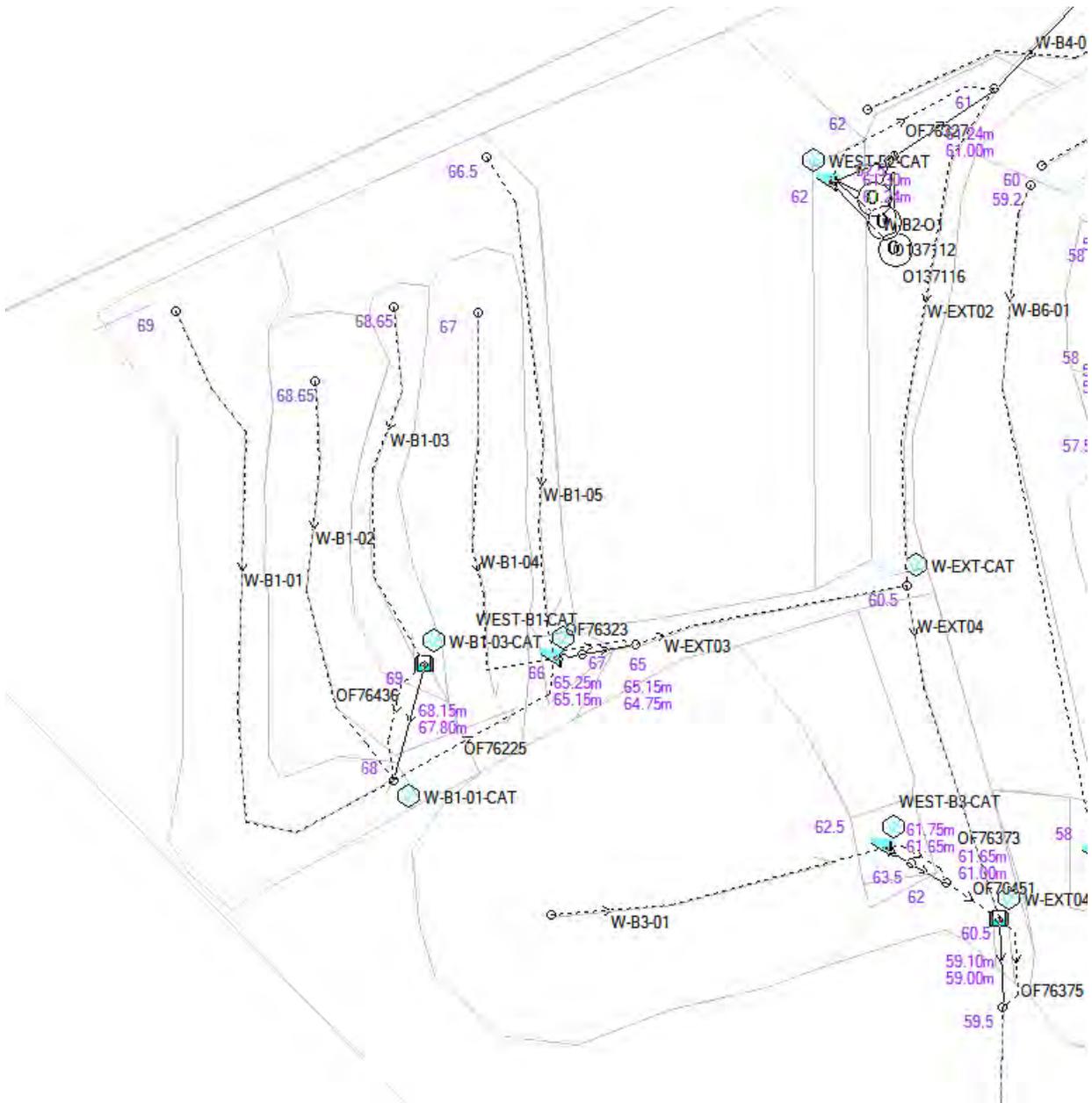


Figure G.5 West-3 schematic diagram

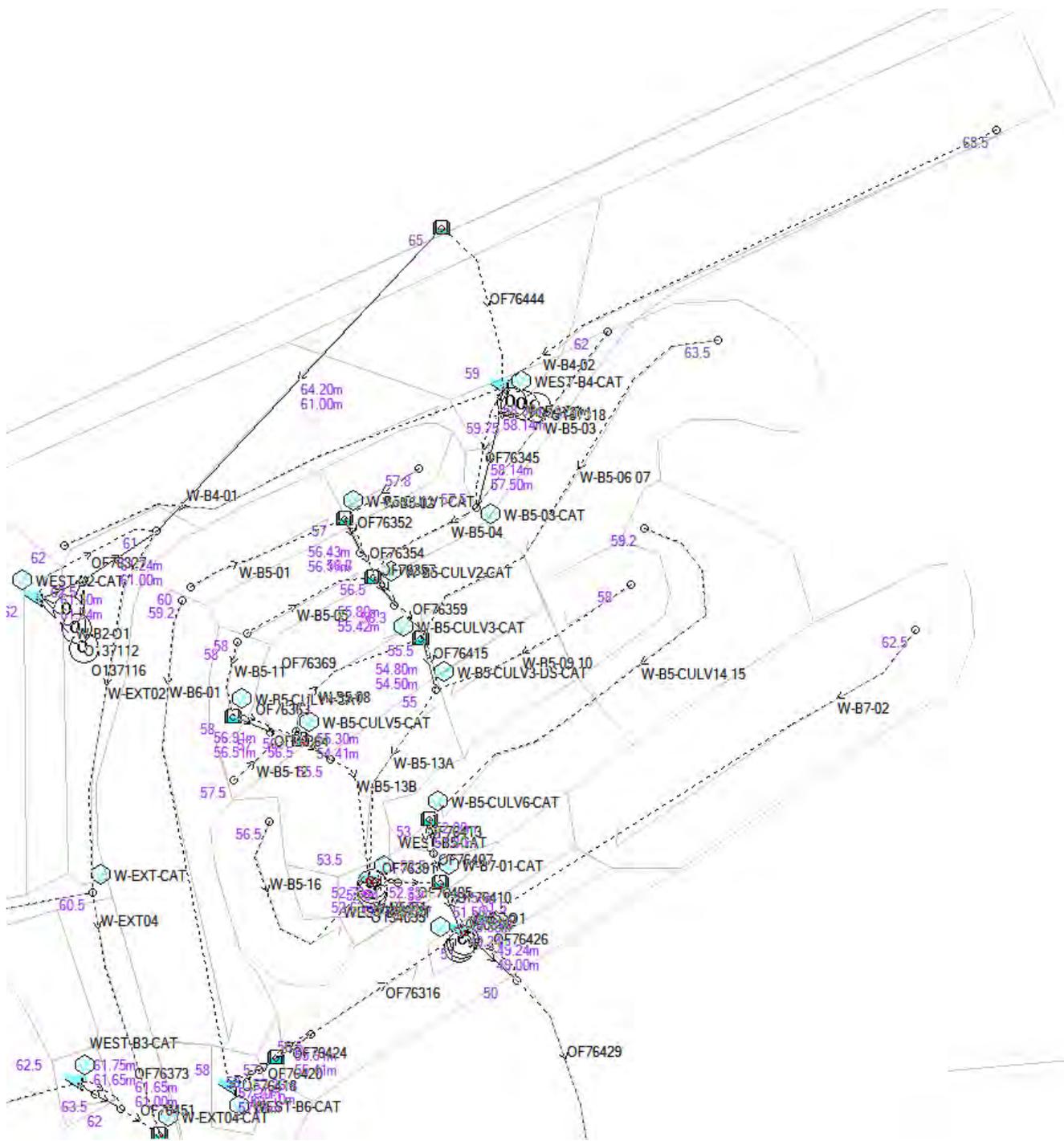


Figure G.6 West-2 schematic diagram



# Appendix H

**Site and soil evaluation for onsite  
wastewater management**



# **Albany Motorsport Park – Development Application**

**Site and Soil Evaluation for Onsite  
Wastewater Management**

City of Albany

19 August 2021

→ **The Power of Commitment**



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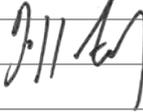
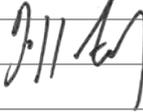
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# Executive summary

The City of Albany (CoA) has engaged GHD to prepare a Site and Soil Evaluation for Onsite Wastewater Management report for the staged construction of the Albany Motorsport Park (AMP) at Lot 5780 (No. 54) Down Road South, Drome (the Site) (Figure 1, Appendix A). The project Proponent is the Great Southern Motorplex Group Inc. (GSMG).

Due to the scale and nature of the proposed development, the works have been broken down into two key stages which comprise the following:

- Stage 1:
  - Stage 1A: Construction of motocross track and 4WD driver training, ATV area and associated infrastructure.
  - Stage 1B: Construction of racetrack and associated infrastructure (subject to funding).
- Future Development: Construction and replacement of final permanent structures to support the function of the motorsports complex (subject to funding). Stage 2 will be addressed as a separate Development Application.

This Site and Soil Evaluation for Onsite Wastewater Management report has been developed as per the Department of Health, Western Australia (DOHWA) template report based on the *Health (Treatment of Sewage and Disposal of Effluent and Liquid Waste) Regulations 1974*, Government Sewerage Policy 2019, State Planning Policy 2.9, AS/NZS 1547 and other supporting documentation (DOHWA, 2021).

The purpose of this Site and Soil Evaluation (SSE) report is to outline the site, soil and groundwater conditions at the proposed AMP site with regarding to suitability for onsite effluent disposal during operation of the AMP. This report provides supporting information for the Development Application for the Stage 1 of the Site.

Based on an assessment of the soil physical and chemical results for the six test pit locations, it is recommended that the LAAs for the Race Track Precinct and Motocross Precinct are located at TP01 and TP06, respectively. The sizing for a wastewater treatment system and LAA has been developed in this SSE report for Stage 1A in the Motocross Precinct only.

The proposed clubhouse within the Motocross Precinct will be constructed in Stage 1A of the development. It is anticipated that this will be an unlicensed facility (15 L/ person/ day) however provision has been made for anticipated wastewater volumes for a licensed facility (35 L/ person/ day), to allow for possible increased loading at the site if it were to become a licensed facility.

The Motocross Precinct clubhouse is expected to have intermittent use throughout the Motocross season and on a weekly basis, with up to 300 patrons on Sunday or Saturday followed by minimal usage during the week and off-season downtime. Therefore, for the purpose of calculating anticipated wastewater volumes it is assumed that there is an average of 100 people/ day.

In order to accommodate spikes in wastewater volumes on event days when there is up to 300 patrons using the Motocross Precinct clubhouse facilities, it is proposed to install a 15,000 L holding tank, to balance storage over the course of a typical week.

The results of a water balance for the Motocross Precinct, for an average of 100 persons/day, indicate that 1,100 m<sup>2</sup> will be required for the sub-soil irrigation area. There is adequate area of land available within the vicinity of TP01 to accommodate the site of the required LAA.

As per the requirements of the Department of Water *WQPN 100* (DoW, 2007) and the *Government Sewerage Policy* (DPLH, 2019) a 'Secondary' wastewater treatment plant, with engineering certification to meet effluent quality of Biological Oxygen Demand (BOD) < 20 mg/L; Total Suspended Solids (TSS) < 30 mg/L; Total Nitrogen (TN) < 10 mg/L; Total Phosphorus (TP) < 1 mg/L; and *Escherichia coli* < 10 cfu/100mL is required in a Priority 2 PDWSA.

It is recommended that a DOHWA approved 'Secondary' treatment system, certified to AS1546.3:2008, is selected and installed for the Motocross Precinct during Stage 1A of development.

At time of writing, an onsite effluent disposal system was not proposed to be installed in the Race Track Precinct. All liquid waste from transportable buildings, toilets and washdown facilities is proposed to be removed offsite, as required, by an approved contractor. If onsite effluent disposal is proposed in the future is it expected a similar system, with holding tank, will be utilised to manage spikes in wastewater volumes for events and off-season downtime.

*This report is subject to, and must be read in conjunction with, the limitations set out in section 1.2 and the assumptions and qualifications contained throughout the Report.*

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# 1. Introduction

## 1.1 Background

The City of Albany (CoA) has engaged GHD to prepare a Site and Soil Evaluation for Onsite Wastewater Management report for the staged construction of the Albany Motorsport Park (AMP) at Lot 5780 (No. 54) Down Road South, Drome (the Site) (Figure 1, Appendix A). The project Proponent is the Great Southern Motorplex Group Inc. (GSMG).

The Great Southern Motorplex Group Inc. (GSMG), the Proponent, in partnership with the City of Albany, intend to develop the site as a regional motorsport facility. In October 2018, the City of Albany Council resolved to purchase the site and settlement of the land purchase was concluded in 2019. Once constructed, the AMP will be operated and managed by Albany Motorsport Venue Incorporated (AMV Inc.).

The proposed AMP forms part of the CoA's strategy to expand upon its existing motorsports facilities within the greater Albany area. The AMP is to be the largest facility of its kind in Western Australia and will support the local economy.

## 1.2 Purpose of this report

This Site and Soil Evaluation for Onsite Wastewater Management report has been developed as per the Department of Health, Western Australia (DOHWA) template report based on the *Health (Treatment of Sewage and Disposal of Effluent and Liquid Waste) Regulations 1974*, Government Sewerage Policy 2019, State Planning Policy 2.9, AS/NZS 1547 and other supporting documentation (DOHWA, 2021).

The purpose of this Site and Soil Evaluation (SSE) report is to outline the site, soil and groundwater conditions at the proposed AMP site with regarding to suitability for onsite effluent disposal during operation of the AMP. This report provides supporting information for the Development Application for the Stage 1 of the Site.

## 1.3 Evaluator's qualifications, experience and professional indemnity

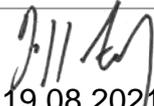
The SSE has been undertaken by Dr Jeff Foley who is a Chemical Engineer with 20 years' technical experience specialising in the areas of wastewater treatment and recycling and integrated water management. His involvement in water cycle projects has ranged from policy and planning, concept design and process modelling, through to detailed design, construction, commissioning and process optimisation.

GHD's site evaluation has been supported in the field by Great Southern Geotechnics (GSG), who specialise in high-quality testing of construction materials and consultancy services to the civil construction, agriculture, environmental, mining and resources industries across WA's Great Southern region. GSG operates an independent NATA Accredited Construction Materials Testing Laboratory, in compliance with AS ISO/IEC 17025 and ISO 9001.

Dr Foley is suitably qualified to provide interpretation of site, soil and climate conditions, undertake water balances, selection and design of appropriate wastewater treatment systems, disposal and reuse options. A summary of the Dr Foley's site evaluator details has been provided in Table 1 and a copy of his CV and qualifications can be provided on request.

A copy of GHD's Professional Indemnity Insurance certificate is included in Appendix C.

Table 1 Site Evaluator Details

Site evaluator details	
Name Company	Dr Jeff Foley, Technical Director – Wastewater process engineering GHD Pty Ltd
Phone Email	(08) 9840 5101 Jeff.Foley@ghd.com
Qualification Knowledge, skills and practical experience	MIEAust, BE(Chem) (Hons I), BA, PhD (UQ) – <i>Life cycle assessment of wastewater treatment systems</i> Employed as a wastewater process designer (inc. on-site systems) by GHD 2001 – 2021.
Date of site assessment	16/08/2021
Signature	
Date	19.08.2021

## 1.4 Scope and limitations

This report: has been prepared by GHD for City of Albany and may only be used and relied on by City of Albany for the purpose agreed between GHD and City of Albany as set out in section 1.2 of this report.

GHD otherwise disclaims responsibility to any person other than City of Albany arising in connection with this report. GHD also excludes implied warranties and conditions, to the extent legally permissible.

The services undertaken by GHD in connection with preparing this report were limited to those specifically detailed in the report and are subject to the scope limitations set out in the report.

The opinions, conclusions and any recommendations in this report are based on conditions encountered and information reviewed at the date of preparation of the report. GHD has no responsibility or obligation to update this report to account for events or changes occurring subsequent to the date that the report was prepared.

The opinions, conclusions and any recommendations in this report are based on assumptions made by GHD described in this report. GHD disclaims liability arising from any of the assumptions being incorrect.

The opinions, conclusions and any recommendations in this report are based on information obtained from, and testing undertaken at or in connection with, specific sample points. Site conditions at other parts of the site may be different from the site conditions found at the specific sample points.

Investigations undertaken in respect of this report are constrained by the particular site conditions, such as the location of buildings, services and vegetation. As a result, not all relevant site features and conditions may have been identified in this report.

Site conditions (including the presence of hazardous substances and/or site contamination) may change after the date of this Report. GHD does not accept responsibility arising from, or in connection with, any change to the site conditions. GHD is also not responsible for updating this report if the site conditions change.

GHD has prepared this report on the basis of information provided by City of Albany and others who provided information to GHD (including Government authorities), which GHD has not independently verified or checked beyond the agreed scope of work. GHD does not accept liability in connection with such unverified information, including errors and omissions in the report which were caused by errors or omissions in that information.

## 2. Site development description

The AMP is proposed to be developed at Lot 5780 Down Road South, Drome which is located approximately 20 km to the north of the Albany CBD and is 192.34 ha in size. The AMP comprises 141.7 ha (including 0.2 ha for crossovers) in the eastern portion of the Site. Two areas within Lot 5780 are excluded from the AMP development and include 49.47 ha at the western end of the Site which is covered with native vegetation and a dam area (1.37 ha) on the northern boundary which is subleased to Plantation Energy.

The Site is zoned as 'Special Use – SU26' under Local Planning Scheme No. 1, Scheme Amendment No. 35.

At full development, the proposed AMP will consist of:

- Sealed, configurable multi-use track (3.5 km long × 12 m wide) for motor car racing, motorcycle racing, drifting, driver training and cycling:
  - Designed to comply with Motorsport Australia *Track Operator's Safety Guide* (CAMS, 2012) and Motorcycling Australia (MA) *Track Guidelines* (MA, 2011)
  - To be licensed by Motorsport Australia for Fédération Internationalé de l'Automobile (FIA) Grade 2 and Fédération Internationalé Motocyclisme (FIM) Grade B (i.e. up to second-tier international motor racing)
- A motocross circuit designed and constructed in association with MA guidelines.
- An off-road four-wheel drive (4WD) and all-terrain vehicle (ATV) training area.
- Associated buildings and infrastructure.

### 2.1 Staging of the development

Due to the scale and nature of the proposed development, the works have been broken down into two key stages which comprise the following:

- Stage 1:
  - Stage 1A: Construction of motocross track and 4WD driver training, ATV area and associated infrastructure.
  - Stage 1B: Construction of racetrack and associated infrastructure (subject to funding).
- Future Development: Construction and replacement of final permanent structures to support the function of the motorsports complex (subject to funding). Stage 2 will be addressed as a separate Development Application.

A Master Plan, which illustrates the various aspects of the Site and staging areas, has been developed by the GSMG and CoA to support the Development Application for the AMP (Figure 2, Appendix A).

### 2.2 Anticipated wastewater volumes

The proposed clubhouse within the Motocross Precinct will be constructed in Stage 1A of the development. It is anticipated that this will initially be an unlicensed facility (15 L/ person/ day) however provision has been made for anticipated wastewater volumes for a licensed facility (35 L/ person/ day), to allow for possible increased loading at the site if it were to become a licensed facility.

The Motocross Precinct clubhouse is expected to have intermittent use throughout the Motocross season (approx. March to October) and on a weekly basis, with up to 300 patrons on Sunday or Saturday followed by minimal usage (max. 20 persons per day) during the week and off-season downtime. Therefore, for the purpose of calculating anticipated wastewater volumes (Table 2) it is assumed that there is an average of 100 people/ day (Appendix B).

In order to accommodate spikes in wastewater volumes on event days when there is up to 300 patrons using the Motocross Precinct clubhouse facilities, it is proposed to install a 15,000 L holding tank, to balance out wastewater flows over the course of a typical week. The holding tank will also help store effluent during the off-season period.

At this stage, an onsite effluent disposal system is not proposed to be installed in the Race Track Precinct. All liquid waste from transportable buildings, toilets and washdown facilities is proposed to be removed offsite, as required, by an approved contractor. If onsite effluent disposal is proposed in the future is it expected a similar system, with holding tank, will be utilised to manage spikes in wastewater volumes for events and off-season downtime.

**Table 2** Anticipated wastewater volumes

Type	Input volume	Load per person	Daily flow (L/day)
<b>Stage 1A – Motocross Precinct</b>			
Permanent building (5 x sinks, 4 x toilet pans, urinal)	Up to 300 persons (average 100 persons/day)	35 L/person/day	3,500 L/day (average)
Transportable toilets	One permanent block and additional transportables for special events	35 L/person/day	Liquid waste to be removed offsite by an approved contractor, as required
Washdown area	Variable	-	
<b>Total</b>			<b>3,500 L/day (average)</b>
<b>Stage 1B – Racetrack Precinct</b>			
Transportable building	500 persons	35 L/person/day	Liquid waste to be removed offsite by an approved contractor, as required
Transportable toilets	Special events	35 L/person/day	
Washdown area	Variable	-	
<b>Total</b>			

## 2.3 Site development description

The AMP site development description is outlined in Table 3.

**Table 3** Description of the development

Development characteristic	Description		
Site address	Lot 5780 (No. 54) Down Road South, Drome		
Owner/ developer	City of Albany		
Proponent	Great Southern Motorplex Group (GSMG)		
Postal address	PO Box 484, ALBANY WA 6331		
Contact for SSE	Ph: 9840 5101	Mob: 0410 541 971	Email: jeff.foley@ghd.com
Date of field work	25 June 2021		
Local Government	City of Albany		
Zoning	Special Use		
Lot size	192.34 ha		
Proposal	Albany Motorsport Park		
Water supply	Bore and rainwater		
Availability of sewer	Unavailable		
Development located within:	Public drinking water source area: Yes – Priority 2 PDWSA	Sewage sensitive areas Yes – Sewerage Category (f) Within 1 km of significant wetlands	
Anticipated wastewater volume:	Sewage (L): Motocross Precinct 3,500 L/day (average)	Trade waste (L): Zero	

## 3. Site and soil assessment

### 3.1 Site assessment

GHD have undertaken a number of site walkovers for the AMP site from 2018 to 2021 and are very familiar with the existing site conditions. In addition, an intrusive field investigation was undertaken, by Great Southern Geotechnics, on 25 June 2021. This investigation involved excavating six test pits to a depth of 2500 mm below ground level (bgl), using a mini excavator with a 300 mm auger. Soil types, profiles and groundwater levels were then visually assessed and recorded onsite at time of site investigation, as per the DOHWA (2021) SSE template guidelines (Great Southern Geotechnics, 2021).

The findings of the desktop and field assessment, level of constraint and proposed mitigation measures, for the proposed Motocross Precinct and Race Track Precinct onsite effluent disposal locations, have been summarised in Table 4.

**Table 4** Key site characteristics, level of constraint and proposed mitigation measures for the proposed Motocross Precinct and Race Track Precinct effluent disposal areas

Site characteristics	Investigations and reporting	Level of constraint	Mitigation measures																																																				
Climate	Albany is located on the south coast of Western Australia and the climate is broadly described as Mediterranean, with warm dry summers and mild wet winters. The nearest Bureau of Meteorology (BoM) official recording station that has mean daily evaporation data (1968 to 2012) is the Albany Airport Comparison weather station (Site number 9741) (BoM, 2021).	High	Divert stormwater from upslope around sub-soil irrigation area																																																				
	Mean monthly rainfall levels at the Albany Airport Comparison weather station (BoM, 2021) and pan evaporation data (DPIRD, 1987) are presented below. This shows that mean monthly evaporation exceeds mean monthly rainfall for seven months of the year, from November to April.																																																						
	<table border="1"> <thead> <tr> <th>Month</th> <th>Jan</th> <th>Feb</th> <th>Mar</th> <th>Apr</th> <th>May</th> <th>Jun</th> <th>Jul</th> <th>Aug</th> <th>Sep</th> <th>Oct</th> <th>Nov</th> <th>Dec</th> </tr> </thead> <tbody> <tr> <td>Mean Rainfall (mm)</td> <td>23.6</td> <td>22.3</td> <td>33.6</td> <td>61.3</td> <td>89.8</td> <td>108.0</td> <td>119.3</td> <td>106.3</td> <td>88.5</td> <td>70.8</td> <td>47.0</td> <td>27.8</td> </tr> <tr> <td>Evap. (mm)</td> <td>220</td> <td>171</td> <td>150</td> <td>91</td> <td>63</td> <td>47</td> <td>49</td> <td>67</td> <td>84</td> <td>106</td> <td>150</td> <td>199</td> </tr> <tr> <td>Evap. Exceeds Rainfall</td> <td>Yes</td> <td>Yes</td> <td>Yes</td> <td>Yes</td> <td>No</td> <td>No</td> <td>No</td> <td>No</td> <td>No</td> <td>Yes</td> <td>Yes</td> <td>Yes</td> </tr> </tbody> </table>			Month	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Mean Rainfall (mm)	23.6	22.3	33.6	61.3	89.8	108.0	119.3	106.3	88.5	70.8	47.0	27.8	Evap. (mm)	220	171	150	91	63	47	49	67	84	106	150	199	Evap. Exceeds Rainfall	Yes	Yes	Yes	Yes	No	No	No	No	No	Yes	Yes	Yes
	Month			Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec																																								
	Mean Rainfall (mm)			23.6	22.3	33.6	61.3	89.8	108.0	119.3	106.3	88.5	70.8	47.0	27.8																																								
Evap. (mm)	220	171	150	91	63	47	49	67	84	106	150	199																																											
Evap. Exceeds Rainfall	Yes	Yes	Yes	Yes	No	No	No	No	No	Yes	Yes	Yes																																											
Exposure	The proposed Land Application Areas (LAA) within the Race Track and Motocross Precincts have a high exposure to sun, with no shade cover and good ventilation.	Nil to Low	Not required																																																				

Site characteristics	Investigations and reporting	Level of constraint	Mitigation measures
Vegetation	The majority of the Site has been previously cleared for agriculture with isolated stands of trees (112.9 ha). The proposed Land Application Area (LAA) is open grassland. Refer to site photographs in the Great Southern Geotechnics (2021) Site Investigation report (Appendix D).	Nil to Low	Maintain grassed area within the LAA
Landform and drainage	The Site is mapped as the following Department of Primary Industries and Regional Development (DPIRD) landscape mapping units (Figure 3, Appendix A): TP01-TP03 – 242KgDMc Sands on laterite on elongate crests. TP04-TP05 – 242ReDMc Sands on laterite on elongate crests. TP06 – Broad valleys in sedimentary in sedimentary rocks; 30 m relief, smooth slopes. Deep sands and iron podzols on slopes.	Nil to Low	Not required
Slope	Slope of land within the site investigation areas for the Race Track Precinct and Motocross Precinct is approximately 6% (Figure 4, Appendix A).	Nil to Low	Diversion of stormwater from upslope around sub-soil irrigation area proposed
Fill (imported)	No imported fill was encountered during the site investigation	Nil to Low	Not required
Surface gravel and rock outcrops	During the Site Investigation, the soil profile (to 2500 mm bgl) was generally found to have Topsoil over Sandy GRAVEL over Sandy CLAY. No rock outcrops were observed within the test pit location areas and gravel soils had approximately 10% coarse fragments (Great Southern Geotechnics, 2021)	Nil to Low	Not required
Erosion potential	The water erosion risk mapped by DPIRD indicates that for test pit locations TP01 – TP05 “<3% of map unit has a high to extreme water erosion risk”. TP06 is mapped as “3-10% of map unit has a high to extreme water erosion risk” (Figure 5, Appendix A). The test pit locations within the Site are currently grassed and considered likely to be Nil or low if sub-soil irrigation is installed and grassed surface is maintained. Refer to photos in the Site Investigation report (Appendix D).	Nil to Low	Maintain as grassed area and divert stormwater from upslope around sub-soil irrigation area to maintain Nil or Low risk rating
Separation from groundwater	During the Site Investigation, undertaken in late June (Appendix D), ground water was not intercepted at 2500 mm bgl at any of the six test pit locations (Figure 4, Appendix A). These locations meet the vertical separation of greater than 2 m separation to groundwater in PDWSA.	Nil to Low	Not required
Public Drinking Water Source Area (PDWSA) and Sewage Sensitive Area (SSA)	The Site is located in a Priority 2 PDWSA – Marbellup Brook Catchment Area and SSA (<1 km from conservation category wetland) (Figure 4, Appendix A).	High	Maintain >2 m vertical separation to groundwater

Site characteristics	Investigations and reporting	Level of constraint	Mitigation measures
Surface waters and separation from water resources	All sub-soil irrigation areas will be located >100 m to Protected Exclusion Area and Marbelup Flats (Conservation Class wetland) (Figure 3, Appendix A).	Nil to Low	Not required
Rainfall run-off and seepage	The test pit location areas, in both the Race Track Precinct and Motocross Precinct, are located on waxing upperslope (UX) (National Committee on Soil and Terrain, 2009). No evidence of evidence of water pooling on the surface or seepage was observed during the Site Investigation (Great Southern Geotechnics, 2021) or during site walkovers undertaken by GHD.	Nil to Low	Diversion of stormwater from upslope around sub-soil irrigation area proposed
Flood potential	The flood erosion risk mapped by DPIRD indicates that test pit locations TP01 – TP05 that “<3% of map unit has a moderate to high flood risk”. TP06 is mapped as “3-10% of map unit has a moderate to high flood risk” (Figure 9, Appendix A).	Nil to Low	Not required
Horizontal setback distances	All sub-soil irrigation areas will be setback >100 m to site boundaries, Protected Exclusion Area and Marbelup Flats (Conservation Class wetland) (Figure 3, Appendix A).	Nil to Low	Not required
Available Land Application Area (LAA)	Sufficient land is available within the Race Track and Motocross Precinct area for sub-soil irrigation of wastewater.	Nil to Low	Not required

## 3.2 Soil assessment

During the Site Investigation, undertaken by Great Southern Geotechnics, three test pits were excavated in each of the Motocross Track Area and Race Track Area. Table 5 includes a summary of the soil physical and chemical characteristics (Appendix E) for SSE at the six test pit locations.

Table 5 Summary of soil physical and chemical characteristics for SSE of the AMP site

Location	Layer depth (mm)	Sample depth (mm)	Soil strata	Depth to GW	Coarse fragments (%)	Soil colour & mottling	Soil field texture	Soil structure	Indicative soil permeability (m/d) ( $K_{sa}^{-1}$ )	Design loading rate (DLR) (mm/d) Trenches and beds			pH	EC (dS/m)	Sodicity (ESP) (%)	Phosphate Sorption Capacity (mg P sorbed/kg)
										Primary treated effluent		Secondary treated effluent				
										Conservative rate	Maximum rate					
<b>Race Track Precinct</b>																
TP01	0-180		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP01	180-490		Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 250 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub-angular, ( F:20% / M:20% / C:15%)	Structureless	>3.0	20	35	50	-	-	-	-
TP01	550-2500	900-1100	Sandy CLAY		NA	Brown/red mottled Light brown/orange (40%)	Light Clay - Low to medium plasticity	Massive	<0.06	NA	NA	8	6.1	0.022	5.8	688
TP02	0-140		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP02	140-400		Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Moderately cemented - Fine to coarse, sub-rounded to sub-angular, ( F:20% / M:20% / C:15%)	Structureless	>3.0	20	35	50	-	-	-	-
TP02	400-1400	500-900	Sandy CLAY		NA	Light brown	Low to medium plasticity	Massive	<0.06	NA	NA	8	6.1	0.025	4.8	1650
TP02	1400-2500		Sandy CLAY		NA	Brown/red mottled Light brown/orange (40%)	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP03	0-250		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey to grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP03	250-830	300-600	Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to medium, sub-rounded to sub-angular, ( F:30% / M:30% )	Structureless	>3.0	20	35	50	5.7	0.028	5.7	3660
TP03	830-1600		Sandy CLAY		NA	Light brown	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP03	1600-2500		Sandy CLAY		NA	Brown/red mottled Light brown/grey (30%)	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-

Location	Layer depth (mm)	Sample depth (mm)	Soil strata	Depth to GW	Coarse fragments (%)	Soil colour & mottling	Soil field texture	Soil structure	Indicative soil permeability (m/d) ( $K_{sa}^{-1}$ )	Design loading rate (DLR) (mm/d)			pH	EC (dS/m)	Sodicity (ESP) (%)	Phosphate Sorption Capacity (mg P sorbed/kg)
										Trenches and beds		Secondary treated effluent				
										Primary treated effluent	Conservative rate					
<b>Motocross Precinct</b>																
TP04	0-220		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP04	220-1250	400-800	Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub-angular, ( F:25% / M:20% / C:10%)	Structureless	>3.0	20	35	50	5.8	0.028	6.2	3000
TP04	1250-1750		Sandy CLAY		NA	Light brown/ orange	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP04	1750-2500		Sandy CLAY		NA	Grey mottled red (30%) & orange (10%).	Low to medium plasticity	Massive	<0.06	NA	NA	8	-	-	-	-
TP05	0-230		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP05	230-880	400-800	SAND with silt		NA	Grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	5.4	0.004	<0.1	<250
TP05	880-2500		Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub-angular, ( F:15% / M:30% / C:10%).	Structureless	>3.0	20	35	50	-	-	-	-
TP06	0-350		(Topsoil) SAND with silt	Not intercepted	Roots and root fibres	Dark grey	Sand - Fine to medium	Structureless	>3.0	20	35	50	-	-	-	-
TP06	350-1200	500-800	Sandy GRAVEL		Contains approximately 10% Cobbles and Boulders in excess of 400 mm diameter	Brown	Gravel and sand - Fine to coarse, sub-rounded to sub-angular, ( F:20% / M:20% / C:10%)	Structureless	>3.0	20	35	50	5.9	0.02	1.4	966
TP06	1200-1800		Sandy GRAVEL			Brown	Gravel and sand - Fine to coarse, sub-rounded to sub-angular, ( F:20% / M:30% / C:10%)	Structureless	>3.0	20	35	50	-	-	-	-
TP06	1800-2500		Sandy GRAVEL			Brown	Gravel and sand - Fine to coarse, sub-rounded to sub-angular, ( F:40% / M:20%)	Structureless	>3.0	20	35	50	-	-	-	-

### 3.3 Site assessment results

Based on an assessment of the soil physical and chemical results for the six test pit locations in Table 5, it is recommended that the LAAs for the Race Track and Motocross Precincts are located at TP01 and TP06, respectively.

- Motocross Precinct (TP06):
  - AS1547 soil type = Gravel
  - Indicative soil permeability (Ksat) = > 3.0 m/d
  - Design irrigation rate = 5 mm/d
- Race Track Precinct (TP01):
  - AS1547 soil type = Light clay
  - Indicative soil permeability (Ksat) = < 0.06 m/d
  - Design irrigation rate = 3 mm/d

As per the DOHWA (2021) guidance, a Level of Constraint (Low, Moderate or High) is determined by applying a risk assessment to each site characteristic and the following mitigation measures may be applied:

- Nil or Low
  - *If all constraints are Low, standard designs are generally satisfactory and no mitigation measures are required.*
- Moderate
  - *For each Moderate constraint an appropriate mitigation measure or design modification over and above that of a standard design, should be outlined.*
- High
  - *Any High constraint might prove an impediment to successful on-site wastewater management, or alternatively will require in-depth investigation and incorporation of sophisticated mitigation measures in the design to permit compliant onsite wastewater management.*

A summary of site assessment results, including the level of constraint for each characteristic, within the Motocross Precinct in Table 6 and Race Track Precinct is outlined in Table 7.

#### 3.3.1 Motocross Precinct

A summary of site assessment results for SSE for the recommended LAA within the Motocross Precinct (TP06) has been provided in Table 6.

**Table 6** Summary of site assessment results for SSE of the proposed LAA within the Motocross Precinct (TP06)

Characteristic	Level of Constraint			Results for TP06	Assessed Level of Constraint for Site
	Nil or Low	Moderate	High		
<b>General Characteristics</b>					
Climate (difference between average annual rainfall and average pan evaporation, mm/year)	Excess of evaporation over rainfall in the wettest months	Rainfall approximates to evaporation	Excess of rainfall over evaporation in the wettest months	Rainfall in excess of evaporation from May to September	<b>High</b>
Exposure to sun and wind	Full sun and/or high wind or minimal shading and North / North-East	Dappled light East / West / South-East / South-West aspect	Limited patches of light and little wind to heavily shaded all day and South aspect	Full sun	<b>Nil or Low</b>

Characteristic	Level of Constraint			Results for TP06	Assessed Level of Constraint for Site
	Nil or Low	Moderate	High		
	/North-West aspect				
Vegetation coverage over the site	Plentiful vegetation with healthy growth and good potential for nutrient uptake Turf or pasture	Limited variety of vegetation	Sparse vegetation or no vegetation, dense forest with little understorey	Good cover of existing pasture	<b>Nil or Low</b>
Landslip (or landslip potential)	Nil	Low to moderate	High or Severe	No landslip evident	<b>Nil or Low</b>
Slope Form (affects water shedding ability)	Hill crests, convex or divergent side-slopes and plains	Straight side-slopes and footslopes	Floodplains, concave or convergent side-slopes and incised channels	Straight waxing upslope (UX)	<b>Moderate</b>
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	<b>Nil or Low</b>
<b>Slope gradient (%)</b>					
(a) for absorption trenches and beds	<5%	5-15%	>15%	Approximately 6%	<b>Moderate</b>
(b) for surface/subsurface irrigation	<10%	10-20%	>20%	Approximately 6%	<b>Nil or Low</b>
Erosion (or potential for erosion)	Nil or Low	Moderate	Severe	Good cover of existing pasture, upslope stormwater diversion and sub-surface irrigation proposed	<b>Nil or Low</b>
Fill (imported)	No fill at present or fill is good quality topsoil or minimal fill required	Moderate coverage and good quality fill	Extensive poor-quality fill and variable quality fill	No fill at present	<b>Nil or Low</b>
Flood frequency (AEP)	Less than 1 in 100 years	Between 100 and 20 years	More than 1 in 20 years	Less than 1 in 100 years	<b>Nil or Low</b>
Private bore used for household/drinking water purposes	No bores onsite or on neighbouring properties	>30 m to the nearest private bore	<30 m to the nearest private bore	APEC bores located >30 m	<b>Moderate</b>
Proximity to water resources	>100 m	<100 m but reduced setback is supported (refer to Section 5.2.2 of the GSP)	<100 m and reduced setback is not supported (refer to Section 5.2.2 of the GSP)	>100 m to Protected Exclusion Area and Marbellup Flats	<b>Nil or Low</b>

Characteristic	Level of Constraint			Results for TP06	Assessed Level of Constraint for Site
	Nil or Low	Moderate	High		
Public Drinking Water Source Areas (PDWSA) and Sewage Sensitive Areas (SSA)	Site not located within a PDWSA or SSA	Site located within a PDWSA or SSA	Site located within both a PDWSA and SSA	Priority 2 PDWSA – Marbellup Brook Catchment Area SSA (<1 km from conservation category wetland)	<b>High</b>
Groundwater (wettest time of the year)	>2 m	2.0 – 0.6 m need for fill to achieve setbacks listed in Appendix 1	<0.6 m fill is not practical to achieve setbacks listed in Appendix 1	Groundwater not intercepted >2.5 m	<b>Nil or Low</b>
Land area available for LAA	Exceeds the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Meets the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Insufficient area available for LAA as per AS1547 or Schedule 2 of the GSP	550 m <sup>2</sup> available for sub-surface irrigation	<b>Nil or Low</b>
Rock outcrops (% of surface)	<10%	10-20%	>20%	No rock outcrops observed	<b>Nil or Low</b>
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit.	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	<b>Nil or Low</b>
Stormwater run-on/run-off	Low likelihood of stormwater run-on/run-off	Moderate likelihood of stormwater run-on/run-off, need for diversionary structures	High likelihood of inundation by stormwater run-on/run-off, diversion not practical	Upslope stormwater diversion proposed	<b>Nil or Low</b>
<b>Soil profile characteristics</b>					
Soil permeability Category (AS1547)	2 and 3	4 and 5	1 and 6	1	<b>High</b>
Profile depth	>2 m	2.0-1.0	< 1.0 m	2.5 m bgl	<b>Nil or Low</b>
Hardpan or bedrock	>1.5 m	1.5-0.6 m Special design requirements and distribution techniques or soil modification will be necessary, depends on quality of treated wastewater and type of LAS	<0.6 m	Sandy GRAVEL encountered to 2.5 m bgl	<b>Nil or Low</b>
Presence of mottling	None	Moderate	Extensive	None	<b>Nil or Low</b>
Coarse fragments	< 10%	10-40%	>40%	10% Cobbles and boulders in excess of 400 mm diameter	<b>Nil or Low</b>

Characteristic	Level of Constraint			Results for TP06	Assessed Level of Constraint for Site
	Nil or Low	Moderate	High		
pH	6.0 - 8.0	4.5 – 6.0	<4.5, >8	5.9 - pH between <5 and >8 therefore likely to be suitable for plant growth	<b>Moderate</b>
Electrical Conductivity (ECe)(dS/m)	<0.3	0.3 - 2	>2	0.02	<b>Nil or Low</b>
Sodicity ESP%	<3	3.0 - 8.0	>8	1.4	<b>Nil or Low</b>
Phosphorus adsorption (mg/kg)	>500	200-500	<200	966	<b>Nil or Low</b>

### 3.3.2 Race Track Precinct

A summary of site assessment results for SSE for the recommended LAA within the Race Track Precinct (TP01) has been provided in Table 7.

**Table 7** Summary of site assessment results for SSE of the proposed LAA within the Race Track Precinct (TP01)

Characteristic	Level of Constraint			Results for TP01	Assessed Level of Constraint for Site
	Nil or Low	Moderate	High		
<b>General Characteristics</b>					
Climate (difference between average annual rainfall and average pan evaporation, mm/year)	Excess of evaporation over rainfall in the wettest months	Rainfall approximates to evaporation	Excess of rainfall over evaporation in the wettest months	Rainfall in excess of evaporation from May to September	<b>High</b>
Exposure to sun and wind	Full sun and/or high wind or minimal shading and North / North-East /North-West aspect	Dappled light East / West / South-East / South-West aspect	Limited patches of light and little wind to heavily shaded all day and South aspect	Full sun	<b>Nil or Low</b>
Vegetation coverage over the site	Plentiful vegetation with healthy growth and good potential for nutrient uptake Turf or pasture	Limited variety of vegetation	Sparse vegetation or no vegetation, dense forest with little understorey	Good cover of existing pasture	<b>Nil or Low</b>
Landslip (or landslip potential)	Nil	Low to moderate	High or Severe	No landslip evident	<b>Nil or Low</b>
Slope Form (affects water shedding ability)	Hill crests, convex or divergent side-slopes and plains	Straight side-slopes and footslopes	Floodplains, concave or convergent side-slopes and incised channels	Straight waxing upperslope (UX)	<b>Moderate</b>

Characteristic	Level of Constraint			Results for TP01	Assessed Level of Constraint for Site
	Nil or Low	Moderate	High		
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	<b>Nil or Low</b>
<b>Slope gradient (%)</b>					
(a) for absorption trenches and beds	<5%	5-15%	>15%	Approximately 6%	<b>Moderate</b>
(b) for surface/subsurface irrigation	<10%	10-20%	>20%	Approximately 6%	<b>Nil or Low</b>
Erosion (or potential for erosion)	Nil or Low	Moderate	Severe	Good cover of existing pasture, upslope stormwater diversion and sub-surface irrigation proposed	<b>Nil or Low</b>
Fill (imported)	No fill at present or fill is good quality topsoil or minimal fill required	Moderate coverage and good quality fill	Extensive poor-quality fill and variable quality fill	No fill at present	<b>Nil or Low</b>
Flood frequency (AEP)	Less than 1 in 100 years	Between 100 and 20 years	More than 1 in 20 years	Less than 1 in 100 years	<b>Nil or Low</b>
Private bore used for household/drinking water purposes	No bores onsite or on neighbouring properties	>30 m to the nearest private bore	<30 m to the nearest private bore	APEC bores located >30 m	<b>Moderate</b>
Proximity to water resources	>100 m	<100 m but reduced setback is supported (refer to Section 5.2.2 of the GSP)	<100 m and reduced setback is not supported (refer to Section 5.2.2 of the GSP)	>100 m to Protected Exclusion Area and Marbellup Flats	<b>Nil or Low</b>
Public Drinking Water Source Areas (PDWSAs) and Sewage Sensitive Areas (SSA)	Site not located within a PDWSA or SSA	Site located within a PDWSA or SSA	Site located within both a PDWSA and SSA	Priority 2 PDWSA – Marbellup Brook Catchment Area and SSA (<1 km from conservation category wetland)	<b>High</b>
Groundwater (wettest time of the year)	>2 m	2.0 – 0.6 m need for fill to achieve setbacks listed in Appendix 1	<0.6 m fill is not practical to achieve setbacks listed in Appendix 1	Groundwater not intercepted >2.5 m	<b>Nil or Low</b>
Land area available for LAA	Exceeds the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Meets the minimum required LAA size of AS1547 or Schedule 2 of the GSP	Insufficient area available for LAA as per AS1547 or Schedule 2 of the GSP	Sufficient area available for sub-surface irrigation	<b>Nil or Low</b>
Rock outcrops (% of surface)	<10%	10-20%	>20%	No rock outcrops observed	<b>Nil or Low</b>

Characteristic	Level of Constraint			Results for TP01	Assessed Level of Constraint for Site
	Nil or Low	Moderate	High		
Site Drainage (qualitative)	No visible signs or likelihood of dampness, even in wet season	Some signs or likelihood of dampness Moist soil but no standing water in soil pit.	Wet soil, moisture-loving plants, standing water in pit; water ponding on surface	No visible signs or likelihood of dampness, even in wet season	<b>Nil or Low</b>
Stormwater run-on/run-off	Low likelihood of stormwater run-on/run-off	Moderate likelihood of stormwater run-on/run-off, need for diversionary structures	High likelihood of inundation by stormwater run-on/run-off, diversion not practical	Upslope stormwater diversion proposed	<b>Nil Low</b>
<b>Soil profile characteristics</b>					
Soil permeability Category (AS1547)	2 and 3	4 and 5	1 and 6	5	<b>Moderate</b>
Profile depth	>2 m	2.0-1.0	< 1.0 m	2.5 m bgl	<b>Nil or Low</b>
Hardpan or bedrock	>1.5 m	1.5-0.6 m Special design requirements and distribution techniques or soil modification will be necessary, depends on quality of treated wastewater and type of LAS	<0.6 m	Sandy CLAY intercepted at 550 mm bgl	<b>High</b>
Presence of mottling	None	Moderate	Extensive	Sandy CLAY mottled	<b>Moderate</b>
Course fragments	< 10%	10-40%	>40%	10% Cobbles and boulders in excess of 250 mm diameter	<b>Nil or Low</b>
pH	6.0 - 8.0	4.5 – 6.0	<4.5, >8	6.1	<b>Nil or Low</b>
Electrical Conductivity (ECe)(dS/m)	<0.3	0.3-2	>2	0.022	<b>Nil or Low</b>
Sodicity Exchangeable sodium percentage (ESP%)	<3	3.0 - 8.0	>8	5.8 – no evidence of dispersion, slaking, or structural decline	<b>Moderate</b>
Phosphorus adsorption (mg/kg)	>500	200-500	<200	688	<b>Nil or Low</b>

### 3.3.3 Mitigation measures

The majority of constraints assessed in 3.3.1 and 3.3.1 were found to be Nil or Low, however several key constraints were found to be High or Moderate. Proposed mitigation measures for the aspects which are considered to have a High or Moderate constraint within the Race Track Precinct and Motocross Precinct are included in Table 8.

Table 8 Proposed mitigation measures for High and Moderate constraints

Constraints		
Race Track Precinct	Motocross Precinct	Proposed mitigation measures
<b>High</b>		
Climate - Rainfall in excess of evaporation from May to September		Diversion of stormwater from upslope around sub-soil irrigation area
Priority 2 PDWSA – Marbellup Brook Catchment Area and SSA (<1 km from conservation category wetland)		The proposed LAA achieves a 2 m vertical separation to groundwater
Hardpan or bedrock <0.6 m - Sandy CLAY intercepted at 550 mm bgl	-	Amend soils in LAA
-	Soil permeability Category (AS1547) – (1) Gravels and sands	Accommodate permeability via Design Loading Rates (DLRs) and Design Irrigation Rates (DIRs)
<b>Moderate</b>		
Slope Form (affects water shedding ability) – Straight waxing upslope		Diversion of stormwater from upslope around sub-soil irrigation area
Slope gradient (%) (a) for absorption trenches and beds – 5-15%		No absorption trenches or beds proposed
APEC bores located >30 m		APEC bore located 250 m away – no modification considered necessary
Presence of mottling - Sandy CLAY mottled	-	Amend soils in potential LAA
Soil permeability Category (AS1547) – (5) Light clay	-	Accommodate permeability via Design Loading Rates (DLRs) and Design Irrigation Rates (DIRs)
Sodicity ESP – 5.8%	-	No evidence of dispersion, slaking or structural decline in the soils on or near the potential LAA
-	pH 5.9	No evidence of scald or bare areas on or near the potential LAA

## 4. Wastewater management system type and design

### 4.1 Specific assessment SSE – Sizing for treatment system and land application area

The sizing for a wastewater treatment system and LAA has been developed in this SSE report for Stage 1A in the Motocross Precinct only.

As per the requirements of the Department of Water *WQPN 100* (DoW, 2007) and the *Government Sewerage Policy* (DPLH, 2019) a 'Secondary' wastewater treatment plant, with engineering certification to meet effluent quality of Biological Oxygen Demand (BOD) < 20 mg/L; Total Suspended Solids (TSS) < 30 mg/L; Total Nitrogen (TN) < 10 mg/L; Total Phosphorus (TP) < 1 mg/L; and *Escherichia coli* < 10 cfu/100mL is required in a Priority 2 PDWSA.

It is recommended to install a 'Secondary' treatment system, with nutrient removal such as Aquarius Wastewater Systems Pty Ltd, which provide DOHWA approved systems. An example of the type of system that would meet the requirement of a 'Secondary' treatment system is provided in Appendix F. These systems have a nutrient reduction capability of which includes reduction of TN to < 10 mg/L and TP to < 1 mg/L and are certified to AS1546.3:2008.

#### 4.1.1 Water balance

A water balance has been developed for the operation of the wastewater system, as per the water balance in the DOHWA (2021) guidance, for Stage 1A of the AMP development in the Motocross Precinct and included in Appendix B.

The water balance has been developed based on the following:

- A design wastewater flow of 3,500 L/day (average of 100 persons and 15,000 L storage tank)
- Design irrigation rate for sub-surface irrigation of 5.0 mm/day
- Rainfall run-off factor of 0.9
- Mean monthly rainfall levels at the Albany Airport Comparison weather station (BoM, 2021)
- Pan evaporation data (DPIRD, 1987)

The results of the water balance for the Motocross Precinct, for an average of 100 persons/day, indicate that 1,100 m<sup>2</sup> will be required for the sub-soil irrigation area. There is adequate area of land available within the vicinity of TP06 to accommodate the site of the required LAA.

## 4.2 Siting and configuration of the Land Application Area

### 4.2.1 Setback distances

Based on an assessment of the soil physical and chemical results for the six test pit locations in Table 5, it is recommended that the LAAs for the Race Track and Motocross Precincts are located at TP01 and TP06, respectively.

All sub-soil irrigation areas will be located >100 m to Protected Exclusion Area and Marbelup Flats (Conservation Class wetland) (Figure 3, Appendix A).

The sub-soil irrigation area will be fenced and will be separate from the activities within the Precinct to maintain public amenity.

## 4.2.2 Stormwater management

Stormwater management will include diversion drains, water treatment areas and attenuation basins to control stormwater across the Race Track Precinct and Motocross Precinct as per the Stormwater Management Plan (GHD, 2021) prepared for the Development Application for the AMP.

## 5. Monitoring, operation and maintenance

Baseline groundwater and surface water quality sampling of the Site was undertaken by Bio Diverse Solutions in 2018 and 2019 (Bio Diverse Solutions, 2018). DWER has been consulted during the development of the Site Local Water Management Strategy (LWMS) (GHD, 2021) as part of the Scheme Amendment process. The following surface and groundwater pre-development, construction and post-development monitoring is outlined as per the approved LWMS.

### 5.1 Surface water monitoring

#### 5.1.1 Pre-development and construction monitoring

Ongoing quarterly monitoring of existing Site surface water conditions shall be continued prior to development, and during construction of the AMP as per the Local Water Management Strategy approved by DWER as part of the Scheme Amendment process.

In combination with the existing 2018 and 2019 data, the ongoing monitoring will be used as a baseline for ongoing assessment of the potential impact of the development on shallow groundwater and surface water quality. Additionally, pre-development water monitoring data will be used to identify water quality trigger levels at which a response is required.

For surface water monitoring during the construction phase of the development, a CEMP shall be prepared by the Contractor which will include erosion and sedimentation control measures, as well as drainage and dewatering systems (if required) in order to minimise potential pollution impacts and prevent contamination to surface water and groundwater.

#### 5.1.2 Post-development monitoring

Ongoing monthly monitoring of surface water conditions shall be continued post-development (for the duration of the operation of the facility), with continued monitoring at sites CS01 and CS02, and establishment of a new upstream monitoring location. Additional sampling shall also be undertaken in response to any spill events.

The post-development monitoring program will also involve the collection of grab samples from the compensating basins. Sampling of basins should comprise 3-4 events per year, during or immediately following significant rainfall events (1EY, 1 year ARI event). It is assumed the first flush events will have the highest level of nutrients and chemicals, therefore sampling should occur at the time/after the first significant rainfall event of each wet season, and after extended dry periods. Field notes should include details of the rainfall events, site conditions, time of sampling and time of sample testing.

Monitoring of the compensation basin inlet and outlet water quality will be used to assess performance of the basins in improving stormwater quality.

Annual water monitoring reports shall be submitted to DWER and the Water Corporation. A water quality response and contingency plan will be prepared and provided to the Water Corporation, City of Albany and DWER for advice.

### 5.1.3 Monitoring program summary

The recommended monitoring parameters for the ongoing pre-development, construction and post-development monitoring program are outlined in Table 9.

Table 9 Summary of surface water monitoring

Site	Frequency	Duration	Parameters
<b>Surface water</b> - Upstream of the site (TBC) - Mid-stream (CS02) - Downstream of the site (CS01)	Monthly	Ongoing, with annual reporting	In-situ: pH, EC, temperature Unfiltered sample: pH, EC, TN, FRP, TKN, ammonia, TP, TRH, PAH, BTEXN, Surfactants, microbial analysis Filtered sample: Filtered total nitrogen and filtered total phosphorus (to quantify organic component), NO <sub>2</sub> /NO <sub>3</sub> , PO <sub>4</sub> , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)
<b>Compensating basin</b> - Inlet (4 No.) - Outlet (4 No.)	3-4 events per year following 1EY rainfall events		

## 5.2 Groundwater monitoring

### 5.2.1 Pre-development and construction monitoring

Ongoing monitoring of existing Project Site shallow groundwater conditions shall be continued prior to development, and during construction of the AMP. In combination with the existing 2018 and 2019 data, the ongoing monitoring will be used as a baseline for ongoing assessment of the potential impact of the development on shallow groundwater and surface water quality.

Additionally, pre-development water monitoring data will be used to identify water quality trigger levels at which a response is required.

### 5.2.2 Post-development monitoring

A groundwater monitoring network should be established post development, the locations of which will be based on groundwater monitoring strategy.

Ongoing monitoring of the groundwater monitoring bores shall be conducted for the duration of the operation of the facility and in accordance with the groundwater monitoring program in Table 10.

Annual water monitoring reports will be submitted to DWER and the Water Corporation.

A water quality response and contingency plan will be prepared and provided to the Water Corporation, City of Albany and DWER for advice.

In addition if the development proposal seeks a licence to take water and approval to install a production bore for abstraction of groundwater as a water supply source for the development, then six-monthly groundwater monitoring for water levels and salinity will be a required.

### 5.2.3 Monitoring program summary

The program and parameters outlined in Table 10 will provide a suitable representation of groundwater quality at the site. The groundwater bores established for pre-development monitoring will be used for construction phase and incorporated into the post-development monitoring network.

**Table 10** Summary of groundwater monitoring

Site	Frequency	Duration	Parameters
Monitoring bores Production bore	Monthly	Pre-development, during construction, on-going throughout the life of development.	Water level  In-situ: pH, EC, temperature Unfiltered sample: pH, EC, TN, FRP, TKN, ammonia, TP, TRH, PAH, BTEXN, Surfactants, microbial analysis Filtered sample: Filtered total nitrogen and filtered total phosphorus (to quantify organic component), NO <sub>2</sub> /NO <sub>3</sub> , PO <sub>4</sub> , dissolved heavy metals (As, Cd, Cr, Cu, Pb, Ni, Zn, Hg)

### 5.2.4 Contingency measures

Pre-development water monitoring data shall be used to identify water quality trigger levels at which a management response is required. A water quality response and contingency plan shall be included in the surface and groundwater monitoring plans.

In the event of a major water quality incident at the Site, it is recommended that increased monitoring be undertaken to quantify if there is any impact to surface and groundwater quality. Contingency monitoring and response measures shall be developed in consultation with DWER and documented in the post-development monitoring program.

Potential incidents due to system failure and/ or mechanical breakdown during operation and maintenance of the installed system shall be addressed, as required, as per the manufacturer and installation instructions.

## 6. Conclusion and recommendations

The SSE report for the AMP site involved evaluation of site and soil, physical and chemical properties, to identify appropriate onsite effluent disposal LAAs within the Race Track Precinct and Motocross Precinct. Based on an assessment of the soil physical and chemical results for the six test pit locations, it is recommended that the LAAs for the Race Track Precinct and Motocross Precinct are located at TP01 and TP06, respectively.

The sizing for a wastewater treatment system and LAA has been developed in this SSE report for Stage 1A in the Motocross Precinct only.

The proposed clubhouse within the Motocross Precinct will be constructed in Stage 1A of the development. It is anticipated that this will be an unlicensed facility (15 L/ person/ day) however provision has been made for anticipated wastewater volumes for a licensed facility (35 L/ person/ day), to allow for possible increased loading at the site if it were to become a licensed facility.

The Motocross Precinct clubhouse is expected to have intermittent use throughout the Motocross season and on a weekly basis, with up to 300 patrons on Sunday or Saturday followed by minimal usage during the week and off-season downtime. Therefore, for the purpose of calculating anticipated wastewater volumes it is assumed that there is an average of 100 people/ day.

In order to accommodate spikes in wastewater volumes on event days when there is up to 300 patrons using the Motocross Precinct clubhouse facilities, it is proposed to install a 15,000 L holding tank, to balance storage over the course of a typical week.

The results of a water balance for the Motocross Precinct, for an average of 100 persons/day, indicate that 1,100 m<sup>2</sup> will be required for the sub-soil irrigation area. There is adequate area of land available within the vicinity of TP06 to accommodate the site of the required LAA.

As per the requirements of the Department of Water *WQPN 100* (DoW, 2007) and the *Government Sewerage Policy* (DPLH, 2019) a 'Secondary' wastewater treatment plant, with engineering certification to meet effluent quality of Biological Oxygen Demand (BOD) < 20 mg/L; Total Suspended Solids (TSS) < 30 mg/L; Total Nitrogen (TN) < 10 mg/L; Total Phosphorus (TP) < 1 mg/L; and *Escherichia coli* < 10 cfu/100mL is required in a Priority 2 PDWSA.

It is recommended that a DOHWA approved 'Secondary' treatment system, certified to AS1546.3:2008, is selected and installed for the Motocross Precinct during Stage 1A of development.

At time of writing, an onsite effluent disposal system was not proposed to be installed in the Race Track Precinct. All liquid waste from transportable buildings, toilets and washdown facilities is proposed to be removed offsite, as required, by an approved contractor. If onsite effluent disposal is proposed in the future is it expected a similar system, with holding tank, will be utilised to manage spikes in wastewater volumes for events and off-season downtime.

In addition it is recommended, as per the DOHWA (2021) guidelines, that the following is undertaken:

- *Have a suitably qualified maintenance contractor service the secondary and advanced secondary treatment system every three months, as required by Council under the approval to operate.*
- *Annual inspections should be undertaken on treatment tanks and desludging undertaken on annual, two yearly or four yearly cycles depending on the size of the tank installed.*
- *All land application systems should be sited in an area that will not be frequented by vehicle or foot traffic or will not be built on or covered with paved over.*
- *Any subsurface irrigation areas should be vegetated (i.e. with grass that can be mown regularly) to encourage growth and maximise nutrient uptake.*
- *Irrigation lines should be maintained as per manufacturer's instructions (e.g. flushing).*
- *Stormwater and surface run-on should be diverted around, or away from, land application areas.*

- *Landowners should be cognisant of the operation of their system and monitor the treatment and land application area to identify any potential issues (e.g. insufficient septic treatment, clogging of the system, pooling of treated effluent).*
- *The volume of wastewater produced should remain the same and not exceed the operational capacity of the system, it will ensure the effective long-term operation of the systems*
- *Chemicals, large quantities of cleaning products, fats, oils and grease, and food scraps should not be discharged to the wastewater treatment and disposal system, as they risk overloading or interfering with the functioning of the system.*

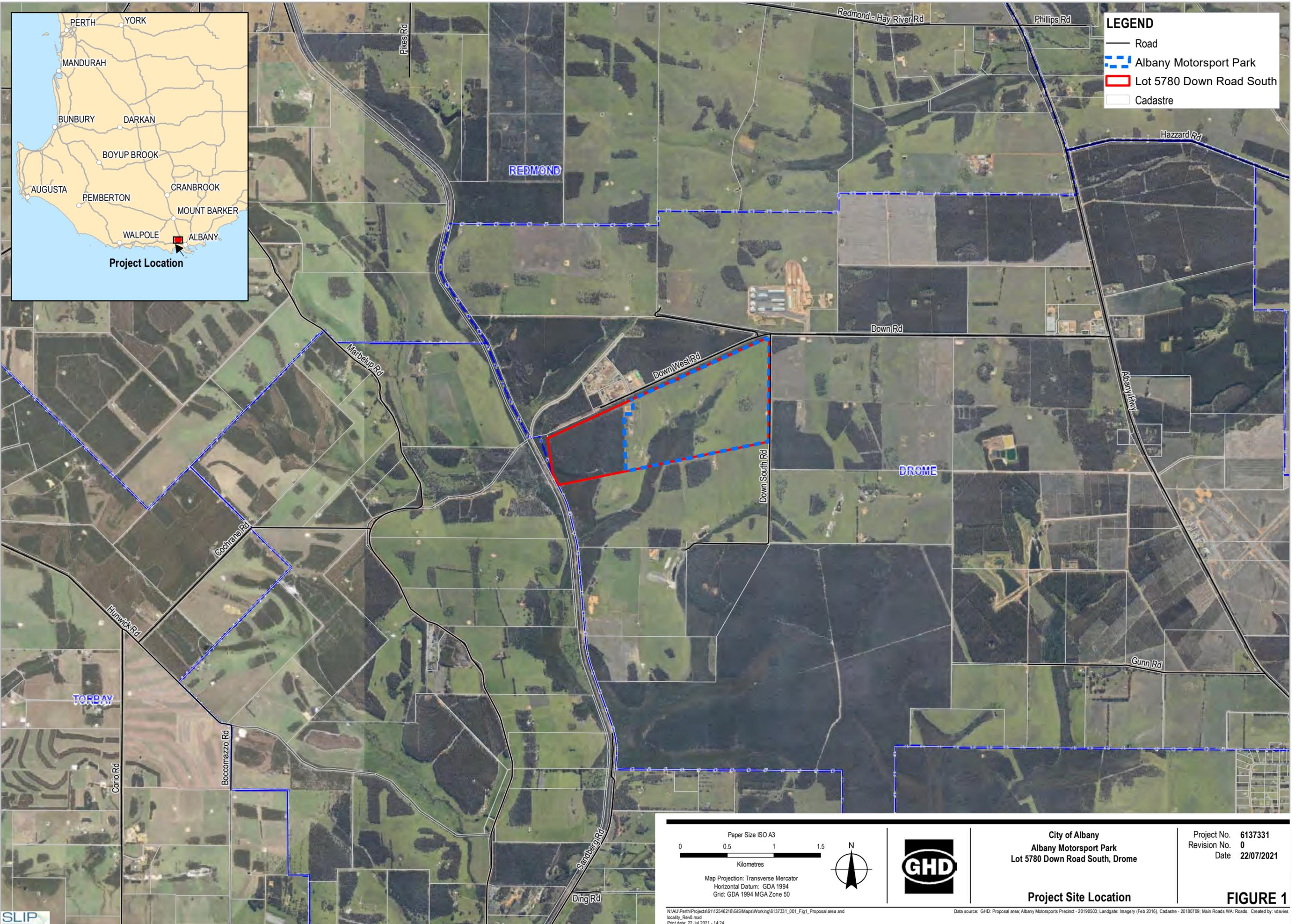
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# Appendix A

## Figures

- Figure 1*      *Project Site Location*
- Figure 2*      *Albany Motorsport Park Master Plan – Stage 1 (Roberts Gardiner Architects, 2021)*
- Figure 3*      *DPIRD Soil Landscape Mapping Units and Test Pit Locations*
- Figure 4*      *Groundwater Conditions, Topography and Test Pit Locations*
- Figure 5*      *Water Erosion Risk (DPIRD-013)*
- Figure 6*      *Hydrology and Hydrogeology*
- Figure 7*      *PDWSA and Water Management Areas*
- Figure 8*      *Master Plan – 100 m Setback to Protected Exclusion Area and Marbellup Flats (Conservation Class)*
- Figure 9*      *Flood Risk (DPIRD-007)*



**LEGEND**

- Road
- ▬▬▬ Albany Motorsport Park
- ▭ Lot 5780 Down Road South
- ▭ Cadastre



Paper Size ISO A3

0 0.5 1 1.5

Kilometres

Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50



City of Albany  
 Albany Motorsport Park  
 Lot 5780 Down Road South, Drome

Project No. 6137331  
 Revision No. 0  
 Date 22/07/2021

**Project Site Location**

**FIGURE 1**

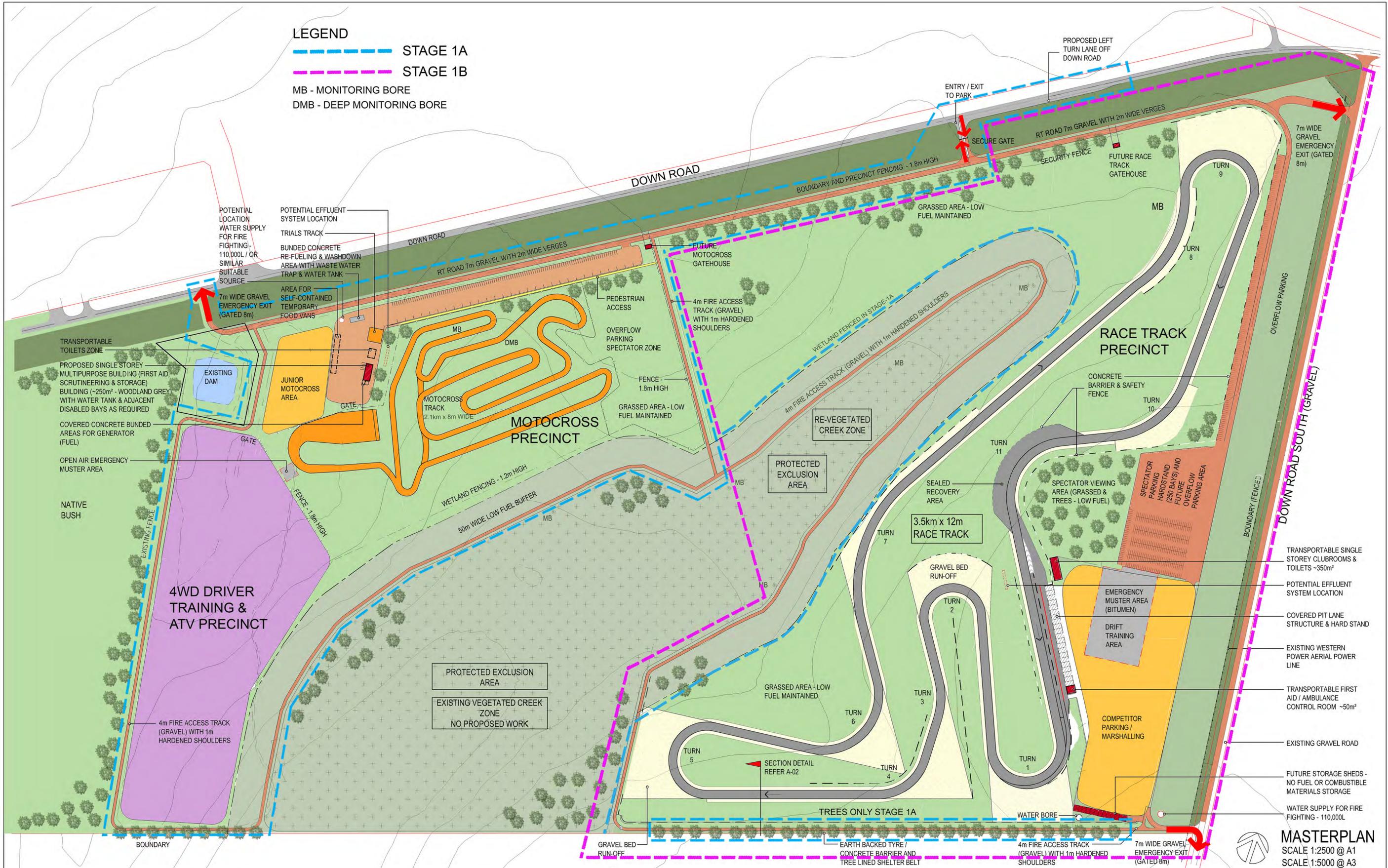
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Data source: GHD: Proposal area; Albany Motorsports Precinct - 20190503; Landgate: Imagery (Feb 2016); Cadastre - 20180709; Main Roads WA: Roads. Created by: vdavies



**LEGEND**

- STAGE 1A
- STAGE 1B
- MB - MONITORING BORE
- DMB - DEEP MONITORING BORE



**MASTERPLAN**  
 SCALE 1:2500 @ A1  
 SCALE 1:5000 @ A3

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rev	date	description
A	15-04-2021	ISSUED FOR CLIENT REVIEW
B	27-04-2021	ISSUED FOR CLIENT REVIEW
C	12-05-2021	ISSUED FOR CLIENT REVIEW
D	26-05-2021	ISSUED FOR CLIENT REVIEW
E	05-07-2021	ISSUED FOR DA

p.o. box 1502, albany, western australia 6331  
 telephone: (08) 9841 5455  
 email: admin@rgarchitects.com.au

**Roberts Gardiner**  
**Architects**

project  
**Albany Motorsport Park**  
 Lot 5780 Down Rd, Drome, WA 6330  
 client  
 City of Albany

Masterplan - Stage 1

cad file

drawn CB project number 21-002

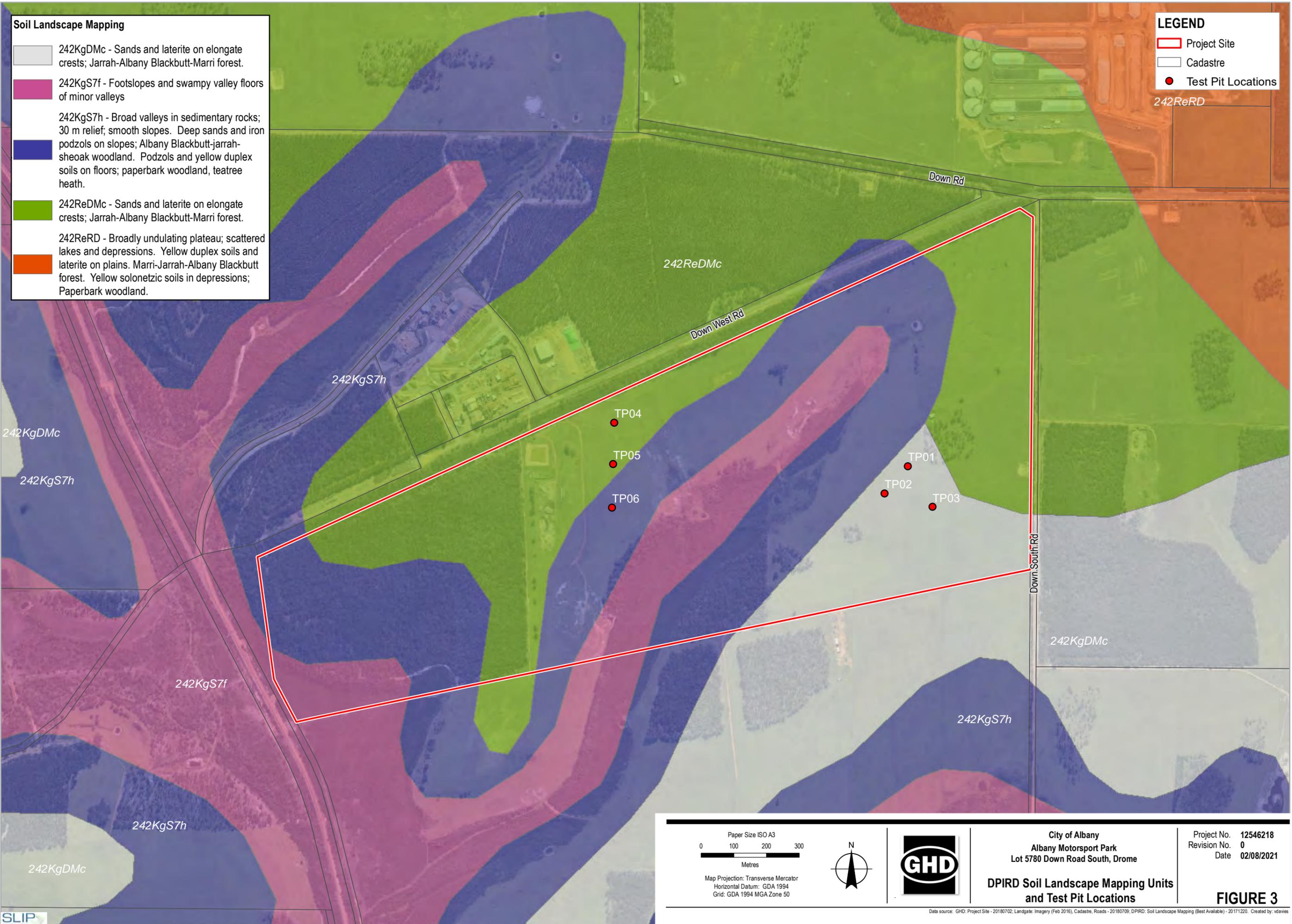
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 dwg no. **A-01** rev. **E**

**Soil Landscape Mapping**

- 242KgDMc - Sands and laterite on elongate crests; Jarrah-Albany Blackbutt-Marri forest.
- 242KgS7f - Foothlopes and swampy valley floors of minor valleys
- 242KgS7h - Broad valleys in sedimentary rocks; 30 m relief; smooth slopes. Deep sands and iron podzols on slopes; Albany Blackbutt-jarrah-sheoak woodland. Podzols and yellow duplex soils on floors; paperbark woodland, teatree heath.
- 242ReDMc - Sands and laterite on elongate crests; Jarrah-Albany Blackbutt-Marri forest.
- 242ReRD - Broadly undulating plateau; scattered lakes and depressions. Yellow duplex soils and laterite on plains. Marri-Jarrah-Albany Blackbutt forest. Yellow solonetzic soils in depressions; Paperbark woodland.

**LEGEND**

- Project Site
- Cadastre
- Test Pit Locations

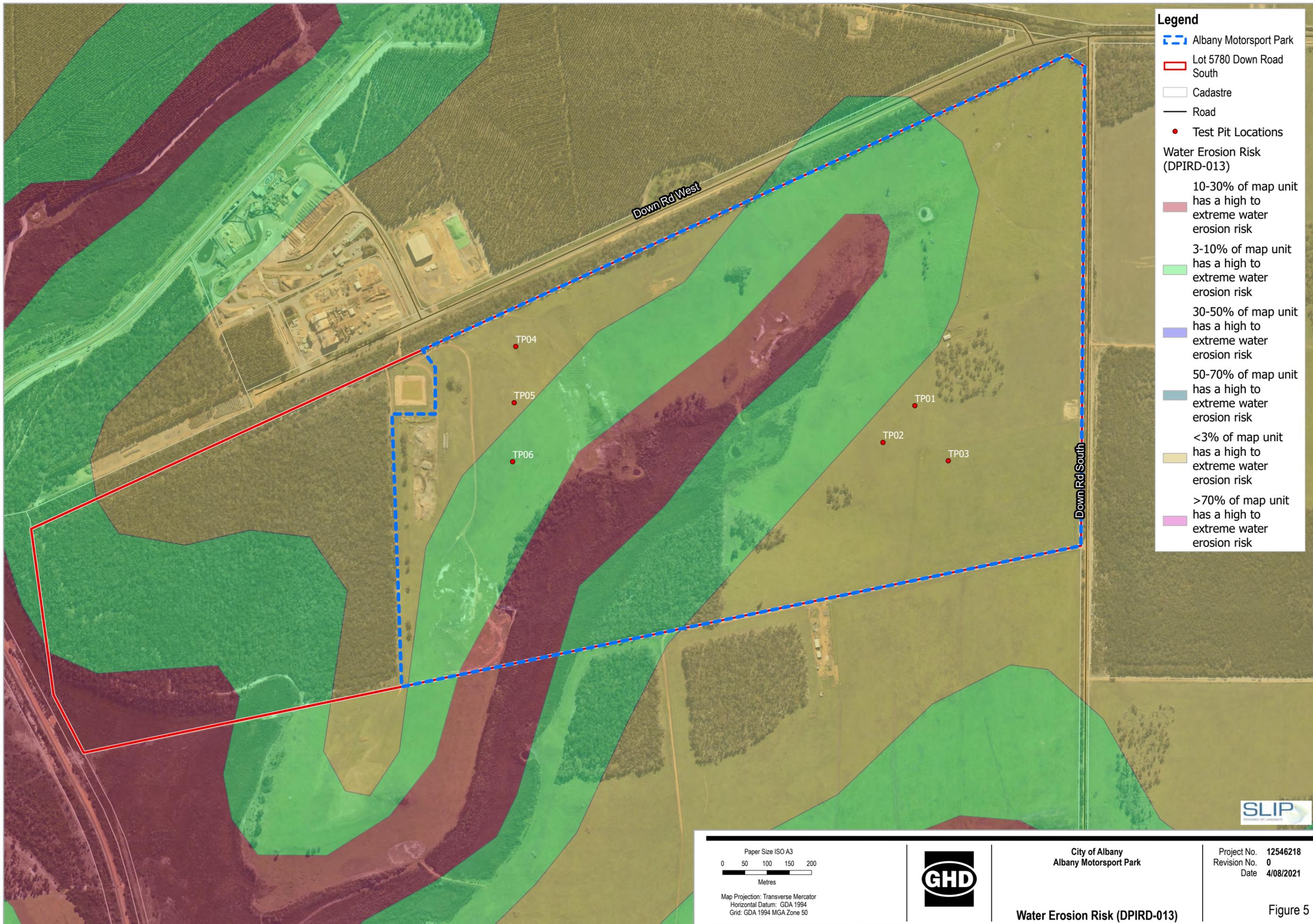


Paper Size ISO A3 0 100 200 300 Metres Map Projection: Transverse Mercator Horizontal Datum: GDA 1994 Grid: GDA 1994 MGA Zone 50			City of Albany Albany Motorsport Park Lot 5780 Down Road South, Drome	Project No. 12546218 Revision No. 0 Date 02/08/2021
			<b>DPIRD Soil Landscape Mapping Units and Test Pit Locations</b>	<b>FIGURE 3</b>

Data source: GHD: Project Site - 20180702; Landgate: Imagery (Feb 2016), Cadastre, Roads - 20180709; DPIRD: Soil Landscape Mapping (Best Available) - 20171220. Created by: vdavies







**Legend**

- - - Albany Motorsport Park
- Lot 5780 Down Road South
- Cadastre
- Road
- Test Pit Locations

**Water Erosion Risk (DPIRD-013)**

- 10-30% of map unit has a high to extreme water erosion risk
- 3-10% of map unit has a high to extreme water erosion risk
- 30-50% of map unit has a high to extreme water erosion risk
- 50-70% of map unit has a high to extreme water erosion risk
- <3% of map unit has a high to extreme water erosion risk
- >70% of map unit has a high to extreme water erosion risk

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Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50



City of Albany  
 Albany Motorsport Park

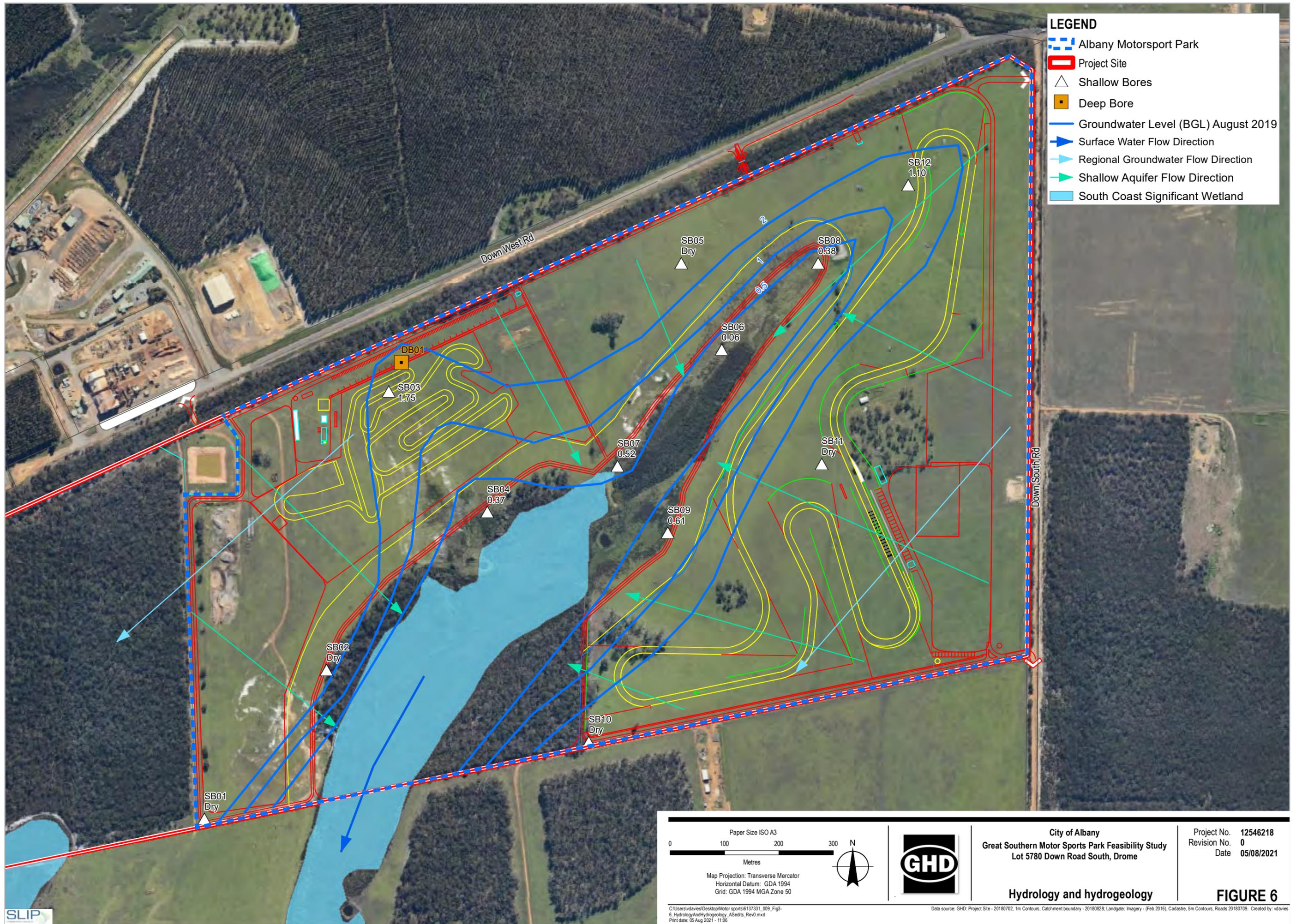
**Water Erosion Risk (DPIRD-013)**

Project No. 12546218  
 Revision No. 0  
 Date 4/08/2021

Figure 5

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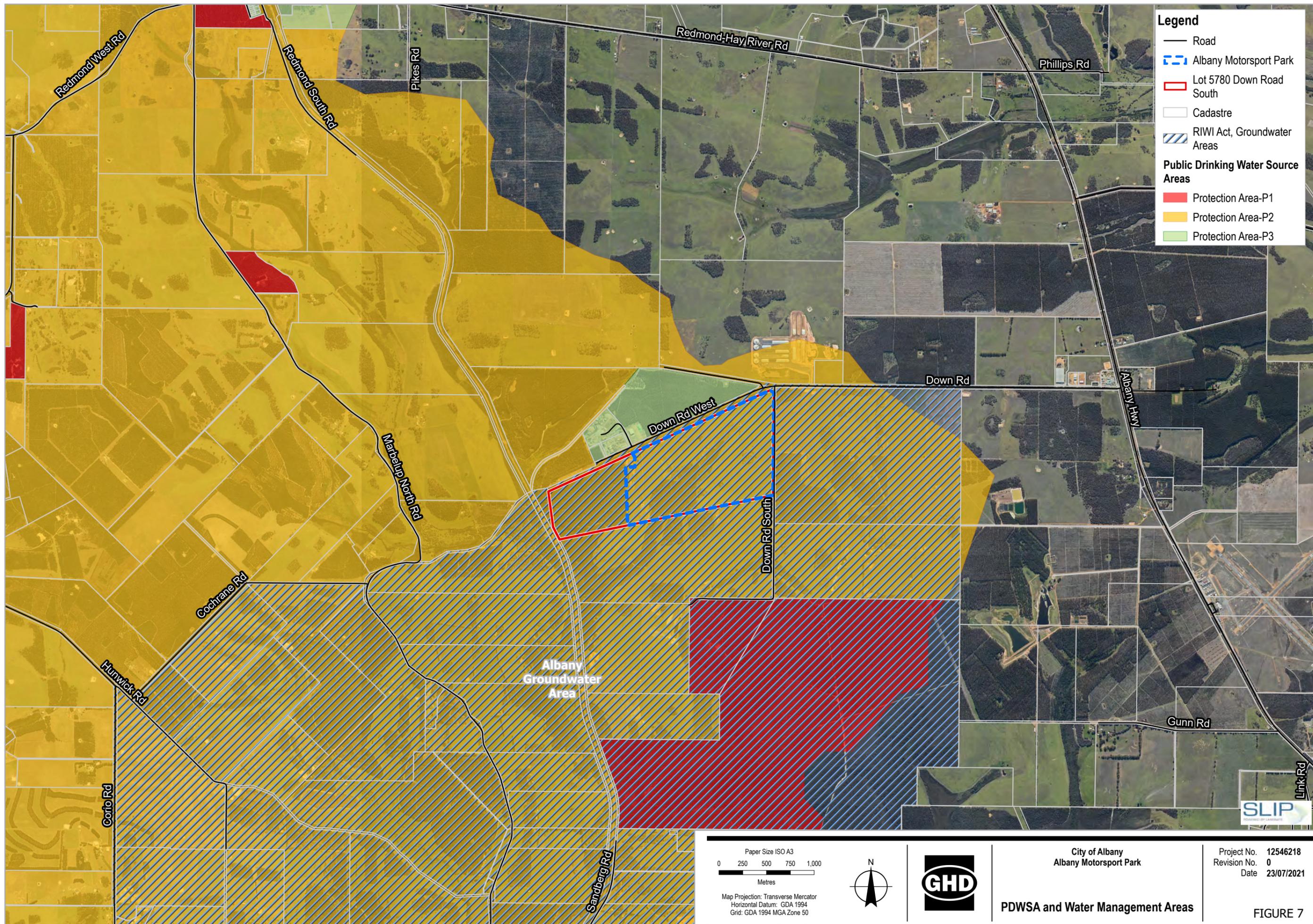
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**LEGEND**

- Albany Motorsport Park
- Project Site
- Shallow Bores
- Deep Bore
- Groundwater Level (BGL) August 2019
- Surface Water Flow Direction
- Regional Groundwater Flow Direction
- Shallow Aquifer Flow Direction
- South Coast Significant Wetland

<p>Paper Size ISO A3</p> <p>0 100 200 300</p> <p style="text-align: center;">Metres</p> <p>Map Projection: Transverse Mercator Horizontal Datum: GDA 1994 Grid: GDA 1994 MGA Zone 50</p>			<p>City of Albany</p> <p>Great Southern Motor Sports Park Feasibility Study</p> <p>Lot 5780 Down Road South, Drome</p>	<p>Project No. 12546218</p> <p>Revision No. 0</p> <p>Date 05/08/2021</p>
<p>Hydrology and hydrogeology</p>			<p><b>FIGURE 6</b></p>	



**Legend**

- Road
- ▭ Albany Motorsport Park
- ▭ Lot 5780 Down Road South
- ▭ Cadastre
- ▨ RIWI Act, Groundwater Areas

**Public Drinking Water Source Areas**

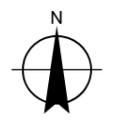
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- ▭ Protection Area-P2
- ▭ Protection Area-P3

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Metres

Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50



City of Albany  
 Albany Motorsport Park

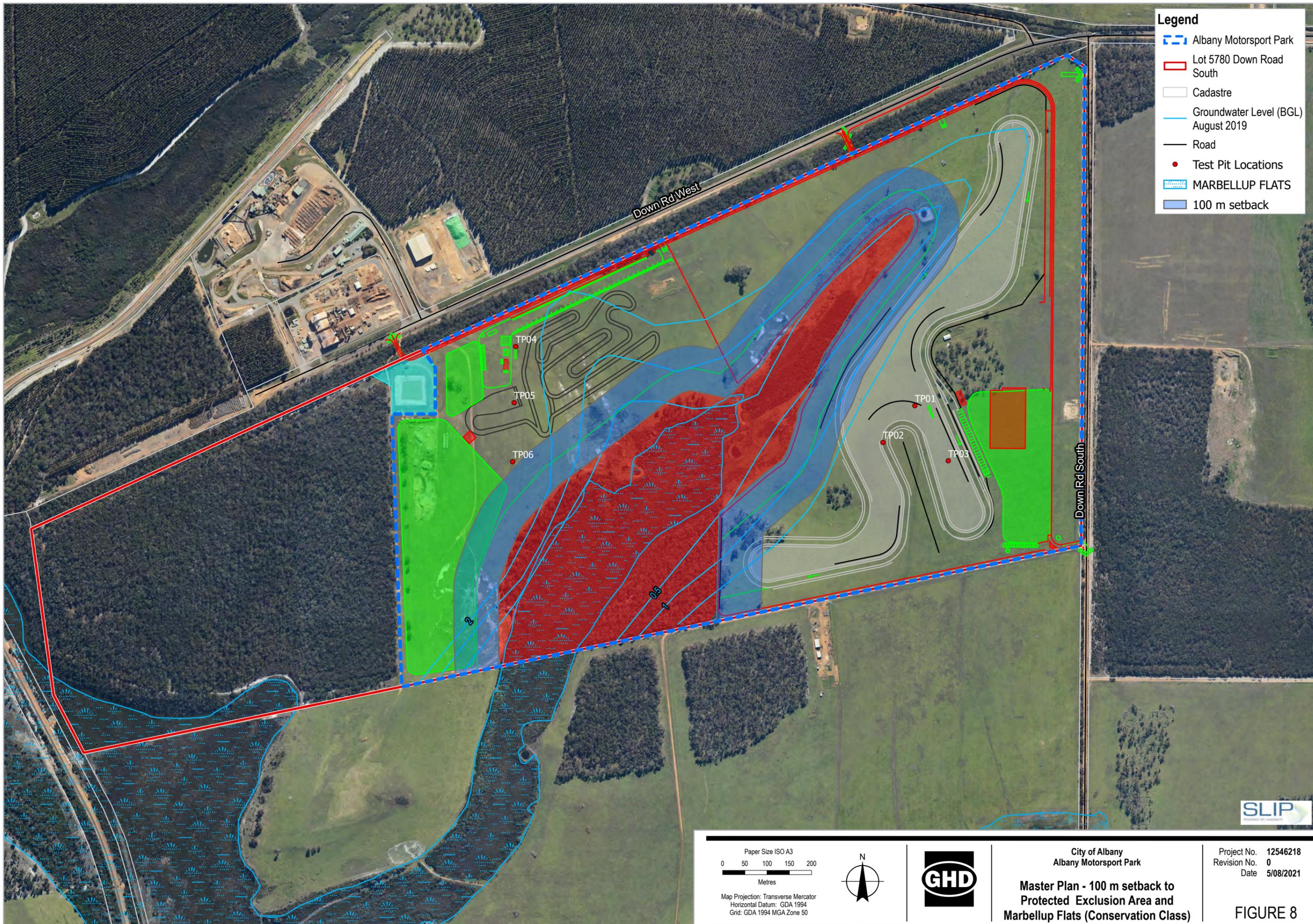
**PDWSA and Water Management Areas**

Project No. 12546218  
 Revision No. 0  
 Date 23/07/2021

**FIGURE 7**

N: \\AU\Perth\Projects\6112546218\GIS\Maps\Working\12546218\12546218\_StormwaterManagementPlan\12546218\_StormwaterManagementPlan.aprx\12546218  
 Print date: 23 Jul 2021 - 11:25

Data source: Landgate\_Subscription\_Imagery\WAnow: Landgate / SLIP. Created by: v-davies



- Legend**
- Albany Motorsport Park
  - Lot 5780 Down Road South
  - Cadastre
  - Groundwater Level (BGL) August 2019
  - Road
  - Test Pit Locations
  - MARBELLUP FLATS
  - 100 m setback

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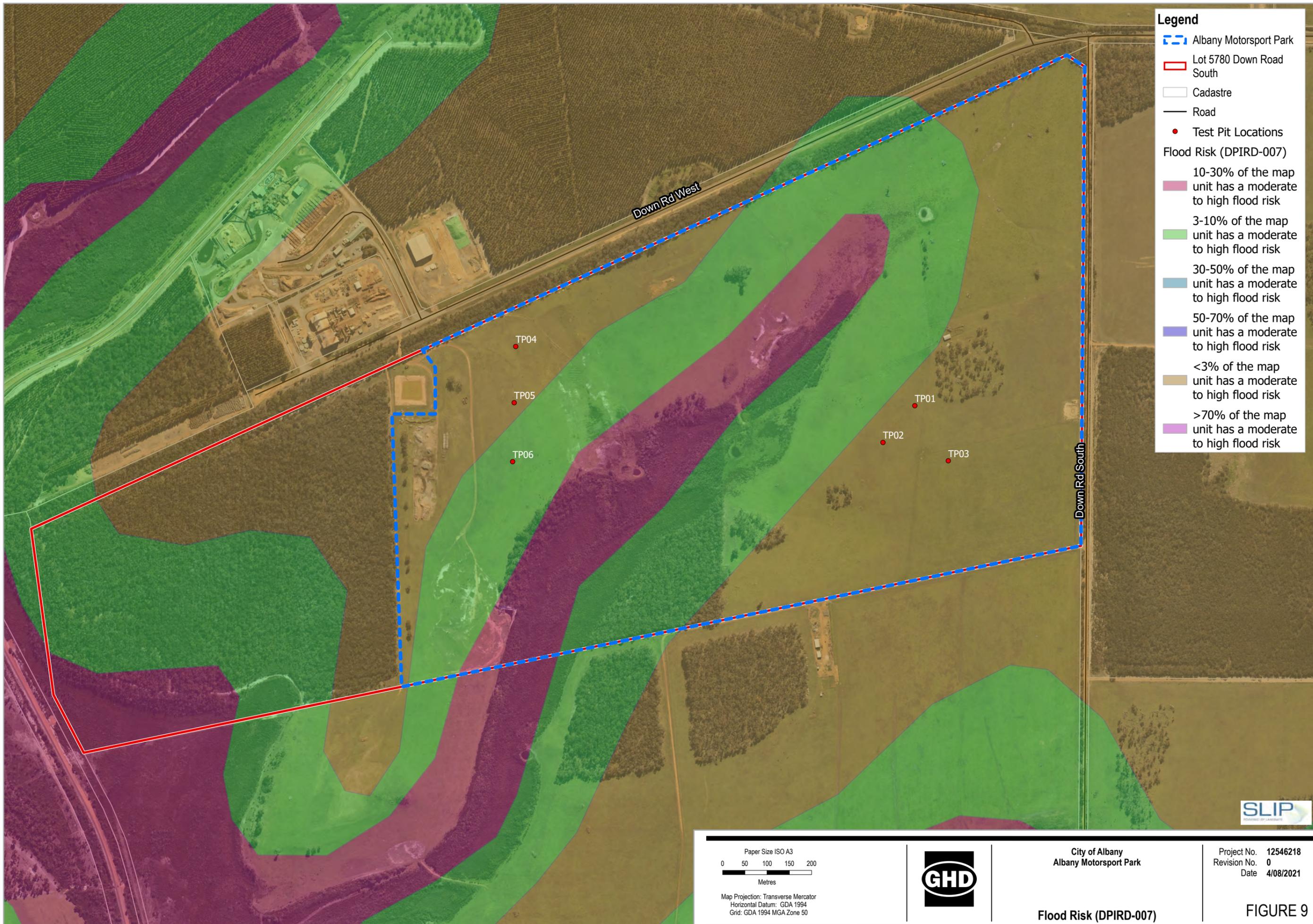


City of Albany  
 Albany Motorsport Park  
**Master Plan - 100 m setback to  
 Protected Exclusion Area and  
 Marbellup Flats (Conservation Class)**

Project No. 12546218  
 Revision No. 0  
 Date 5/08/2021

**FIGURE 8**

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**Legend**

- Albany Motorsport Park
- Lot 5780 Down Road South
- Cadastre
- Road
- Test Pit Locations

**Flood Risk (DPIRD-007)**

- 10-30% of the map unit has a moderate to high flood risk
- 3-10% of the map unit has a moderate to high flood risk
- 30-50% of the map unit has a moderate to high flood risk
- 50-70% of the map unit has a moderate to high flood risk
- <3% of the map unit has a moderate to high flood risk
- >70% of the map unit has a moderate to high flood risk

Paper Size ISO A3  
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 Metres

Map Projection: Transverse Mercator  
 Horizontal Datum: GDA 1994  
 Grid: GDA 1994 MGA Zone 50



City of Albany  
 Albany Motorsport Park

**Flood Risk (DPIRD-007)**

Project No. 12546218  
 Revision No. 0  
 Date 4/08/2021



**FIGURE 9**

C:\Users\vdavies\Desktop\Motor sports\12546218\_Effluent disposal aprx\12546218\_SMP\_SSE\_Flood Risk\_Rev0  
 Print date: 04 Aug 2021 - 22:35

Data source: Landgate\_Subscription\_Imagery\WAnow: Landgate / SLIP. Created by: vdavies

# Appendix B

## Water balance

**Albany Motorsport Park**

**Motocross - Effluent Disposal Water Balance**

Hydraulic loading: **35** L/person/d

Section 29 of *Health (Treatment of Sewage and Disposal of Effluent and Liquid Waste) Regulations 1974*

Activity	Mon	Tues	Wed	Thu	Fri	Sat	Sun			
Training - attendees	20	20	20	20	20					
Club event - attendees						300	300			
Flow	700	700	700	700	700	10500	10500	<b>24,500</b>	L/week (total)	
								<b>3,500</b>	L/d (average)	
									100	persons
Cum. IN	700	1400	2100	2800	3500	14000	24500			
Cum. OUT	3,500	7,000	10,500	14,000	17,500	21,000	24,500			
	11,200	8,400	5,600	2,800	0	7,000	14,000		Tank size:	14,000

# Water Balance for Zero Storage

<b>Site Address:</b>	Lot 5780 Down Road South, Drome		
<b>Date:</b>	Thursday, 12 August 2021	<b>Assessor:</b>	Jeff Foley

## INPUT DATA

Design Wastewater Flow	Q	3,500	L/day	Based on maximum potential occupancy and derived from the Supplement to Regulation 29 and Schedule 9 - Wastewater system loading rates
Design Irrigation Rate	DIR	5.0	mm/day	Based on soil texture class/permeability and derived from Table M1 of AS/NZS 1547:2012
Nominated Land Application Area	L	1100	m <sup>2</sup>	<sup>1</sup>
Crop Factor	C	0.8-1.0	unitless	Estimates evapotranspiration as a fraction of pan evaporation; varies with season and crop type <sup>2</sup>
Rainfall Runoff Factor	RF	0.9	unitless	Proportion of rainfall that remains onsite and infiltrates, allowing for any runoff
Mean Monthly Rainfall Data	<a href="http://om.gov.au/climate/averages/tables/cw_009">om.gov.au/climate/averages/tables/cw_009</a>			BoM Station and number
Mean Monthly Pan Evaporation Data	Albany - Agric reference			BoM Station and number or data from the Evaporation Data for Western Australia Report <a href="https://researchlibrary.agric.wa.gov.au/cgi/viewcontent.cgi?article=1058&amp;context=rmt">https://researchlibrary.agric.wa.gov.au/cgi/viewcontent.cgi?article=1058&amp;context=rmt</a>

Parameter	Symbol	Formula	Units	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
Days in month	D		days	31	28	31	30	31	30	31	31	30	31	30	31	365
Rainfall	R		mm/month	23.6	22.3	33.6	61.3	89.8	108	119.3	106.8	88.5	70.8	47	27.8	798.8
Evaporation	E		mm/month	220	171	150	91	63	47	59	67	84	106	150	199	1407
Crop Factor	C		unitless	1.00	1.00	0.90	0.90	0.80	0.80	0.80	0.80	0.90	1.00	1.00	1.00	

## OUTPUTS

Evapotranspiration	ET	ExC	mm/month	220	171	135	82	50	38	47	54	76	106	150	199	1327.3
Percolation	B	DIRxD	mm/month	155.0	140	155.0	150.0	155.0	150.0	155.0	155.0	150.0	155.0	150.0	155.0	1825.0
Outputs		ET+B	mm/month	375.0	311	290.0	231.9	205.4	187.6	202.2	208.6	225.6	261.0	300.0	354.0	3152.3

## INPUTS

Retained Rainfall	RR	RxRF	mm/month	20.06	18.955	28.56	52.105	76.33	91.8	101.405	90.78	75.225	60.18	39.95	23.63	678.98
Applied Effluent	W	(QxD)/L	mm/month	98.6	89.1	98.6	95.5	98.6	95.5	98.6	98.6	95.5	98.6	95.5	98.6	1161.4
Inputs		RR+W	mm/month	118.7	108.0	127.2	147.6	175.0	187.3	200.0	189.4	170.7	158.8	135.4	122.3	1840.3

## STORAGE CALCULATION

Storage remaining from previous month			mm/month	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Storage for the month	S	(RR+W)-(ET+B)	mm/month	-256.3	-203.0	-162.8	-84.3	-30.4	-0.3	-2.2	-19.2	-54.9	-102.2	-164.6	-231.7	
Cumulative Storage	M		mm	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
Maximum Storage for Nominated Area	N		mm	0.00												
	V	NxL	L	0												

## LAND AREA REQUIRED FOR ZERO STORAGE

	m <sup>2</sup>	306	336	415	584	841	1096	1076	921	698	540	404	328
--	----------------	-----	-----	-----	-----	-----	------	------	-----	-----	-----	-----	-----

## MINIMUM AREA REQUIRED FOR ZERO STORAGE:

**1097** m<sup>2</sup>

## CELLS

	Please enter data in blue cells
XX	Enter available Land Application Area
XX	Data in yellow cells is calculated by the spreadsheet, DO NOT ALTER THESE CELLS

## NOTES

<sup>1</sup> This value should be the largest of the following: land application area required based on the most limiting nutrient balance or minimum area required for zero storage

<sup>2</sup> Values selected are suitable for grass in WA

# Appendix C

## GHD Pty Ltd Professional Indemnity Insurance Certificate

Telephone: +61 2 9285 4000  
Fax: +61 2 9995 7297  
Website: www.willistowerswatson.com.au  
Direct Line: +61 2 9285 4060  
Email: tanya.stevenson@willistowerswatson.com

**Issue Date: 24 November 2020**

**To Whom It May Concern**

## Certificate of Placement – Professional Indemnity

In our capacity as Insurance Broker to the Named Insured shown below, we confirm having arranged the following insurance, the details of which are correct as at the Issue Date:

**Named Insured:** GHD Group Limited and Subsidiaries including GHD Pty Ltd  
**Form:** Civil Liability Wording which includes coverage for the Trade Practices Act and the Competition and Consumer Act  
**Policy Number:** B080113856P20  
**Limit of Indemnity:** AUD2,000,000 any one claim and in the aggregate  
**Period of Insurance:** 1 December 2020 at 4.00pm to 1 December 2021 at 4.00pm  
**Insurer:** Certain Underwriters at Lloyd's of London



-----  
Signed for and on behalf of  
**Willis Australia Ltd ("Willis Towers Watson")**

**Disclaimer:**

This document has been prepared at the request of our client and does not represent an insurance policy, guarantee or warranty and cannot be relied upon as such. All coverage described is subject to the terms, conditions and limitations of the insurance policy and is issued as a matter of record only. This document does not alter or extend the coverage provided or assume continuity beyond the Expiry Date. It does not confer any rights under the insurance policy to any party. Willis Towers Watson is under no obligation to inform any party if the insurance policy is cancelled, assigned or changed after the Issue Date.

# Appendix D

**Albany Motorsport Park Development -  
Site Investigation Report 4626/1 (Great  
Southern Geotechnics, 2021)**



# GREAT SOUTHERN GEOTECHNICS

CONSTRUCTION MATERIALS TESTING

## Site Investigation

Report 4626/1

Monday, 28 June 2021

**GHD**

Albany Motorsport Park Development

# GREAT SOUTHERN GEOTECHNICS

## 1.0 INTRODUCTION

As authorised by GHD

an investigation for the proposed Albany Motorsport Park Development adjacent to Down Rd, Mirambeena was performed on the 25/06/2021

## 2.0 GENERAL

The intent of the investigation was to determine the following:

- Soil types and profiles.
- Groundwater levels at time of investigation.

## 3.0 SITE INVESTIGATION

Site conditions and test pit locations were recorded and are displayed in [Appendix A - Maps](#).

Test pits logs/ soil profiles are noted in [Appendix B - Test Pit Logs](#)

The field investigation consisted of 6 Boreholes excavated on-site to depths of up to 2.5 meters using a Kubota KX41-3V mini excavator with a 300mm Auger.

Test pits were spread across the extent of the proposed development and locations were predetermined by GHD.

All soil layers encountered were visually assessed and classified on-site.

Samples gathered from site were the taken back to Great Southern Geotechnics Albany Laboratory then

**IMPORTANT NOTE:** The test pits have been spread so that they are representative of the subsurface materials across the intended reconstruction area, however, soil conditions may change dramatically over short distances and our investigations may not locate all soil variations across the site.

## 4.0 LABORATORY TESTING

No laboratory testing have been undertaken at Great southern Geotechnics laboratory.

Sampled taken have been transported by freight to Eurofins Scientific for further analysis.

Testing requirements will be confirmed by GHD post review of investigation findings.

This report and associated documentation was undertaken for the specific purpose described in the report and shall not be relied on for other purposes.

This report was prepared solely for the use by GHD any reliance assumed by other parties on this report shall be at such parties own risk.



# **Appendix A**

## Maps



# Figure 1

Test Pits 1 to 6

## Test Pit Locations



**GREAT SOUTHERN  
GEOTECHNICS**  
CONSTRUCTION MATERIALS TESTING

Job No: 4626  
Client: GHD  
Project: Albany Motorsport Park Development





# **Appendix B**

Test Pit Logs





**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** QU-0498  
**Location:** 34°55'55.6"S 117°44'53.0"E

**Date Commenced**  
25/06/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 180	180	<b>(Topsoil) SAND with silt:</b> Dark grey, fine to medium. Roots and root fibres.	M	L-MD		No water table encountered.			
180 - 490	310	<b>Sandy GRAVEL:</b> Brown, fine to coarse, sub-rounded to sub-angular, ( F:20% / M:20% / C:15%). Fine to medium grained sand. Contains approximately 10% Cobbles & Boulders in excess of 250mm diameter.	M	MD-D				#	
550 - 2500	1950	<b>Sandy CLAY:</b> Low to medium plasticity, Brown/red mottled Light brown/orange (40%). Fine to medium grained sand.	M	F				#	

Samples Taken				Target Depth	✓	2500
TP1 - 180mm to 490mm				Cave In		
TP1 - 900mm to 1100mm				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High		EH - Extremely High		

## Test Pit No.1



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.:** QU-0498  
**Location:** 34°55'58.3"S 117°44'50.2"E

**Date Commenced**  
25/06/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 140	140	<b>(Topsoil) SAND with silt:</b> Dark grey, fine to medium. Roots and root fibres.	M	L-MD		No water table encountered.			
140 - 400	260	<b>Sandy GRAVEL:</b> Brown, fine to coarse, sub-rounded to sub-angular, ( F:20% / M:20% / C:15%). Fine to medium grained sand. Contains approximately 10% Cobbles & Boulders in excess of 400mm diameter.	M	VD	MC				
400 - 1400	1000	<b>Sandy CLAY:</b> Low to medium plasticity, Light brown. Fine to medium grained sand.	M	F				#	
1400 - 2500	1100	<b>Sandy CLAY:</b> Low to medium plasticity, Brown/red mottled Light brown/orange (40%). Fine to medium grained sand.	M	F				#	

Samples Taken				Target Depth	✓	2500
TP2 - 500mm to 900mm				Cave In		
TP2 - 1700mm to 2000mm				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.2



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.:** QU-0498  
**Location:** 34°55'59.6"S 117°44'56.4"E

**Date Commenced**  
25/06/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 250	250	<b>(Topsoil) SAND with silt:</b> Dark grey to grey, fine to medium. Roots and root fibres.	M	L-MD		No water table encountered.			
250 - 830	580	<b>Sandy GRAVEL:</b> Brown, fine to medium, sub-rounded to sub-angular, ( F:30% / M:30% ). Fine to medium grained sand. Contains approximately 10% Cobbles & Boulders in excess of 400mm diameter.	M	MD-D				#	
830 - 1600	770	<b>Sandy CLAY:</b> Low to medium plasticity, Light brown. Fine to medium grained sand.	M	F				#	
1600 - 2500	900	<b>Sandy CLAY:</b> Low to medium plasticity, Brown/red mottled Light brown/grey (30%). Fine to medium grained sand.	M	F				#	

Samples Taken				Target Depth	✓	2500
TP3 - 300mm to 600mm				Cave In		
TP3 - 900mm to 1200mm				Refusal		
TP3 - 1600mm to 2000mm				Near Refusal		
Cohesive	Non-Cohesive	Rock	Cementation	Flooding		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	Lack of Reach		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented	General		
F - Firm	MD - Medium Dense	L - Low		MC - moderately Cemented	D - Dry M - Moist W - Wet	
St - Stiff	D - Dense	M - Medium	N/A - Not Applicable			
VSt - Very Stiff	VD - Very Dense	H - High	N/D - Not Determined			
H - Hard	CO - Compact	VH - Very High	WC - Well Cemented			
		EH - Extremely High				

## Test Pit No.3



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.:** QU-0498  
**Location:** 34°55'51.5"S 117°44'17.6"E

**Date Commenced**  
25/06/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 220	220	<b>(Topsoil) SAND with silt:</b> Dark grey, fine to medium. Roots and root fibres.	M	L-MD		No water table encountered.			
220 - 1250	1030	<b>Sandy GRAVEL:</b> Brown, fine to coarse, sub-rounded to sub-angular, ( F:25% / M:20% / C:10%). Fine to medium grained sand. Contains approximately 10% Cobbles & Boulders in excess of 400mm diameter.	M	D				#	
1250 - 1750	500	<b>Sandy CLAY:</b> Low to medium plasticity, Light brown/orange. Fine to medium grained sand.	M	F				#	
1750 - 2500	750	<b>Sandy CLAY:</b> Low to medium plasticity, grey mottled red (30%) & orange (10%). Fine to medium grained sand.	M	F				#	

Samples Taken				Target Depth	✓	2500
TP4 - 400mm to 800mm				Cave In		
TP4 - 1350mm to 1650mm				Refusal		
TP4 - 1800mm to 2200mm				Near Refusal		
Cohesive	Non-Cohesive	Rock	Cementation	Flooding		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	Lack of Reach		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented	General		
F - Firm	MD - Medium Dense	L - Low		MC - moderately Cemented	D - Dry	M - Moist
St - Stiff	D - Dense	M - Medium	N/A - Not Applicable			
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented		N/D - Not Determined	
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.4



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.** QU-0498  
**Location:** 34°55'55.6"S 117°44'17.5"E

**Date Commenced**  
25/06/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 230	230	<b>(Topsoil) SAND with silt:</b> Dark grey, fine to medium. Roots and root fibres.	M	L-MD		No water table encountered.			
230 - 880	650	<b>SAND with silt:</b> Grey, fine to medium.	M	MD			#		
880 - 2500	1620	<b>Sandy GRAVEL:</b> Brown, fine to coarse, sub-rounded to sub-angular, ( F:15% / M:30% / C:10%). Fine to medium grained sand. Contains approximately 10% Cobbles & Boulders in excess of 400mm diameter.	M	MD-D			#		

Samples Taken				Target Depth	✓	2500
TP5 - 400mm to 800mm				Cave In		
TP5 - 1200mm to 1500mm				Refusal		
				Near Refusal		
				Flooding		
				Lack of Reach		
Cohesive	Non-Cohesive	Rock	Cementation	General		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	D - Dry M - Moist W - Wet N/A - Not Applicable N/D - Not Determined		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented			
F - Firm	MD - Medium Dense	L - Low	MC - moderately Cemented			
St - Stiff	D - Dense	M - Medium				
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented			
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.5



**Excavation**



**Spoil**



**Client:** GHD  
**Project:** Albany Motorsport Park Development  
**Project No.:** QU-0498  
**Location:** 34°55'59.9"S 117°44'17.4"E

**Date Commenced**  
25/06/2021  
**Logged By**  
M.Coffey

**Operator/Contractor:** GSG  
**Equipment type:** Kubota KX41-3V  
**Excavation Method :** 300mm Auger  
**Position:** Refer to site plan

Depth Below Surface (mm)	Layer Depth (mm)	Material Description  SOIL TYPE, Plasticity, Colour, Particle characteristics, Secondary and other minor components	Moist. Condition	Consistency / Strength	Cementation	Water Table	Classification Symbol	Sample/Test	
0 - 350	350	<b>(Topsoil) SAND with silt:</b> Dark grey, fine to medium. Roots and root fibres.	M	L-MD		No water table encountered.			
350 - 1200	850	<b>Sandy GRAVEL:</b> Brown, fine to coarse, sub-rounded to sub-angular, ( F:20% / M:20% / C:10%). Fine to medium grained sand. Contains approximately 10% Cobbles & Boulders in excess of 400mm diameter.	M	D-VD				#	
1200 - 1800	600	<b>Sandy GRAVEL:</b> Light brown, fine to coarse, sub-rounded to sub-angular, ( F:20% / M:30% / C:10%). Fine to medium grained sand.	M	D				#	
1800 - 2500	700	<b>Sandy GRAVEL:</b> Brown/orange, fine to medium, sub-rounded to sub-angular, ( F:40% / M:20% ). Fine to medium grained sand.	M	MD-D				#	

Samples Taken				Target Depth	✓	2500
TP6 - 500mm to 800mm				Cave In		
TP6 - 1300mm to 1600mm				Refusal		
TP6 - 2000mm to 2300mm				Near Refusal		
Cohesive	Non-Cohesive	Rock	Cementation	Flooding		
VS - Very Soft	VL - Very Loose	EL - Extremely Low	IN - Indurated	Lack of Reach		
S - Soft	L - Loose	VL - Very Low	PC - Poorly Cemented	General		
F - Firm	MD - Medium Dense	L - Low		MC - moderately Cemented	D - Dry	M - Moist
St - Stiff	D - Dense	M - Medium	N/A - Not Applicable			
VSt - Very Stiff	VD - Very Dense	H - High	WC - Well Cemented		N/D - Not Determined	
H - Hard	CO - Compact	VH - Very High				
		EH - Extremely High				

## Test Pit No.6



**Excavation**



**Spoil**

## COLOURS

	BLACK - BROWN (bk)		BLUE (bl)		ORANGE (or)
	BROWN (br)		BLUE - GREEN (bl/gr)		RED (rd)
	GREY - BROWN (gy/br)		GREEN (gr)		RED - BROWN (rd/br)
	GREY (gy)		YELLOW (yl)		PINK (pk)
	BLUE - GREY (bl/gy)		YELLOW - BROWN (yl/br)		PURPLE (pr)

## MOISTURE CONDITION OF SOIL

TERM	DESCRIPTION
Dry	Cohesive soils; hard and friable or powdery, well dry of plastic limit. Granular soils; cohesionless and free-running.
Moist	Soil feels cool, darkened in colour. Cohesive soils can be moulded. Granular soils tend to cohere.
Wet	Soil feels cool, darkened in colour. Cohesive soils usually weakened and free water forms on hands when handling. Granular soils tend to cohere and free water forms on hands when handling.

## PARTICLE SHAPES

ANGULAR	SUB-ANGULAR	SUB-ROUNDED	ROUNDED
			

## PARTICLE SIZES

BOULDERS	COBBLES	COARSE GRAVEL	MEDIUM GRAVEL	FINE GRAVEL	COARSE SAND	MEDIUM SAND	FINE SAND	SILT	CLAY
>200mm	63-200mm	20-63mm	6-20mm	2.36-6mm	0.6-2.36mm	0.2-0.6mm	0.075-0.2mm	0.002-0.075mm	<0.002mm

## GRAIN SIZE

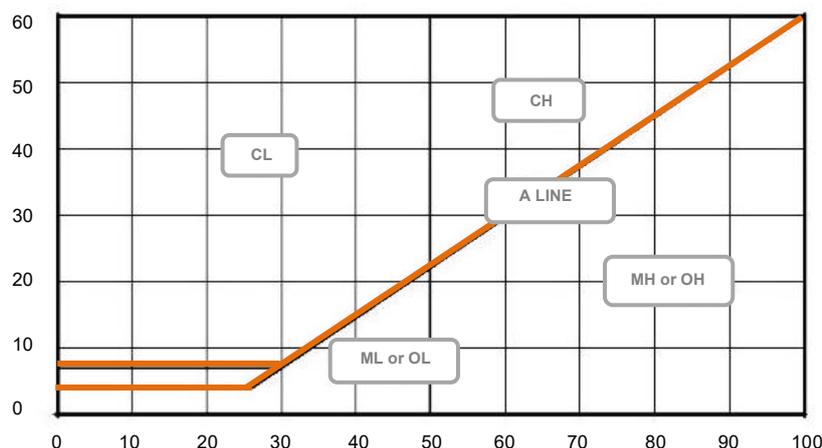
SOIL TYPE (ABBREV.)	CLAY (CL)	SILT (SI)	SAND (SA)			GRAVEL (GR)		COBBLES (CO)	
SIZE	< 2µm	2-75µm	Fine 0.075-0.2mm	Medium 0.2-0.6mm	Coarse 0.6-2.36mm	Fine 2.36-6mm	Medium 6-20mm	Coarse 20-63mm	63-200mm
SHAPE & TEXTURE	Shiny	Dull	angular or sub angular or sub rounded or rounded						
FIELD GUIDE	Not visible under 10x	Visible under 10x	Visible by eye	Visible at < 1m	Visible at < 3m	Visible at < 5m	Road gravel	Rail ballast	Beaching

## CLASSIFICATION CHART

FIELD IDENTIFICATION PROCEDURES (Excluding particles larger than 60mm and basing fractions on estimated mass)				GROUP SYMBOLS	TYPICAL NAMES	
<b>COARSE GRAINED SOILS</b> More than 50% of material less than 63 mm is larger than 0.075 mm	<b>GRAVELS</b> More than 50% of coarse fraction is larger than 2.36mm	<b>CLEAN GRAVELS</b> (Little or no fines)	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength	GW	Well graded gravels, gravel-sand mixtures, little or no fines	
			Predominantly one size or range of sizes with some intermediate sizes missing, not enough fines to bind coarse grains, no dry strength	GP	Poorly Graded gravels and gravel-sand mixtures, little or no fines, uniform gravels	
		<b>GRAVELS WITH FINES</b> (Appreciable amount of fines)	Dirty materials with excess of non-plastic fines, zero to medium dry strength	GM	Silty gravels, gravel-sand-silt mixtures	
			'Dirty' materials with excess of plastic fines, medium to high dry strength	GC	Clayey gravels, gravel-sand-clay mixtures	
	<b>SANDS</b> More than 50% of coarse fraction is smaller than 2.36mm	<b>CLEAN SANDS</b> (Little or no fines)	Wide range in grain size and substantial amounts of all intermediate sizes, not enough fines to bind coarse grains, no dry strength	SW	Well graded sands, gravelly sands, little or no fines	
			Predominantly one size or range of sizes with some intermediate sizes missing, not enough fines to bind coarse grains, no dry strength	SP	Poorly graded sands and gravelly sands; little or no fines, uniform sands	
		<b>SANDS WITH FINES</b> (Appreciable amount of fines)	Dirty materials with excess of non-plastic fines, zero to medium dry strength	SM	Silty sands, sand-silt mixtures	
			'Dirty' materials with excess of plastic fines, medium to high dry strength	SC	Clayey sands, sand-clay mixtures	
<b>FINE GRAINED SOILS</b> More than 50% of material less than 63 mm is smaller than 0.075 mm	IDENTIFICATION PROCEDURES ON FRACTIONS <0.2mm					
	<b>SILTS AND CLAYS</b> Liquid limit less than 50	DRY STRENGTH	DILATANCY	TOUGHNESS		
		None to low	Quick to slow	None	ML	Inorganic silts and very fine sands, rock flour, silty or clayey fine sands with low plasticity. Silts of low to medium Liquid Limit.
		Medium to high	None to very slow	Medium	CL, CI	Inorganic clays of low to medium plasticity, gravelly clays, sandy clays, silty clays.
	<b>SILTS AND CLAYS</b> Liquid limit greater than 50	Low to medium	Slow	Low	OL	Organic silts and organic silt-clays of low to medium plasticity.
		Low to medium	Slow to none	Low to medium	MH	Inorganic silts, micaceous or diatomaceous fine sandy or silty soils, silts of high Liquid Limit.
		High to very high	None	High	CH	Inorganic clays of high plasticity.
	<b>SILTS AND CLAYS</b> Liquid limit greater than 50	Medium to high	None to very slow	Low to medium	OH	Organic clays of high plasticity
		HIGHLY ORGANIC SOILS			Readily identified by colour, odour, spongy feel and frequently by fibrous texture	Pt

## PLASTICITY CHART

For laboratory classification of fine grained soils



## PLASTICITY

DESCRIPTIVE TERM	OF LOW PLASTICITY	OF MEDIUM PLASTICITY	OF HIGH PLASTICITY
Range Of Liquid Limit (%)	≤ 35	> 35 ≤ 50	> 50

## DESCRIPTION OF ORGANIC OR ARTIFICIAL MATERIALS

PREFERRED TERMS	SECONDARY DESCRIPTION
Organic Matter	Fibrous Peat/ Charcoal/ Wood Fragments/ Roots (greater than approximately 2mm diameter)/ Root Fibres (less than approximately 2mm diameter)
Waste Fill	Domestic Refuse/ Oil/ Bitumen/ Brickbats/ Concrete Rubble/ Fibrous Plaster/ Wood Pieces/ Wood Shavings/ Sawdust/ Iron Filings/ Drums/ Steel Bars/ Steel Scrap/ Bottles/ Broken Glass/ Leather

## CONSISTENCY – Cohesive soils

TERM	VERY SOFT	SOFT	FIRM	STIFF	VERY STIFF	HARD
Symbol	VS	S	F	St	VSt	H
Undrained Shear Strength (kPa)	< 12	12 – 25	25 – 50	50 – 100	100 – 200	> 200
SPT (N) Blowcount	0 – 2	2 – 4	4 – 8	8 – 15	15 – 30	> 30
Field Guide	Exudes between the fingers when squeezed	Can be moulded by light finger pressure	Can be moulded by strong finger pressure	Cannot be moulded by fingers. Can be indented by thumb nail	Can be indented by thumb nail	Can be indented with difficulty with thumb nail

## CONSISTENCY – Non-cohesive soils

TERM	VERY LOOSE	LOOSE	MEDIUM DENSE	DENSE	VERY DENSE	COMPACT
Symbol	VL	L	MD	D	VD	CO
SPT (N) Blowcount	0 – 4	4 – 10	10 – 30	30 – 50	50 – 100	> 50/150 mm
Density Index (%)	< 15	15 – 35	35 – 65	65 – 85	85 – 95	> 95
Field Guide	Ravels	Shovels easily	Shovelling very difficult	Pick required	Pick difficult	Cannot be picked

## MINOR COMPONENTS

TERM	TRACE	WITH
% Minor Component	Coarse grained soils: < 5% Fine grained soils: <15%	Coarse grained soils: 5 – 12% Fine grained soils: 15 – 30%
Field Guide	Presence just detectable by feel or eye, but soil properties little or no different to general properties of primary components	Presence easily detectable by feel or eye, soil properties little different to general properties of primary component

## GEOLOGICAL ORIGIN

	TYPE	DETAILS
TRANSPORTED SOILS	Aeolian Soils	Deposited by wind
	Alluvial Soils	Deposited by streams and rivers
	Colluvial Soils	Deposited on slopes
	Lacustrine Soils	Deposited by lakes
	Marine Soils	Deposited in ocean, bays, beaches and estuaries
FILL MATERIALS	Soil Fill	Describe soil type, UCS symbol and add 'FILL'
	Rock Fill	Rock type, degree of weathering, and word 'FILL'.
	Domestic Fill	Percent soil or rock, whether pretrucible or not.
	Industrial Fill	Percent soil, whether contaminated, particle size & type of waste product, ie brick, concrete, metal

## STRENGTH OF ROCK MATERIAL

TERM	SYMBOL	IS (50)	(MPA)	FIELD GUIDE TO STRENGTH
Extremely Low	EL	≤0.03		Easily remoulded by hand to a material with soil properties.
Very Low	VL	>0.03	≤0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxle sample by hand. Pieces up to 3 cm thick can be broken by finger pressure.
Low	L	>0.1	≤0.3	Easily scored with a knife; indentations 1 mm to 3 mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150 mm long by 50 mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling.
Medium	M	>0.3	≤1.0	Readily scored with a knife; a piece of core 150 mm long by 50 mm diameter can be broken by hand with difficulty.
High	H	>1	≤3	A piece of core 150 mm long by 50 mm diameter cannot be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.
Very High	VH	>3	≤10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.
Extremely High	EH	>10		Specimen requires many blows with geological pick to break through intact material; rock rings under hammer.

## ROCK MATERIAL WEATHERING CLASSIFICATION

TERM	SYMBOL	DEFINITION
Residual Soil	RS	Soil developed on extremely weathered rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported
Extremely Weathered Rock	XW	Rock is weathered to such an extent that it has 'soil' properties, i.e. it either disintegrates or can be remoulded, in water.
Distinctly Weathered Rock	DW	Rock strength usually changed by weathering. Rock may be highly discoloured, usually be iron staining. Porosity may be increased by leaching or may be decreased due to deposition of weathering products in pores.
Slightly Weathered Rock	SW	Rock is slightly discoloured but shows little or no change of strength from fresh rock.
Fresh Rock	FR	Rock shows no sign of decomposition or staining.

# Appendix E

## Laboratory results

## CERTIFICATE OF ANALYSIS

<b>Work Order</b> : <b>EP2107544</b> <b>Client</b> : <b>GHD PTY LTD</b> <b>Contact</b> : <b>MS VICKI DAVIES</b> <b>Address</b> : <b>999 HAY STREET</b> <b>PERTH WA, AUSTRALIA 6000</b>  <b>Telephone</b> : ---- <b>Project</b> : <b>12546218 Albany Motorsports Park DA</b> <b>Order number</b> : <b>12546218</b> <b>C-O-C number</b> : ---- <b>Sampler</b> : ---- <b>Site</b> : ---- <b>Quote number</b> : <b>EP/444/21</b> <b>No. of samples received</b> : <b>15</b> <b>No. of samples analysed</b> : <b>6</b>	<b>Page</b> : 1 of 4 <b>Laboratory</b> : Environmental Division Perth <b>Contact</b> : Nick Courts <b>Address</b> : 26 Rigali Way Wangara WA Australia 6065  <b>Telephone</b> : +61-8-9406 1301 <b>Date Samples Received</b> : 01-Jul-2021 13:30 <b>Date Analysis Commenced</b> : 02-Jul-2021 <b>Issue Date</b> : 13-Jul-2021 13:47
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This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full.

This Certificate of Analysis contains the following information:

- General Comments
- Analytical Results

**Additional information pertinent to this report will be found in the following separate attachments: Quality Control Report, QA/QC Compliance Assessment to assist with Quality Review and Sample Receipt Notification.**

### Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

<i>Signatories</i>	<i>Position</i>	<i>Accreditation Category</i>
Ankit Joshi	Inorganic Chemist	Sydney Inorganics, Smithfield, NSW
Chris Lemaitre	Laboratory Manager (Perth)	Perth Inorganics, Wangara, WA



## General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis.

Where the LOR of a reported result differs from standard LOR, this may be due to high moisture content, insufficient sample (reduced weight employed) or matrix interference.

When sampling time information is not provided by the client, sampling dates are shown without a time component. In these instances, the time component has been assumed by the laboratory for processing purposes.

Where a result is required to meet compliance limits the associated uncertainty must be considered. Refer to the ALS Contact for details.

Key : CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.  
LOR = Limit of reporting  
^ = This result is computed from individual analyte detections at or above the level of reporting  
ø = ALS is not NATA accredited for these tests.  
~ = Indicates an estimated value.

- Phosphorus Sorption Index + Capacity conducted by ALS Sydney, NATA accreditation no. 825, site no 10911.
- ED007 and ED008: When Exchangeable Al is reported from these methods, it should be noted that Rayment & Lyons (2011) suggests Exchange Acidity by 1M KCl - Method 15G1 (ED005) is a more suitable method for the determination of exchange acidity (H<sup>+</sup> + Al<sup>3+</sup>).



## Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)			Sample ID	TP1 - 900mm to 1100mm	TP2 - 500mm to 900mm	TP3 - 300mm to 600mm	TP4 - 400mm to 800mm	TP5 - 400mm to 800mm
Sampling date / time			25-Jun-2021 00:00	25-Jun-2021 00:00	25-Jun-2021 00:00	25-Jun-2021 00:00	25-Jun-2021 00:00	25-Jun-2021 00:00
Compound	CAS Number	LOR	Unit	EP2107544-002	EP2107544-003	EP2107544-005	EP2107544-008	EP2107544-011
				Result	Result	Result	Result	Result
<b>EA002: pH 1:5 (Soils)</b>								
pH Value	----	0.1	pH Unit	6.1	6.1	5.7	5.8	5.4
<b>EA010: Conductivity (1:5)</b>								
Electrical Conductivity @ 25°C	----	1	µS/cm	22	25	28	24	4
<b>ED007: Exchangeable Cations</b>								
Exchangeable Calcium	----	0.1	meq/100g	0.8	0.8	1.6	0.8	<0.1
Exchangeable Magnesium	----	0.1	meq/100g	0.5	1.0	0.2	0.2	<0.1
Exchangeable Potassium	----	0.1	meq/100g	<0.1	<0.1	<0.1	<0.1	<0.1
Exchangeable Sodium	----	0.1	meq/100g	<0.1	<0.1	0.1	<0.1	<0.1
Cation Exchange Capacity	----	0.1	meq/100g	1.4	1.9	2.0	1.1	0.1
Exchangeable Sodium Percent	----	0.1	%	5.8	4.8	5.7	6.2	<0.1
<b>EK072: Phosphate Sorption Capacity</b>								
Phosphate Sorption Capacity	----	250	mg P sorbed/kg	688	1650	3660	3000	<250
Phosphate Sorption Index	----	1	mgkg-1/log10 ugL-1	60	157	289	244	<1



## Analytical Results

Sub-Matrix: SOIL (Matrix: SOIL)		Sample ID		TP6 - 500mm to 800mm	----	----	----	----
		Sampling date / time		25-Jun-2021 00:00	----	----	----	----
Compound	CAS Number	LOR	Unit	EP2107544-013	-----	-----	-----	-----
				Result	----	----	----	----
<b>EA002: pH 1:5 (Soils)</b>								
pH Value	----	0.1	pH Unit	<b>5.9</b>	----	----	----	----
<b>EA010: Conductivity (1:5)</b>								
Electrical Conductivity @ 25°C	----	1	µS/cm	<b>20</b>	----	----	----	----
<b>ED007: Exchangeable Cations</b>								
Exchangeable Calcium	----	0.1	meq/100g	<b>1.0</b>	----	----	----	----
Exchangeable Magnesium	----	0.1	meq/100g	<b>0.2</b>	----	----	----	----
Exchangeable Potassium	----	0.1	meq/100g	<0.1	----	----	----	----
Exchangeable Sodium	----	0.1	meq/100g	<0.1	----	----	----	----
Cation Exchange Capacity	----	0.1	meq/100g	<b>1.3</b>	----	----	----	----
Exchangeable Sodium Percent	----	0.1	%	<b>1.4</b>	----	----	----	----
<b>EK072: Phosphate Sorption Capacity</b>								
Phosphate Sorption Capacity	----	250	mg P sorbed/kg	<b>966</b>	----	----	----	----
Phosphate Sorption Index	----	1	mgkg-1/log10 ugL-1	<b>62</b>	----	----	----	----

## Inter-Laboratory Testing

Analysis conducted by ALS Sydney, NATA accreditation no. 825, site no. 10911 (Chemistry) 14913 (Biology).

(SOIL) EK072: Phosphate Sorption Capacity

## QUALITY CONTROL REPORT

<b>Work Order</b>	<b>: EP2107544</b>	<b>Page</b>	<b>: 1 of 3</b>
<b>Client</b>	<b>: GHD PTY LTD</b>	<b>Laboratory</b>	<b>: Environmental Division Perth</b>
<b>Contact</b>	<b>: MS VICKI DAVIES</b>	<b>Contact</b>	<b>: Nick Courts</b>
<b>Address</b>	<b>: 999 HAY STREET</b>	<b>Address</b>	<b>: 26 Rigali Way Wangara WA Australia 6065</b>
	<b>PERTH WA, AUSTRALIA 6000</b>		
<b>Telephone</b>	<b>: ----</b>	<b>Telephone</b>	<b>: +61-8-9406 1301</b>
<b>Project</b>	<b>: 12546218 Albany Motorsports Park DA</b>	<b>Date Samples Received</b>	<b>: 01-Jul-2021</b>
<b>Order number</b>	<b>: 12546218</b>	<b>Date Analysis Commenced</b>	<b>: 02-Jul-2021</b>
<b>C-O-C number</b>	<b>: ----</b>	<b>Issue Date</b>	<b>: 13-Jul-2021</b>
<b>Sampler</b>	<b>: ----</b>		
<b>Site</b>	<b>: ----</b>		
<b>Quote number</b>	<b>: EP/444/21</b>		
<b>No. of samples received</b>	<b>: 15</b>		
<b>No. of samples analysed</b>	<b>: 6</b>		



This report supersedes any previous report(s) with this reference. Results apply to the sample(s) as submitted, unless the sampling was conducted by ALS. This document shall not be reproduced, except in full.

This Quality Control Report contains the following information:

- Laboratory Duplicate (DUP) Report; Relative Percentage Difference (RPD) and Acceptance Limits
- Method Blank (MB) and Laboratory Control Spike (LCS) Report; Recovery and Acceptance Limits
- Matrix Spike (MS) Report; Recovery and Acceptance Limits

### Signatories

This document has been electronically signed by the authorized signatories below. Electronic signing is carried out in compliance with procedures specified in 21 CFR Part 11.

<i>Signatories</i>	<i>Position</i>	<i>Accreditation Category</i>
Ankit Joshi	Inorganic Chemist	Sydney Inorganics, Smithfield, NSW
Chris Lemaitre	Laboratory Manager (Perth)	Perth Inorganics, Wangara, WA



## General Comments

The analytical procedures used by ALS have been developed from established internationally recognised procedures such as those published by the USEPA, APHA, AS and NEPM. In house developed procedures are fully validated and are often at the client request.

Where moisture determination has been performed, results are reported on a dry weight basis.

Where a reported less than (<) result is higher than the LOR, this may be due to primary sample extract/digestate dilution and/or insufficient sample for analysis. Where the LOR of a reported result differs from standard LOR, this may be due to high

Key :  
 Anonymous = Refers to samples which are not specifically part of this work order but formed part of the QC process lot  
 CAS Number = CAS registry number from database maintained by Chemical Abstracts Services. The Chemical Abstracts Service is a division of the American Chemical Society.  
 LOR = Limit of reporting  
 RPD = Relative Percentage Difference  
 # = Indicates failed QC

## Laboratory Duplicate (DUP) Report

The quality control term Laboratory Duplicate refers to a randomly selected intralaboratory split. Laboratory duplicates provide information regarding method precision and sample heterogeneity. The permitted ranges for the Relative Percent Deviation (RPD) of Laboratory Duplicates are specified in ALS Method QWI-EN/38 and are dependent on the magnitude of results in comparison to the level of reporting: Result < 10 times LOR: No Limit; Result between 10 and 20 times LOR: 0% - 50%; Result > 20 times LOR: 0% - 20%.

Sub-Matrix: SOIL

				Laboratory Duplicate (DUP) Report					
Laboratory sample ID	Sample ID	Method: Compound	CAS Number	LOR	Unit	Original Result	Duplicate Result	RPD (%)	Acceptable RPD (%)
<b>EA002: pH 1:5 (Soils) (QC Lot: 3770355)</b>									
EP2107544-002	TP1 - 900mm to 1100mm	EA002: pH Value	----	0.1	pH Unit	6.1	6.1	0.0	0% - 20%
<b>EA010: Conductivity (1:5) (QC Lot: 3770356)</b>									
EP2107544-002	TP1 - 900mm to 1100mm	EA010: Electrical Conductivity @ 25°C	----	1	µS/cm	22	22	0.0	0% - 20%
<b>ED007: Exchangeable Cations (QC Lot: 3780436)</b>									
EP2107521-057	Anonymous	ED007: Exchangeable Sodium Percent	----	0.1	%	2.9	3.0	3.6	0% - 20%
		ED007: Exchangeable Calcium	----	0.1	meq/100g	16.8	14.7	13.3	0% - 20%
		ED007: Exchangeable Magnesium	----	0.1	meq/100g	0.4	0.4	0.0	No Limit
		ED007: Exchangeable Potassium	----	0.1	meq/100g	<0.1	<0.1	0.0	No Limit
		ED007: Exchangeable Sodium	----	0.1	meq/100g	0.5	0.5	0.0	No Limit
		ED007: Cation Exchange Capacity	----	0.1	meq/100g	17.8	15.6	13.1	0% - 20%
<b>EK072: Phosphate Sorption Capacity (QC Lot: 3776718)</b>									
EP2107544-002	TP1 - 900mm to 1100mm	EK072: Phosphate Sorption Capacity	----	250	mg P sorbed/kg	688	409	50.9	No Limit
		EK072: Phosphate Sorption Index	----	1	mgkg <sup>-1</sup> /log10ug L <sup>-1</sup>	60	60	0.0	0% - 20%



### Method Blank (MB) and Laboratory Control Sample (LCS) Report

The quality control term Method / Laboratory Blank refers to an analyte free matrix to which all reagents are added in the same volumes or proportions as used in standard sample preparation. The purpose of this QC parameter is to monitor potential laboratory contamination. The quality control term Laboratory Control Sample (LCS) refers to a certified reference material, or a known interference free matrix spiked with target analytes. The purpose of this QC parameter is to monitor method precision and accuracy independent of sample matrix. Dynamic Recovery Limits are based on statistical evaluation of processed LCS.

Sub-Matrix: **SOIL**

Method: Compound	CAS Number	LOR	Unit	Method Blank (MB) Report	Laboratory Control Spike (LCS) Report				
				Result	Spike Concentration	Spike Recovery (%)		Acceptable Limits (%)	
						LCS	Low	High	
<b>EA002: pH 1:5 (Soils) (QCLot: 3770355)</b>									
EA002: pH Value	----	----	pH Unit	----	4 pH Unit	100	70.0	130	
				----	7 pH Unit	100	70.0	130	
<b>EA010: Conductivity (1:5) (QCLot: 3770356)</b>									
EA010: Electrical Conductivity @ 25°C	----	1	µS/cm	<1	1412 µS/cm	99.6	93.6	106	
<b>ED007: Exchangeable Cations (QCLot: 3780436)</b>									
ED007: Exchangeable Calcium	----	0.1	meq/100g	<0.1	21.6 meq/100g	91.0	82.9	117	
ED007: Exchangeable Magnesium	----	0.1	meq/100g	<0.1	1.76 meq/100g	91.3	78.4	119	
ED007: Exchangeable Potassium	----	0.1	meq/100g	<0.1	1 meq/100g	107	87.9	129	
ED007: Exchangeable Sodium	----	0.1	meq/100g	<0.1	0.9 meq/100g	103	92.9	132	
ED007: Cation Exchange Capacity	----	0.1	meq/100g	<0.1	25.3 meq/100g	92.0	84.7	117	
ED007: Exchangeable Sodium Percent	----	0.1	%	<0.1	----	----	----	----	

### Matrix Spike (MS) Report

The quality control term Matrix Spike (MS) refers to an intralaboratory split sample spiked with a representative set of target analytes. The purpose of this QC parameter is to monitor potential matrix effects on analyte recoveries. Static Recovery Limits as per laboratory Data Quality Objectives (DQOs). Ideal recovery ranges stated may be waived in the event of sample matrix interference.

- **No Matrix Spike (MS) or Matrix Spike Duplicate (MSD) Results are required to be reported.**

## QA/QC Compliance Assessment to assist with Quality Review

Work Order	: EP2107544	Page	: 1 of 4
Client	: GHD PTY LTD	Laboratory	: Environmental Division Perth
Contact	: MS VICKI DAVIES	Telephone	: +61-8-9406 1301
Project	: 12546218 Albany Motorsports Park DA	Date Samples Received	: 01-Jul-2021
Site	: ----	Issue Date	: 13-Jul-2021
Sampler	: ----	No. of samples received	: 15
Order number	: 12546218	No. of samples analysed	: 6

This report is automatically generated by the ALS LIMS through interpretation of the ALS Quality Control Report and several Quality Assurance parameters measured by ALS. This automated reporting highlights any non-conformances, facilitates faster and more accurate data validation and is designed to assist internal expert and external Auditor review. Many components of this report contribute to the overall DQO assessment and reporting for guideline compliance.

Brief method summaries and references are also provided to assist in traceability.

### Summary of Outliers

#### Outliers : Quality Control Samples

This report highlights outliers flagged in the Quality Control (QC) Report.

- **NO Method Blank value outliers occur.**
- **NO Duplicate outliers occur.**
- **NO Laboratory Control outliers occur.**
- **NO Matrix Spike outliers occur.**
- **For all regular sample matrices, NO surrogate recovery outliers occur.**

#### Outliers : Analysis Holding Time Compliance

- **NO Analysis Holding Time Outliers exist.**

#### Outliers : Frequency of Quality Control Samples

- **NO Quality Control Sample Frequency Outliers exist.**



## Analysis Holding Time Compliance

If samples are identified below as having been analysed or extracted outside of recommended holding times, this should be taken into consideration when interpreting results.

This report summarizes extraction / preparation and analysis times and compares each with ALS recommended holding times (referencing USEPA SW 846, APHA, AS and NEPM) based on the sample container provided. Dates reported represent first date of extraction or analysis and preclude subsequent dilutions and reruns. A listing of breaches (if any) is provided herein.

Holding time for leachate methods (e.g. TCLP) vary according to the analytes reported. Assessment compares the leach date with the shortest analyte holding time for the equivalent soil method. These are: organics 14 days, mercury 28 days & other metals 180 days. A recorded breach does not guarantee a breach for all non-volatile parameters.

Holding times for VOC in soils vary according to analytes of interest. Vinyl Chloride and Styrene holding time is 7 days; others 14 days. A recorded breach does not guarantee a breach for all VOC analytes and should be verified in case the reported breach is a false positive or Vinyl Chloride and Styrene are not key analytes of interest/concern.

Matrix: **SOIL**

Evaluation: \* = Holding time breach ; ✓ = Within holding time.

Method Container / Client Sample ID(s)	Sample Date	Extraction / Preparation			Analysis			
		Date extracted	Due for extraction	Evaluation	Date analysed	Due for analysis	Evaluation	
<b>EA002: pH 1:5 (Soils)</b>								
<b>Snap Lock Bag (EA002)</b> TP3 - 300mm to 600mm, TP5 - 400mm to 800mm,	TP4 - 400mm to 800mm, TP6 - 500mm to 800mm	25-Jun-2021	02-Jul-2021	02-Jul-2021	✓	02-Jul-2021	02-Jul-2021	✓
<b>Soil Glass Jar - Unpreserved (EA002)</b> TP1 - 900mm to 1100mm,	TP2 - 500mm to 900mm	25-Jun-2021	02-Jul-2021	02-Jul-2021	✓	02-Jul-2021	02-Jul-2021	✓
<b>EA010: Conductivity (1:5)</b>								
<b>Snap Lock Bag (EA010)</b> TP3 - 300mm to 600mm, TP5 - 400mm to 800mm,	TP4 - 400mm to 800mm, TP6 - 500mm to 800mm	25-Jun-2021	02-Jul-2021	02-Jul-2021	✓	02-Jul-2021	30-Jul-2021	✓
<b>Soil Glass Jar - Unpreserved (EA010)</b> TP1 - 900mm to 1100mm,	TP2 - 500mm to 900mm	25-Jun-2021	02-Jul-2021	02-Jul-2021	✓	02-Jul-2021	30-Jul-2021	✓
<b>ED007: Exchangeable Cations</b>								
<b>Snap Lock Bag (ED007)</b> TP3 - 300mm to 600mm, TP5 - 400mm to 800mm,	TP4 - 400mm to 800mm, TP6 - 500mm to 800mm	25-Jun-2021	08-Jul-2021	23-Jul-2021	✓	08-Jul-2021	23-Jul-2021	✓
<b>Soil Glass Jar - Unpreserved (ED007)</b> TP1 - 900mm to 1100mm,	TP2 - 500mm to 900mm	25-Jun-2021	08-Jul-2021	23-Jul-2021	✓	08-Jul-2021	23-Jul-2021	✓
<b>EK072: Phosphate Sorption Capacity</b>								
<b>Soil Glass Jar - Unpreserved (EK072)</b> TP1 - 900mm to 1100mm, TP3 - 300mm to 600mm, TP5 - 400mm to 800mm,	TP2 - 500mm to 900mm, TP4 - 400mm to 800mm, TP6 - 500mm to 800mm	25-Jun-2021	----	----	----	06-Jul-2021	22-Dec-2021	✓



## Quality Control Parameter Frequency Compliance

The following report summarises the frequency of laboratory QC samples analysed within the analytical lot(s) in which the submitted sample(s) was(were) processed. Actual rate should be greater than or equal to the expected rate. A listing of breaches is provided in the Summary of Outliers.

Matrix: **SOIL**

Evaluation: ✖ = Quality Control frequency not within specification ; ✔ = Quality Control frequency within specification.

Quality Control Sample Type	Method	Count		Rate (%)			Quality Control Specification
		QC	Reaular	Actual	Expected	Evaluation	
<b>Analytical Methods</b>							
<b>Laboratory Duplicates (DUP)</b>							
Electrical Conductivity (1:5)	EA010	1	6	16.67	10.00	✔	NEPM 2013 B3 & ALS QC Standard
Exchangeable Cations	ED007	1	8	12.50	10.00	✔	NEPM 2013 B3 & ALS QC Standard
P Sorption Index & P Sorption Capacity	EK072	1	6	16.67	10.00	✔	NEPM 2013 B3 & ALS QC Standard
pH (1:5)	EA002	1	6	16.67	10.00	✔	NEPM 2013 B3 & ALS QC Standard
<b>Laboratory Control Samples (LCS)</b>							
Electrical Conductivity (1:5)	EA010	1	6	16.67	5.00	✔	NEPM 2013 B3 & ALS QC Standard
Exchangeable Cations	ED007	1	8	12.50	5.00	✔	NEPM 2013 B3 & ALS QC Standard
pH (1:5)	EA002	2	6	33.33	10.00	✔	NEPM 2013 B3 & ALS QC Standard
<b>Method Blanks (MB)</b>							
Electrical Conductivity (1:5)	EA010	1	6	16.67	5.00	✔	NEPM 2013 B3 & ALS QC Standard
Exchangeable Cations	ED007	1	8	12.50	5.00	✔	NEPM 2013 B3 & ALS QC Standard



## Brief Method Summaries

The analytical procedures used by the Environmental Division have been developed from established internationally recognized procedures such as those published by the US EPA, APHA, AS and NEPM. In house developed procedures are employed in the absence of documented standards or by client request. The following report provides brief descriptions of the analytical procedures employed for results reported in the Certificate of Analysis. Sources from which ALS methods have been developed are provided within the Method Descriptions.

Analytical Methods	Method	Matrix	Method Descriptions
pH (1:5)	EA002	SOIL	In house: Referenced to Rayment and Lyons 4A1 and APHA 4500H+. pH is determined on soil samples after a 1:5 soil/water leach. This method is compliant with NEPM Schedule B(3).
Electrical Conductivity (1:5)	EA010	SOIL	In house: Referenced to Rayment and Lyons 3A1 and APHA 2510. Conductivity is determined on soil samples using a 1:5 soil/water leach. This method is compliant with NEPM Schedule B(3).
Exchangeable Cations	ED007	SOIL	In house: Referenced to Rayment & Lyons Method 15A1. Cations are exchanged from the sample by contact with Ammonium Chloride. They are then quantitated in the final solution by ICPAES and reported as meq/100g of original soil. This method is compliant with NEPM Schedule B(3).
P Sorption Index & P Sorption Capacity	EK072	SOIL	In house: Referenced to Rayment & Lyons Method 9H1 & 9I1 Soil is brought to equilibrium with a solution of P at known concentration. P absorbed, released is determined by FIA analysis of the final solution.

Preparation Methods	Method	Matrix	Method Descriptions
Exchangeable Cations Preparation Method	ED007PR	SOIL	In house: Referenced to Rayment & Lyons method 15A1. A 1M NH <sub>4</sub> Cl extraction by end over end tumbling at a ratio of 1:20. There is no pretreatment for soluble salts. Extracts can be run by ICP for cations.
1:5 solid / water leach for soluble analytes	EN34	SOIL	10 g of soil is mixed with 50 mL of reagent grade water and tumbled end over end for 1 hour. Water soluble salts are leached from the soil by the continuous suspension. Samples are settled and the water filtered off for analysis.



# Appendix F

**Aquarius Wastewater Systems Pty Ltd**

# AQUARIUS® Systems

<b>1 – 5 Bedrooms</b>	O-3 ATU	O-2 NR ATU	O-2 ATU
<b>6 – 9 Bedrooms</b>	O-3 3KL ATU	O-2 NR 3KL ATU	O-2 3KL ATU
<b>Commercial</b>	AQUARIUS® Standard or Custom Designed Commercial Systems Please speak to our Sales Consultant		

## Specifications

	O-3	O-2 NR	O-2
<b><u>System Features</u></b>			
Poly/Duralen Plastic or Concrete Tank Construction	✓	✓	✓
<b>Nutrient Retentive</b> (Phosphorous removal)	✓	✓	
Ozone Disinfection	✓		
Recycles all wastewater through irrigation into gardens, orchards, etc.	✓	✓	✓
Supplied complete with irrigation components, electrical components and pumps	✓	✓	✓
Footprint required approx 6m x 2.5m x 2m**	✓	✓	✓
Low Energy use	✓	✓	✓
<b><u>Irrigation Area</u></b>			
Above Ground Dripper Irrigation	✓		
Sub-Surface Dripper Irrigation	✓	✓	✓
Irrigation area in sandy soil conditions – *150m <sup>2</sup>	✓	✓	✓
<b><u>Other Disposal options</u></b>			
Leach Drains / Soakwells / Aquasafe Drains	✓	✓	✓
<b><u>Maintenance</u></b>			
Service calls per year as per DoH WA requirements	2	2	2
<b><u>Manufacturers Warranties</u></b>			
Poly/Duralen Plastic Tanks 15 years	✓	✓	✓
Orange Pumps 1 year	✓	✓	✓
Irrigation and Electrical components 1 year	✓	✓	✓
<b><u>Approvals</u></b>			
Fully approved by the WA Department of Health	✓	✓	✓
Australian Standards approved AS/NZS 1546.3	✓	✓	✓
<b><u>Why choose Aquarius</u></b>			
Wholly owned West Australian Company	✓	✓	✓
Manufactured in Western Australia	✓	✓	✓
Extensive Support Network covering all of WA	✓	✓	✓
Local Agents fully trained and registered with Department of Health WA	✓	✓	✓

\*Subject to local authority approval

\*\*Subject to configuration of ATU

## Treatment Process

	O-3	O-2 NR	O-2
<p><b><u>Primary Tank</u></b> Retains the solids and uses aerobic and anaerobic bacteria to breakdown the BOD<sub>5</sub> levels in the sewage.</p>	✓	✓	✓
<p><b><u>Alum Tank</u></b> Doses the Clarifying chamber of the Treatment tank with Alum. Alum acts as a flocculent to remove the nutrients and suspended solids and settle them to the bottom of the tank for further aerobic bacteria breakdown.</p>	✓	✓	
<p><b><u>Treatment Tank</u></b></p> <p><b>Secondary / Aeration Chamber</b> Incorporates aeration to further break down BOD<sub>5</sub> and nitrates.</p> <p>✓</p>	✓	✓	
<p><b>Clarifying Chamber</b> The Clarifying Chamber provides a settling and clarifying period for the water prior to discharge.</p> <p>✓</p>	✓	✓	
<p><b>Discharge Chamber</b> The Discharge chamber contains the Discharge Pump to pump the treated water out to irrigation or other disposal methods.</p> <p>✓</p>	✓	✓	
<p><b>Ozonation Pump</b> Ozone is a powerful disinfectant, many times more effective than chlorine and kills all bacteria.</p> <p>✓</p>			
<p><b><u>DoH WA ATU Water Quality Criteria</u></b></p> <p>&lt;20mg/L BOD<sub>5</sub></p> <p>&lt;30mg/L suspended solids</p> <p>&lt;10 E.coli/100ml</p> <p>&gt;3mg/L Ozone concentration</p> <p>&lt;1mg/L (98.5%) TP (% removal)</p> <p>&lt;10mg/L (97.8%) TN (% removal)</p>	<p>✓</p> <p>✓</p> <p>✓</p> <p>✓</p> <p>✓</p> <p>✓</p>	<p>✓</p> <p>✓</p> <p></p> <p>✓</p> <p>✓</p> <p>✓</p>	<p>✓</p> <p>✓</p> <p></p> <p></p> <p></p> <p>✓</p>



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